

CERAMIC BEARINGS AND **EXSEV** BEARINGS

FOR EXTREME SPECIAL ENVIRONMENTS







CAT. NO. B2004E-2



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Koyo CERAMIC BEARINGS AND EXSEV BEARINGS FOR EXTREME SPECIAL ENVIRONMENTS





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Products and Applications

Koyo Ceramic Bearings and **EXSEV** Bearings for Extreme Special Environments are used for a wide range of the state of the art technologies.



Ceramic Bearings

Application

Corrosive Electric field orrosion Resistant Hybrid Ceramic Bearing Ceramic Bearings Non-magnetic Hybrid Ceramic Bearings **Hybrid Ceramic Bearings** High temperature High Temperature Clean Pro Bearings **PN** Bearings **WS Bearings MO Bearings MG Bearings** III Complement Ceramic Ball Bearing Magnetic field Full Complement Ceramic Ball Bearing **Ceramic Bearings**

Non-magnetic Hybrid Ceramic Bearing

EXSEV BEAR ING SERIES

ull Complement Ceramic Ball Bearing

Ceramic Bearings

on-magnetic Hybrid Ceramic Bearin series Full Complement Hybrid Ceramic Ball Beari

Development and Manufacturing Facilities

By continuously incorporating new improvements, Koyo Ceramic Bearings and **EXSEV** Bearings are applicable in more technologies than ever.

Technologies are advancing rapidly and bearings are required to satisfy more complicated and varied requirements under increasingly hostile operating conditions.

In response to such needs, JTEKT is committed to the development and manufacture of the EXSEV Bearing Series using the latest research / development and manufacturing facilities.

JTEKT intends to supply products that live up to customers' expectations, while contributing to environmental conservation and energy saving through streamlined manufacturing.

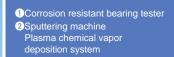






















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EXSEV Bearings: Composition and Selection

Conventional bearings, made from bearing steel, and lubricants such as oil and grease, may not be applicable in an extreme special environment such as a clean room, vacuum, high temperature application or corrosive environment, or when special characteristics are required, such as being non-magnetic, or insulating, or having superior high speed performance.

Koyo EXSEV Bearings are a special bearing series, developed specifically to address such needs.

Please consult JTEKT when using bearings in a new, unprecedented environment, or when bearings with special characteristics are required.



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Bearings and Special Steel

1 Ceramic Bearings and Special Steel Bearings

The EXSEV Bearing Series has been developed for use in special applications where conventional bearings are not practical.

The EXSEV Bearings incorporate components made from special material and use special lubricants, to be applicable in extreme special environments such as a clean room, vacuum,

1-1 Ceramic Bearings

Ceramic Bearings, including components made from ceramic, have the special properties that steel bearings do not have, such as being non-magnetic or insulating. They can be used in new applications where conventional bearings have not been practical.

high temperature application, or corrosive condition, and to realize special characteristics, such as being non-magnetic, or insulating, or having superior high speed performance.

The EXSEV Bearing series consist of Ceramic Bearings and Special Steel Bearings, depending on the specific materials of the components.

Ceramic Bearings are highly heat resistant, enabling a rolling bearing to be practical in a high temperature environment. The low density of ceramic decreases the centrifugal force induced by rolling elements (balls or rollers), contributing to an increased speed of the apparatus.

Properties of ceramic materials

1) Material characteristics

Table 1-1 below lists the mechanical and physical properties of major ceramic materials used as bearing materials. Table 1-2 compares silicon nitride and high carbon chromium bearing steel.

• Table 1-1 Mechanical and physical properties of ceramic materials used as bearing materials

Ceramic Material Property Unit	Silicon Nitride Si ₃ N ₄	Zirconia ZrO ₂	Silicon Carbide SiC
Density g/cm³	3.2	6.0	3.1
Linear expansion coefficient K ⁻¹	3.2×10 ⁻⁶	10.5×10 ⁻⁶	3.9×10 ⁻⁶
Vickers hardness HV	1 500	1 200	2 200
Module of longitudinal elasticity GPa	320	220	380
Poisson's ratio	0.29	0.31	0.16
Three point bending strength MPa	1 100	1 400	500
Fracture toughness MPa · m ^{1/2}	6	5	4
Heat resistance (in atmospheric air) C	800	200	1 000 or higher
Thermal shock resistance °C	750 or higher	350	350
Coefficient of thermal conductivity W/(m · K)	20	3	70
Specific heat J/(kg · K)	680	460	670

Table 1-2 Comparison of characteristics of silicon nitride and high carbon chromium bearing steel

Property Unit	Silicon Nitride Si ₃ N ₄	High Carbon Chromium Bearing Steel SUJ2	Advantages of Ceramic Bearings
Density g/cm ²	3.2	7.8	Decrease in centrifugal force induced by rolling elements (balls or rollers) → Longer service life and reduced bearing temperature rises
Linear expansion coefficient K ⁻¹	3.2×10 ⁻⁶	12.5×10 ⁻⁶	Decreased internal clearance change due to reduced bearing temperature rises → Lowered vibration and reduced preload changes
Vickers hardness HV	1 500	750	
Module of longitudinal elasticity GPa	320	208	Less deformation in rolling contact areas → Higher rigidity
Poisson's ratio	0.29	0.3	, a ringiliar rigidally
Heat resistance °C	800	180	Retention of superior load carrying characteristics under high temperature
Corrosion resistance	High	Low	Useful in acid or alkaline solutions
Magnetism	Non-magnetic	Ferromagnetic	Decreased rotational fluctuation in ferromagnetic field due to non-magnetization
Conductivity	insulator	conductor	Prevents electrical pitting
Bond	Covalent bond	Metallic bond	Decrease in adhesion (or material transfer) due to oil film thinning in rolling contact areas

2) Rolling fatigue of ceramic materials

The individual ceramic materials were tested for rolling fatigue under oil lubrication and under water lubrication, to evaluate their applicability as bearing material. Figs. 1-1 and 1-2 show the results of the tests.

The figures indicate that each ceramic material has a certain level of rolling fatigue strength and that silicon nitride has the highest fatigue strength among the ceramic materials tested.

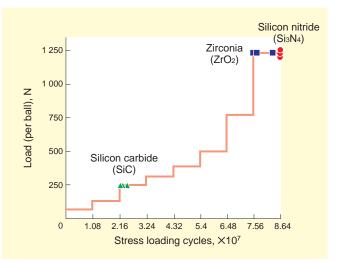


Fig. 1-1 Comparison in rolling fatigue life under oil lubrication

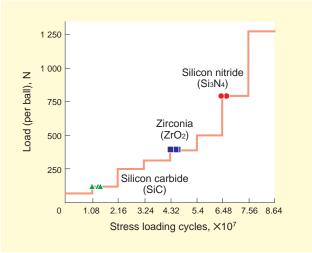
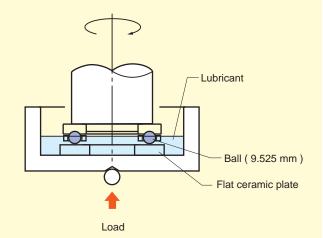


Fig. 1-2 Comparison in rolling fatigue life under water lubrication

Test conditions

	Oil lubrication	Water lubrication	
Lubricant	Spindle oil City water		
Ball	Bearing steel Ceramic		
Load	Increased in stages at every 1.08 × 10 ⁷ cycles		
Rotational speed	1 200 min ⁻¹		

Test equipment



Test equipment appearance



Fig. 1-3 Rolling fatigue life test conditions and test equipment

3) Ceramic materials suitable for rolling bearings

Table 1-3 shows the results of evaluating the ceramic materials in terms of their characteristics and the rolling fatigue strength. Among the ceramic materials tested, silicon nitride is the most suitable as rolling bearing material.

JTEKT uses the silicon nitride produced by the hot isostatic pressing (HIP) method as the standard ceramic material for bearings.

4) Composition of ceramic bearings

Koyo ceramic bearings are divided into Full Ceramic Bearings (with all components, namely, the outer ring, inner ring and rolling elements, made of ceramic) and Hybrid Ceramic Bearings (with only the rolling elements made of ceramic). The outer ring and inner ring of the Hybrid Ceramic Bearings are made from special steel, including high carbon chromium bearing steel. The cage may be made of a metallic material, resin, or composite material, depending on the intended operating conditions of the bearing.

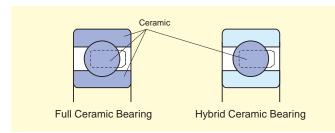


Fig. 1-4 Composition of ceramic bearings

• Table 1-3 Ratings of ceramic materials as rolling bearing materials

		Application to rolling bearings			
	Rating	Performance and use	Characteristics		
Silicon nitride Si ₃ N ₄	0	Comparable to bearing steel in load carrying capability and service life Suitable for high performance applications	High speed High vacuum Corrosion resistant Heat resistant Non-magnetic High rigidity		
Zirconia ZrO ₂	0	Useful under a limited load Applicable in highly corrosive chemicals	· Highly corrosion resistant		
Silicon carbide SiC	0	Useful under a limited load Applicable in highly corrosive chemicals	Highly corrosion resistant Highly heat resistant		

■ Load ratings and service life of ceramic bearings

Silicon nitride, a ceramic material, is more rigid than high carbon chromium bearing steel; therefore, a bearing including silicon nitride components is subject to a higher contact stress on the area of contact between bearing raceways and rolling elements. Accordingly, to estimate the service life of ceramic bearings, whether the rolling bearing theory is applicable or not is critical.

Basic dynamic load rating

The ISO standard defines the basic dynamic load rating as the pure radial load (for radial bearings), constant in magnitude and direction, under which the basic rating life of 1 million revolutions can be obtained, when the inner ring rotates while the outer ring is stationary or vice versa. The basic dynamic load rating represents the resistance of a bearing against rolling fatigue.

Basic static load rating

The basic static load rating is defined as the static load which corresponds to the calculated contact stress shown below, at the center of the most heavily loaded raceway/rolling elements.

Self-aligning ball bearings : 4 600 MPa
Other ball bearings : 4 200 MPa
Roller bearings : 4 000 MPa

JTEKT defines the dynamic load rating and static load rating of ceramic bearings based on the results of their service life tests, the maximum allowable static load of the ceramic materials, the elastic deformation test results of high carbon chromium bearing steel, and other related data, as shown in Table 1-4.

● Table 1-4 Load ratings of ceramic bearings

	Full Ceramic Bearing	Hybrid Ceramic Bearing
Dynamic load rating C_{r}	Comparable to steel bearings	Comparable to steel bearings
Static load rating $C_{0\mathrm{r}}$	Comparable to steel bearings	85% that of steel bearings

The steel bearings here refer to bearings consisting of rings and rolling elements both made of high carbon chromium bearing steel.

1) Rolling fatigue life of ceramic bearings

A typical service life test for Ceramic Bearings and steel bearings was performed under the conditions specified in Fig. 1-6.

The test results showed that the service life of Ceramic Bearings was equal to or longer than that of steel bearings, exceeding the calculated life.

The Ceramic Bearings were found to exhibit flaking (Fig. 1-5) when their service life terminated. The same phenomenon was observed on the steel bearings whose service life terminated.

Based on these findings, as the dynamic load rating of a Ceramic Bearing, that of a steel bearing of the same dimensions can be used.

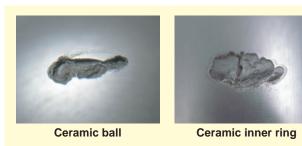
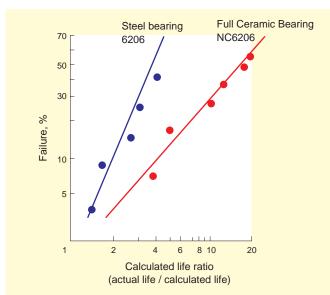


Fig. 1-5 Flaking on ceramic ball and inner ring



Rolling fatigue test conditions

Temperature

Bearing number	Material (outer/inner rings and balls)		Dimensions, mm
NC6206	Silic	con nitride(Si3N4)	30 × 62 × 16
6206	Bea	ring steel(SUJ2)	(bore × outside dia. × width)
Specification		C	Condition
Load			5 800 N
Rotational speed 8		000 min ⁻¹	
Lubrication oil AeroShel		ell Turbine Oil 500	

Fig. 1-6 Rolling fatigue life of Full ceramic bearings and steel bearings

70 ± 2 °C

5

Ceramic Bearings and Special Steel

2) Static load rating of ceramic bearings

The basic static load rating of a steel bearing represents a load that produces a localized permanent deformation in the rolling element/raceway contact area, impeding smooth rotation.

However, ceramic materials, which are highly rigid, produce little permanent deformation. Therefore, the theory of the basic static load rating for steel bearings is not applicable to ceramic bearings.

Static load rating of Full Ceramic Bearings

When exposed to continuous excessive loads, ceramic materials may break down; however, before breakdown occurs, the materials develop cracking.

Fig. 1-7 compares the load measurements at which ceramic balls developed cracking with the basic static load ratings of steel bearings. Fig. 1-8 shows the measurement system.

As these results show, the loads at which cracks develop on the Full Ceramic Bearing are far higher than that of the basic static load rating of steel bearings. This means that the basic load ratings specified in the ISO standard can be used as the allowable static loads of the Full Ceramic Bearing.

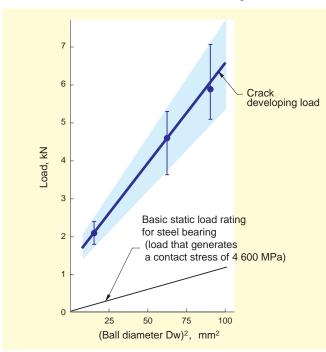


Fig. 1-7 Crack developing loads for Full Ceramic Bearings

Static load rating of Hybrid Ceramic Bearings

The theory of the static load rating for steel bearings is applicable to Hybrid Ceramic Bearings because their outer and inner rings are made of steel and accordingly any deformation is permanent.

Table 1-5 shows the results of a test for which a high carbon chromium bearing steel ball and ceramic ball were pressed against a flat plate of high carbon chromium bearing steel and the resulting permanent deformations (indentation depths) on the flat plate and balls were measured.

 Table 1-5 Measurements of permanent deformation produced on flat steel plate and balls

Load kN		Permanent deformation (average), mm		Permanent deformation	
		Flat plate (bearing steel)	Ball	(sum of averages), mm	
all	0.65	0.5	_	0.5	
ic b	1.3	1.9	_	1.9	
Ceramic ball	2.6	5.2	_	5.2	
Ce	3.9	9.3	_	9.3	
=	0.65	0.4	_	0.4	
ball	1.3	1.3	0.11	1.41	
Steel	2.6	4.0	0.41	4.41	
(O)	3.9	6.8	1.18	7.98	

These results indicate that ceramic balls do not suffer permanent deformation and that the permanent deformation produced on the flat steel plate by the ceramic balls is approximately 1.2 times the sum of the deformation produced on the flat plate by steel ball and the deformation that the steel ball undergo.

Accordingly, the static load rating of Hybrid Ceramic Bearings can be determined based on the permanent deformation of their bearing steel rings. JTEKT uses the load equal to 85% of the static load rating of steel bearings as the static load rating of the Hybrid Ceramic Bearings.

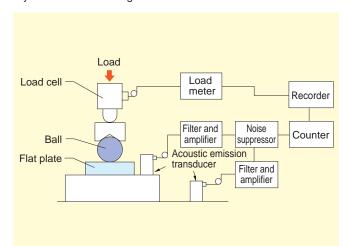


Fig. 1-8 Crack generating load measurement system

3) Impact strength of ceramic bearings

To evaluate the impact strength of ceramic bearings, ceramic balls were crushed by two methods: by a static load and an impact load. The test results are shown in Fig. 1-9. Fig. 1-10 shows the testing methods.

This figure shows that the impact strength of the ceramic bearings is almost equal to the static load strength, which means the bearings possess sufficient impact strength.

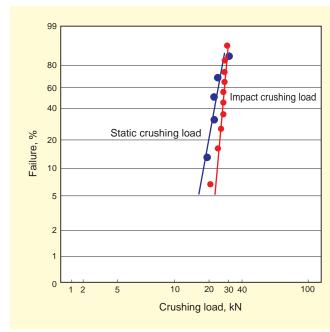


Fig. 1-9 Comparison of static load and impact load that crush ceramic balls

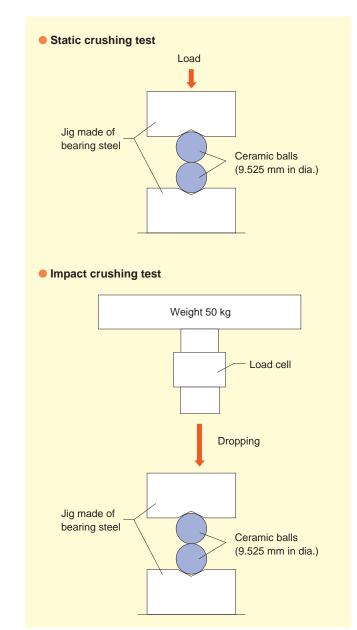


Fig. 1-10 Ceramic ball crushing test method

4) Fitting of ceramic bearings

When using ceramic bearings, it should be noted that ceramic materials are largely different from steel materials in the coefficient of linear expansion. Attention should therefore be paid to fitting stresses and temperature rises.

The following are the results of evaluating the fitting of a Ceramic Bearing on a stainless steel shaft.

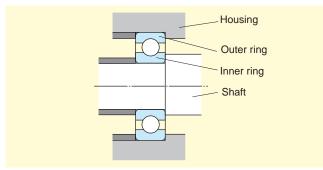


Fig. 1-11 Bearing fitting

Maximum stress produced by fitting

Table 1-6 shows the results of a static strength test conducted on a ceramic ring fitted on a stainless steel shaft. Table 1-7 shows the results of a dynamic strength test (running test) conducted on a ceramic ring fitted on a stainless steel shaft.

Based on the results of these tests, JTEKT makes it a rule for the maximum stress produced by interference to be no greater than 150 MPa when a ceramic inner ring is fitted on a stainless steel shaft.

Consult JTEKT for applications requiring tighter fitting.

 Table 1-6 Typical results of static strength test on ceramic bearing shaft fitting

	Interference, L ₁₀ µ m	Ring's fracture stress MPa
Solid shaft	50	399
Hollow shaft	68	332

 Table 1-7 Typical results of dynamic strength test on ceramic bearing shaft fitting

	Max. allowable interference µ m	Max. allowable stress for ring MPa
Solid shaft	31	243
Hollow shaft	43	204

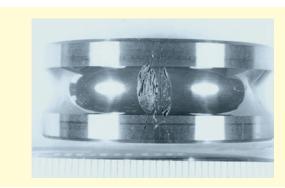


Fig. 1-12 Ceramic inner ring damaged by dynamic strength test

Influence of temperature

During operation, bearing temperature exceeds the ambient temperature. When a ceramic bearing is operated on a stainless steel shaft or in a stainless steel housing, the interference with the shaft increases due to the difference in linear expansion coefficient while the interference with the housing decreases. (When the outer ring is loose-fitted, the clearance increases.)

To determine the class of fit for a ceramic bearing, the maximum temperature during operation should be assessed carefully.

■ The maximum stress generated on the inner ring due to the interference with the shaft can be determined from the following equation:

$$\sigma = P_{\text{m}} \cdot \frac{D_{\text{i}}^{2} + d^{2}}{D_{\text{i}}^{2} - d^{2}}$$

$$P_{\text{m}} = \Delta_{\text{deff}} \left[\frac{d}{E_{\text{B}}} \left(\frac{D_{\text{i}}^{2} + d^{2}}{D_{\text{i}}^{2} - d^{2}} + \nu_{\text{B}} \right) + \frac{d}{E_{\text{S}}} \left(\frac{d^{2} + d_{0}^{2}}{d^{2} - d_{0}^{2}} - \nu_{\text{S}} \right) \right]^{-1}$$

σ	: Maximum circumferential stress to interference	(MPa)
$P_{ m m}$: Pressure of contact on fitting surface	(MPa)
d, D i	: Inner ring bore diameter and outside diameter	(mm)
Δd eff	: Effective interference of inner ring	(mm)
d0	: Bore diameter of hollow shaft	(mm)
E B, ν B	: Bearing's modulus of longitudinal elasticity and Poisson's ratio	(MPa)
E s, ν s	: Shaft's modulus of longitudinal elasticity and Poisson's ratio	(MPa)

1-2 Special Steel Bearings

Table 1-8 lists the typical special steels used to produce the bearing rings and rolling elements of EXSEV Bearings.

● Table 1-8 Characteristics of the typical special steels used for EXSEV Bearings

⊚: Superior, ○: Good

	Hardness HRC	Modulus of longitudinal elasticity GPa	Coefficient of linear expansion ×10 ⁻⁶ K ⁻¹	Load carrying capability	Applications
High carbon chromium bearing steel SUJ2	61	208	12.5	0	Hybrid Ceramic Bearings for insulation, etc.
Martensitic stainless steel SUS440C	60	208	10.5	0	Clean environments and vacuum environments
Precipitation hardening stainless steel SUS630	40	196	11.0	0	Corrosive environments
High speed tool steel M50	61	207	10.6	0	High temperature environments
High speed tool steel SKH4	64	207	12.0	0	High temperature environments
Non-magnetic stainless steel	43	200	18.0	0	Magnetic field environments

1) Bearings for use in clean and/or vacuum environments

The rings and rolling elements of conventional bearings are made of high carbon chromium bearing steel (JIS SUJ2), which is resistant to rolling fatigue. However, due to a relatively low corrosion resistance, this steel requires application of anticorrosive oil or other suitable rust preventive measure.

Applying anticorrosive oil to bearings is not favorable for use in a clean and / or vacuum environment, due to the possibility of contamination. Accordingly, EXSEV Bearings use martensitic stainless steel (JIS SUS440C), which is highly corrosion resistant, as a standard material for use in a clean environment.

2) Bearings for use in corrosive environments

For a highly corrosive environment where the SUS440C is not enough to prevent corrosion, precipitation hardening stainless steel (JIS SUS630) is used. However, SUS630 has a hardness of 40 HRC, which is inferior to other materials in load carrying capability and rolling fatigue strength.

3) Bearings for use in high temperature environments

Fig. 1-13 shows the high temperature hardness of various materials. SUS440C has a hardness of 55 HRC at 300°C, which means it can be used in a high temperature environment of up to approximately 300°C. In an environment heated in excess of 300°C, high speed tool steel (JIS SKH4, AISI M50, etc.) should be used.

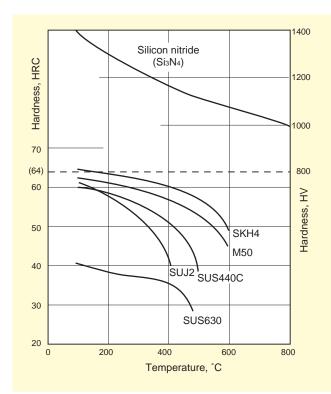


Fig. 1-13 High temperature hardness of various bearing materials

2 Lubricants for EXSEV Bearings

Bearing performance depends on lubrication; it is no exaggeration to say that lubrication determines the service life of bearings. Grease or a solid lubricant is properly used to lubricate the EXSEV bearings.

Compared with solid lubricants, grease is superior for the high speed performance, load carrying capability, and service life of bearings. Therefore, it is recommended to use grease as much as possible.

Grease cannot be used for some application in an ultrahigh vacuum, high temperature, or clean environment. In an application where oil evaporation from grease is unacceptable, solid lubricants should be used.

2-1 Grease

1) High temperature, vacuum or clean environments

Fluorinated greases are known as useful for high temperature applications. Its base oil is perfluoropolyether (PFPE) and its thickener is polytetrafluoroethylene (PTFE).

Fluorinated grease has a low evaporation pressure, and can be used in a vacuum environment of approximately 10⁻⁵ Pa at room temperature. Another advantage of this grease is low particle emissions, and is applicable in a clean environment. Owing to these excellent characteristics, fluorinated grease is used as the standard grease for the EXSEV Bearings.

2) High vacuum environments

Fluorinated greases are classified according to whether the base oil includes an acetal bond (-O-CF2-O-) and whether side chains are included (Table 2-1).

Note that when a fluorinated grease is used in a vacuum, these differences in molecular structure may cause the molecular chains to be disconnected and decompose, resulting in a difference in the amount of gas emissions in the vacuum.

For the PFPE of the three greases listed in Table 2-1, Fig. 2-1 shows the results of gas emissions evaluation, using four ball type vacuum test equipment.

As can be seen Fig. 2-1, oil A, which originally has the acetal structure, apparently emits a great amount of oxide components, such as CF₂O⁺, C₂F₃O⁺ and C₂F₅O⁺, which are attributed to the decomposition of the acetal structure. It emits a greater amount of gas than other oils.

As the standard grease for the EXSEV Bearings, JTEKT uses fluorinated grease containing oil B or PFPE, whose molecular chains are not easily torn off.

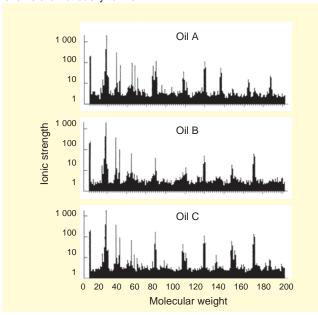


Fig. 2-1 Differences in gas emissions from PFPE

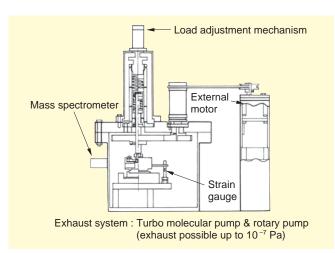


Fig. 2-2 Four ball type vacuum test equipment

■ Table 2-1 Tested PFPEs and their characteristics

Oil	Molecular structure	Viscosity, 20°C mm²/s	Mean molecular weight	Vapor pressure, 20°C Pa
Α	CF ₃ – (OCF ₂ CF ₂) p – (OCF ₂) q – OCF ₃	255	9 500	4 × 10 ⁻¹⁰
В	F – (CF ₂ CF ₂ CF ₂ O) n – CF ₂ CF ₃	500	8 400	7 × 10 ⁻⁹
С	F - (CFCF ₂ O) - CF ₂ CF ₃ CF ₃ m	2 700	11 000	4 × 10 ⁻¹²

2-2 Solid Lubricants

In an environment where oil and grease cannot be used, a solid lubricant is used to lubricate bearings.

Solid lubricants can roughly be classified into soft metals, layer lattice materials, and polymeric materials.

Table 2-2 shows the characteristics of major solid lubricants used for the EXSEV Bearings, along with the major applications where the individual solid lubricants are used.

1) Soft metals

Soft metals, such as silver (Ag) and lead (Pb), are coated on balls by the ion plating method (refer to Fig. 2-3). These lubricants are effective for use in ultrahigh vacuum environments where gas emissions from bearings should be avoided.

Silver coated components require careful handling because silver is susceptible to oxidization and durability deteriorates rapidly once oxidized. Lead is seldom used as a lubricant because it is hostile to the environment.

2) Layer lattice materials

Among layer lattice materials, molybdenum disulfide (MoS2) is coated to the cage and bearing rings, or is used as an additive for composite materials, while tungsten disulfide (WS2) is not used as a coating material but used only as an additive for composite materials (refer to Fig. 2-4).

These lubricants are superior to polymeric materials in heat resistance and load carrying capability, and are used for high temperature applications or applications where a large load carrying capability is required.

Layer lattice materials should not be used in a clean environment because they emit an excessive amount of particles.

3) Polymeric materials

Polymeric materials are coated to the cage and/or bearing rings. They are also used to make cages (refer to Fig. 2-5).

Polymeric materials are suitable for applications where cleanliness is critical or the environment is corrosive. Because they are relatively independent of ambient conditions, they are suitable for applications where bearings are repeatedly exposed to atmospheric air and a vacuum.



Fig. 2-3 Balls coated with silver ion plating

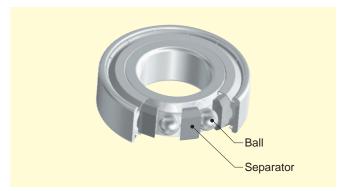


Fig. 2-4 Separator including tungsten disulfide

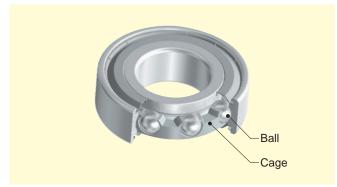


Fig. 2-5 Cage made from fluorocarbon resin

● Table 2-2 Characteristics of major solid lubricants used for EXSEV Bearings

 \bigcirc : Superior. \bigcirc : Good. \triangle : Acceptable

						_			'	
	Solid lubricant		Thermalstability, °C		Coefficient of friction		Particle	Gas	Applications	
	Solid lubi icalit	Atmospheric air	Vacuum	Atmospheric air	Vacuum	MPa	emissions	emissions	Applications	
Soft metals	Silver (Ag)	_	600 or higher	_	0.2 to 0.3	2 500 max.	\triangle	0	Ultrahigh vacuum	
Soft metals	Lead (Pb)	_	300 or higher	0.05 to 0.5	0.1 to 0.15	2 500 max.	\triangle	0	environments	
Layer	Molybdenum disulfide (MoS ₂)	350	400 or higher	0.01 to 0.25	0.001 to 0.25	2 000 max.	\triangle	0	Vacuum environments.	
lattice materials	Tungsten disulfide (WS ₂)	425	400 or higher	0.05 to 0.28	0.01 to 0.2	2 500 max.	\triangle	0	High temperature environments	
	Graphite (C)	500	_	0.05 to 0.3	0.4 to 1.0	2 000 max.	\triangle	0		
Polymeric materials	Polytetrafluoroethylene (PTFE)	260	200	0.04 to 0.2	0.04 to 0.2	1 000 max.	0	\triangle	Clean, vacuum, and/or	
	Polyimide (PI)	300	200 or higher	0.05 to 0.6	0.05 to 0.6	1 000 max.	0	Δ	corrosive environments	

11 12

4) Service life of solid lubricants

Bearings lubricated with a solid lubricant can provide stable running performance as long as the lubricant is supplied continuously. When the lubricant is used up, the metal components become in contact with each other, rapidly increasing running torque and reducing the service life of the bearing. The service life of bearings is greatly influenced by the operating conditions. As a consequence, it is not always possible to accurately estimate the service life of bearings lubricated with solid lubricant because of the variations in operating conditions.

When a solid lubricant is used to lubricate a bearing, the bearing is generally used under a relatively light load, such as 5% or less of the basic dynamic load rating. Based on the results of various experiments under the above mentioned operating conditions, JTEKT provides the following experimental equation to enable an estimation of the service life of a deep groove ball bearing lubricated with a solid lubricant. For details, refer to the following product pages.

Polymeric materials

The average service life of clean pro coated bearings can be estimated by the following equation:

$$L_{\text{av}} = b_2 \cdot \left(\frac{C_{\text{r}} \times 0.85}{P_{\text{r}}} \right)^q \times 0.016667/n$$

Where,

 L_{av} : Average life, h b_2 : Lubrication factor

 $b_2 = 42$

 $C_{
m r}$: Basic dynamic load rating, N $P_{
m r}$: Dynamic equivalent radial load, N q: Exponential coefficient, q = 3

n: Rotational speed, min⁻¹

Clean Pro Bearings Page 31
Clean Pro PRZ Bearings Page 35

Layer lattice materials

The average service life of the EXSEV Bearings whose cage is coated with molybdenum disulfide (MO Bearings) can also be estimated by the above equation, supposing that b_2 equals to 6.

MO Bearings -----Page 45

Soft metal materials

The average service life of the EXSEV Bearing whose balls are silver ion plated (MG Bearing) can be estimated using the following equation:

$$L_{\rm vh} = b_1 \cdot b_2 \cdot b_3 (\frac{C_{\rm r}}{13 \times P_{\rm r}})^q \times 16 667/n$$

Where

 $L_{
m vh}$: 90% reliability service life, h $C_{
m r}$: Basic dynamic load rating, N $P_{
m r}$: Dynamic equivalent radial load, N

q : Exponential coefficient, q = 1

n: Rotational speed, min⁻¹ (10 \leq n \leq 10 000)

 b_1 : Speed factor $b_1 = 1.5 \times 10^{-3} n + 1$

b₂ : Lubrication factor

 $b_2 = 1$

 b_3 : Ambient pressure/temperature factor $b_3 = 1$ (at 10^{-3} Pa and room temperature)

MG Bearings ------Page 47

The basic dynamic load ratings and the permissible radial loads listed in this catalog are as follows.

Basic dynamic load rating: Strength against bearing rolling fatigue

Permissible radial load: They can be regarded as the maximum loads applicable to individual bearings. When an axial load is applied to the bearing, convert this axial load to a dynamic equivalent radial load, and then compare this value to the permissible radial load.

*Bearings lubricated with a solid lubricant are generally damaged by friction and not by rolling fatigue. For this reason, the permissible radial load is listed on each page for bearings lubricated with a solid lubricant.

3 How to Select **EXSEV** Bearings

3-11 Clean Environments

In a clean environment, bearings made of high carbon chromium bearing steel applied with rust preventive oil cannot be used. Accordingly, stainless steel bearings are used without applying rust preventive oil. A low particle emission type lubricant should be used for these bearings.

Fig. 3-1 shows an EXSEV Bearing selection chart on the basis of the cleanliness class and temperature of the environment. In this chart, each numerical value has a margin.

The amounts of particle emissions from bearings differ depending on operating conditions such as temperature, load and rotational speed. Please consult JTEKT for applications who's operating conditions are near the bearing applicability divisions specified in Fig. 3-1.

Table 3-1 compares the particle emissions of various lubricants provided for major EXSEV Bearings.

For an unlubricated EXSEV Bearing, more than 3 million particles are found for every 20 hours. When silver or molybdenum disulfide is used as a lubricant, 10 000 or more particles are emitted, indicating that neither is suitable for clean environments.

Bearings using a fluorine polymer are low in particle emissions and suitable for use in clean environments.

Bearings lubricated with a Clean Pro coating or fluorinated grease are also useful in clean environments because they are low in particle emissions.

Fluorinated grease is superior to solid lubricants in load carrying capability and high speed operation. This grease can be used in applications where a slight amount of scattering of fluorinated oil is acceptable.

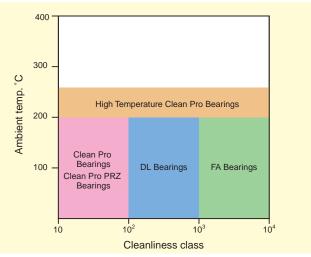
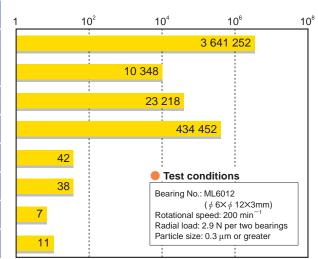


Fig. 3-1 EXSEV Bearings suitable for clean environments

■ Table 3-1 Particle emissions from major EXSEV Bearings

Bearing material composition		Lubrication		Number of emitted	
Bearing rings	Balls	Cage	Lubricated component	Lubricant	1 10 ²
SUS440C	SUS440C	SUS304		(None)	
	Silicon nitride	SUS304	_		
	SUS440C		Balls	Silver ion plating	
		SUS304	Cage	Baking of molybdenum disulfide	
			Cage	Baking of PTFE	42
		Fluorocarbon resin (FA)	Cage	Fluorine polymer	38
			Whole component surfaces	Clean Pro coating	7
		SUS304	_	Fluorinated grease	11





For the properties of the EXSEV Bearings shown in Fig. 3-1, refer to the pages listed below.

Cle

Fluorinated grease

DL Bearings ------37

olymeric materials
ean Pro Bearings·····31
gh Temperature Clean Pro Bearings33
ean Pro PRZ Bearings ······35
Bearings ······39

to Select EXSEV

3-2 Vacuum Environments

Bearing materials

Outer/inner rings and balls of the bearings for use in a vacuum environment are usually made of martensitic stainless steel (SUS440C). For the bearings requiring corrosion resistance, precipitation hardening stainless steel (SUS630) is used. When high temperature resistance is required, high speed tool steel (SKH4, M50, etc.) can be used. For a special operating condition, ceramic having excellent heat/corrosion resistance may be used.

Lubricants

A bearing used in an ordinary vacuum chamber is repeatedly exposed to atmospheric air and vacuum. There is no rolling bearing lubricant that is effective for use under such a wide pressure range. The lubricant should optimally be selected in consideration of principal ambient pressure and temperature as well as required cleanliness and corrosion resistance when necessary.

1) When cleanliness is not critical:

Fig. 3-2 shows the EXSEV Bearings that are suitable for vacuum applications that do not require cleanliness.

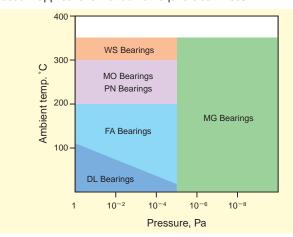


Fig. 3-2 EXSEV Bearings useful for vacuum applications where cleanliness is not critical

When the ambient temperature is near normal room temperature and vacuum is 10⁻⁵ Pa or less, fluorinated grease is used for lubrication. However, since the fluorinated oil contained in the grease gradually begins to evaporates, a solid lubricant should be used in applications where oil scattering should not occur.

In an ultrahigh vacuum environment with pressure lower than 10⁻⁵ Pa, gas emissions from bearings may pose a problem. For this pressure range, MG Bearings lubricated with silver, a soft metal lubricant, should be used.

2) When cleanliness is critical:

When bearings should be clean, solid lubricants such as soft metal materials and layer lattice materials cannot be used because of excessive particle emissions. In such a case, a polymeric material or fluorinated grease is used.

Figs. 3-3 and 3-4 show the EXSEV Bearings applicable for vacuum environments with cleanliness classes 100 and 10,

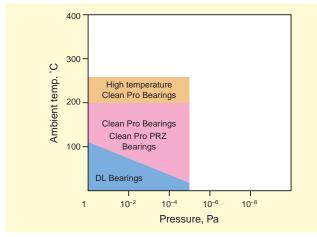


Fig. 3-3 EXSEV Bearings applicable for cleanliness class 100

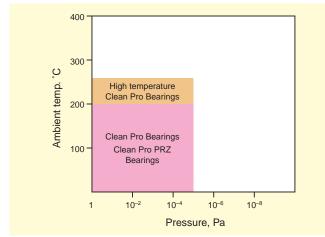


Fig. 3-4 EXSEV Bearings applicable for cleanliness class 10

3-3 High Temperature Environments

Bearing materials

Fig. 3-5 shows bearing materials for high temperature applications.

SUS440C can withstand temperatures up to approximately 300°C.

In the range from 300°C to approximately 500°C, High Temperature Hybrid Ceramic Bearings, whose bearing rings are made of highly heat resistant high speed tool steel (SKH4 or M50) and rolling elements made of ceramic, should be used.

In a high temperature environment in excess of 500°C, full ceramic bearings should be used.

Lubricants

Fig. 3-5 shows lubricants for high temperature applications. In a temperature range of up to approximately 200°C, fluorinated grease can be used. At temperatures over 200°C, a layer lattice material should be used.

Because all laver lattice materials emit a large amount of particles, they are not suitable for applications where cleanliness is required. Graphite cannot be used in a vacuum environment because it does not serve as a lubricant in a vacuum.

In a high temperature environment over 500°C, there is no lubricant that can work perfectly. Unlubricated full ceramic bearings are used for such a high temperature application.

Fig. 3-6 shows the EXSEV Bearings useful for high temperature applications.

The temperatures shown in the figure are approximate. When the operating temperature of your application is near a temperature division specified in this figure, consult JTEKT.

If a bearing is exposed to a high temperature in a clean or vacuum environment, please refer to the sections entitled "Clean Environments" or "Vacuum Environments".

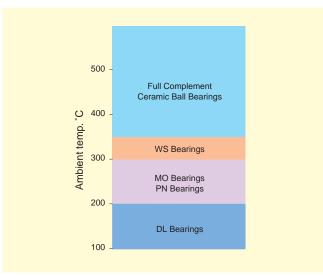


Fig. 3-6 EXSEV Bearing applicable for high temperature environments

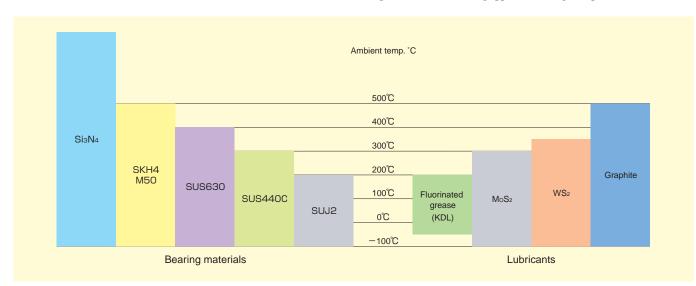


Fig. 3-5 Bearing materials and lubricants for high temperature applications

For the properties of the individual EXSEV Bearings shown in the figures, refer to the applicable pages shown below:

Fluorinated grease	Polymeric materials	Layer lattice materials
DL Bearings ·····37	Clean Pro Bearings31	PN Bearings41
	High Temperature Clean Pro Bearings33	WS Bearings43
	Clean Pro PRZ Bearings35	MO Bearings ·····45
	FA Bearings ······39	

Soft metal materials	No lubrication
MG Bearings ······47	Full Complement Ceramic Ball Bearings ······48

to Select EXSEV Bearings

3-4 Corrosive Environments

1) Corrosion resistance of special steels

Table 3-2 shows the corrosion resistance of the special steels used for the EXSEV Bearings to major corrosive solutions.

In stainless steels, SUS630 is superior to SUS440C in corrosion resistance. However, in such a highly corrosive solution as an acid or alkaline solution, or if the solution must be kept free from rust, these special steels cannot be used.

2) Corrosion resistance of ceramic materials

Table 3-3 shows the corrosion resistance of ceramic materials. Silicon nitride, which is used as the standard material of the ceramic bearings, is excellent in corrosion resistance. However, it may develop corrosion in a highly corrosive chemical, a high temperature, or other highly corrosive ambient condition.

There are two types of ceramic corrosion: One is the corrosion of the alumina-yttria system sintering aid ($Al_2O_3 - Y_2O_3$), which is used to bake ceramic materials. To avoid this type of corrosion, corrosion resistant silicon nitride treated with a spinel sintering aid ($MgAl_2O_4$) should be used. Fig. 3-7 shows the mass reduction and bending strength deterioration of corrosion resistant silicon nitride dipped in an acid or alkaline solution for a given period of time.

The other type of corrosion is the corrosion of the silicon nitride itself. For use in a highly corrosive solution, bearings made of zirconia (ZrO₂) or silicon carbide (SiC) may be effective.

To select a ceramic bearing for use in a highly corrosive environment, its corrosion resistance to the specific condition should be carefully examined.

■ Table 3-2 Corrosion resistance of special steels and materials for cages

			Ste	els			Materials f	or cages
Solution	Concentration	Martensitic stainless steel SUS 440C	Precipitation hardening stainless steel SUS 630	Austenitic stainless steel SUS 304	High carbon chromium bearing steel SUJ 2	Concentration	Fluorocarbon resin FA	PEEK resin PN
Water	_	0	0	0	×	_	Good	Good
Hydrochloric	1%	Δ	0	0	×	5%	% Good	Good
acid	10%	×	×	×	×	5%		Cood
Sulfuric acid	1%	0	0	0	×	5%	Good	Good
Sullulle acid	10%	Δ	0	0	×	3%	Good	Good
Nitric acid	20%	0	0	0	×	25%	Good	_
Caustic soda	5%	0	0	0	Δ	5%	Good	Good
Seawater	_	0	0	0	×	_	Good	Good

Temperature 25°C Corrosion rate $\mathbb O$: Up to 0.125 mm/year

○ : Over 0.125 to 0.5 mm/year

 \triangle : Over 0.5 to 1.25 mm/year

X: Over 1.25 mm/year

● Table 3-3 Corrosion resistance of ceramic materials

②: Fully resistant○: Almost resistant△: Slightly susceptibleX: Susceptible

—. Signify susceptible X. Susceptible						
Ceramic materials Corrosive solutions	Silicon nitride (standard) Si ₃ N ₄	Corrosion resistant silicon nitride Si ₃ N ₄	Zirconia ZrO ₂	Silicon Carbide SiC		
Hydrochloric acid	Δ	0	0	0		
Nitric acid	Δ	0	0	0		
Sulfuric acid	Δ	0	0	0		
Phosphoric acid	0	0	\circ	0		
Fluorine acid	Δ	Δ	×	0		
Sodium hydroxide	Δ	Δ	0	Δ		
Potassium hydroxide	Δ	Δ	Δ	Δ		
Sodium carbonate	Δ	Δ	\triangle	Δ		
Sodium nitrate	Δ	Δ	Δ	Δ		
Water and saltwater	0	0	0	0		

Note) The corrosive natures of individual solutions differ largely depending on the concentration and temperature. Note that mixing two or more chemicals may increase the corrosivity.

Standard Corrosion resistant

Standard Corrosion Standard Corrosion resistant

Fig. 3-7 Anticorrosive performance of corrosion resistant silicon nitride

3) Service life of corrosion resistant bearings

Table 3-4 lists the bearings suitable for applications requiring corrosion resistance, along with their major applications.

● Table 3-4 Typical corrosion resistant EXSEV Bearings

	Applications	Bearing l	Materials	Page
	Applications	Bearing Rings	Balls	raye
Corrosion Resistant Hybrid Ceramic Bearing	In water, alkaline environment and reactive gas	SUS630	Silicon nitride	53
Ceramic Bearing	In a slightly acidic environment, alkaline environment and reactive gas	Silicon nitride	Silicon nitride	55
Corrosion Resistant Ceramic Bearing	In a strongly acidic environment, strongly alkaline environment and reactive gas	Corrosion resistant silicon nitride	Corrosion resistant silicon nitride	57
High Corrosion Resistant Ceramic Bearing	In a strongly acidic environment, strongly alkaline environment and corrosive gas	Silicon carbide	Silicon carbide	59

When EXSEV Bearings are operated in a solution, the solution serves as a lubricant. This means the solution is closely associated with the service life of the bearings. Fig. 3-8 shows the service life evaluation results for three types of EXSEV Bearings under water.

The Ceramic Bearings terminate their service life due to the flaking on the bearing ring or ball surfaces.

In case of the Hybrid Ceramic Bearings, ceramic balls do not develop flaking or wear. Their service life ends due to wear attributed to the minute corrosion of stainless steel bearing rings.

When bearings are used in a solution whose lubrication performance is not enough, such as in water, it is important to evaluate in advance the susceptibility of the bearings to corrosion and the relationship between the bearing load and wear in the solution.

SUS440C has a longer service life than SUS630; however, the former steel is not suitable for use in water because it may rust and cause contamination.

Ceramic Bearings may develop wear at an early stage of use depending on the characteristics of the solution, temperature, and load. Please contact JTEKT before using Ceramic Bearings in solutions.

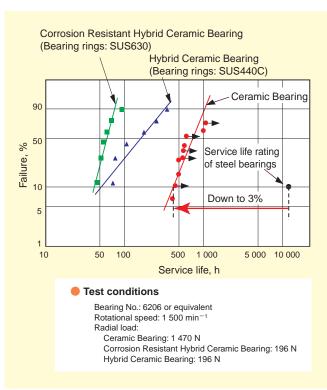


Fig. 3-8 Comparison in underwater service life of EXSEV Bearings

Koyo

4 EXSEV Bearings with Special Characteristics

4-1 Non-magnetic Bearings

Bearings may be exposed to magnetic fields in some applications, including equipment associated with super conductivity, semiconductor production facilities and medical examination facililies. If steel bearings are used for such applications, the running torque may fluctuate or the magnetic field may be disturbed . Non-magnetic bearings should be used for such applications. As a non-magnetic material for such bearings, beryllium copper has conventionally been used. However the use of beryllium copper should be avoided since it contains beryllium, a substance of environmental concern.

For such applications, JTEKT supplies Hybrid Ceramic Bearings, whose rings are made of non-magnetic stainless steel and rolling elements are made of a ceramic material, or the full ceramic bearings.

● Table 4-1 Non-magnetic bearings and relative permeability

	Relative permeability	Page
Non-magnetic Hybrid Ceramic Bearings	1.01 or lower	61
Ceramic Bearings	1.001 or lower	55
(Ref.) Beryllium copper	1.001 or lower	

Fig. 4-1 shows a rolling fatigue strength evaluation result for various non-magnetic materials. As can be seen from the figure, non-magnetic stainless steel is superior to beryllium copper in rolling fatigue strength.

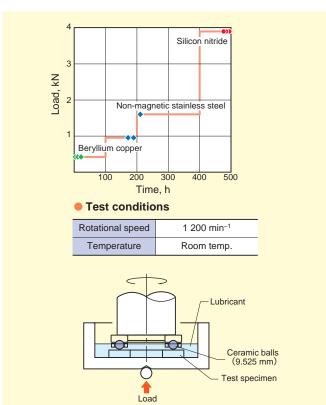


Fig. 4-1 Comparison of non-magnetic materials in rolling fatigue strength

4-2 Insulating Bearings

A cause of bearing failure in motors or generators is electric pitting. Electric pitting occurs when a surface in rolling contact is locally molten due to sparks produced over the very thin lubricating oil film on the surface when electricity passes through the bearing in operation.

Electric pitting appears as a series of pits or a series of ridges on the surface in rolling contact, which is shown in Fig. 4-2 and Fig. 4-3.

An estimation of the mechanism that causes electric pitting on a bearing is shown in Fig. 4-4.



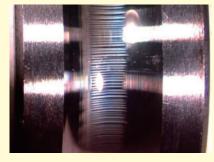
Fig. 4-2 Electric pitting generated on general purpose bearings (pits)



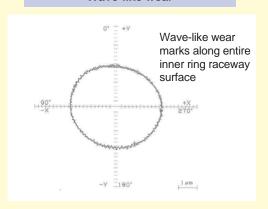
Fig. 4-3 Electric pitting generated on general purpose bearings (ridges)

Continuous sparks of weak current

Example of electric pitting on inner ring raceway surface



Wave-like wear



Estimation of the wave-like wear occurrence mechanism

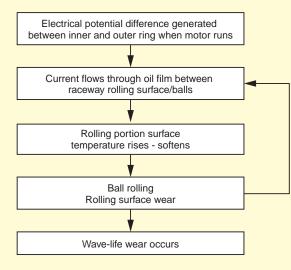


Fig. 4-4 Estimation of electric pitting (wave-like wear) occurrence mechanism

To avoid such pitting, a bypass is provided to ensure that no electric current passes through the bearing. Another method is to use an insulating bearing that can block electric current.

Since ceramic materials exhibit an excellent insulation performance, Hybrid Ceramic Bearings consisting of ceramic rolling elements can be used as insulating bearings. (Fig.4-5)

Hybrid Ceramic Bearings prevent electric pitting, also reduce bearing temperature rise, and lengthen grease service life. For these reasons, Hybrid Ceramic Bearings assure long term maintenance free operation and high speed equipment operation.



Fig. 4-5 Insulating bearings (Hybrid Ceramic Bearings)

4-3 High Speed Bearings

Hybrid Ceramic Bearings, whose rolling elements are made of a ceramic material with a density lower than that of bearing steel, are most suitable for high speed applications. This is because reduced mass of rolling elements suppresses the centrifugal force of the rolling elements, as well as slippage attributable to the gyro-moment, when the bearings are in operation.

Thanks to their superior high speed performance, Hybrid Ceramic Bearings are used in turbochargers and on machine tool spindles.

Power losses at high speed

Fig. 4-6 compares power losses between the Hybrid Ceramic Bearings and steel bearings.

When compared to steel bearings, the Hybrid Ceramic Bearings lose smaller power during high speed operation. The power loss decreases with increasing rotational speed.

The Hybrid Ceramic Bearings also have superior antiseizure characteristics, which means that they consume smaller amount of lubrication oil and thereby reduce rolling resistance (power loss).

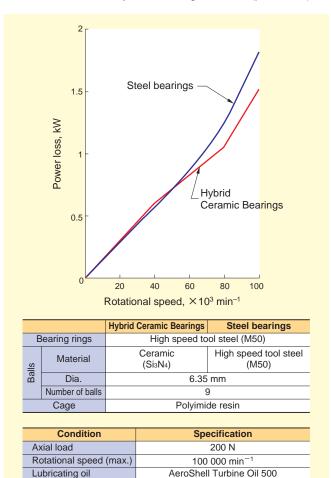


Fig. 4-6 Comparison in power loss between Hybrid Ceramic Bearings and steel bearings

Seizure limit at high speed

Fig. 4-7 shows the seizure limits of Hybrid Ceramic Bearings and steel bearings. The limits were measured by gradually reducing lubricating oil feed rate.

Compared with general purpose steel bearings, Hybrid Ceramic Bearings consume smaller amount of lubricating oil under the same speed condition, while they can run at a higher speed under the same luburicating oil feed rate condition.

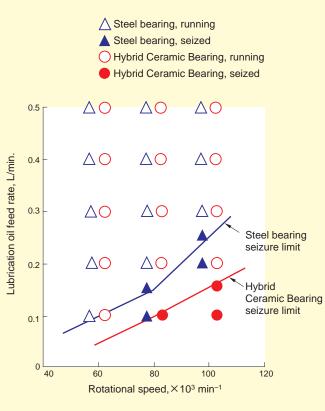


Fig. 4-7 Comparison between Hybrid Ceramic Bearings and steel bearings in seizure limit

Ambient temperature

EXSEV Bearings and Other **EXSEV** Products

For the use of bearings in an extreme, special environment, identifying the best combination of bearing materials and lubricants according to specific conditions is critical.

This chapter describes the component compositions and features of major EXSEV Bearing varieties.

For other EXSEV Bearings suited to more specialized applications, please consult JTEKT.



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	,	

Ceramic Bearings and EXSEV Bearings: Table of Specifications

Ceramic Bearings and **EXSEV** Bearings: Table of Specifications

ı	Products	SK Bearing	Clean Pro Bearing	High Temperature Clean Pro Bearing	Clean Pro PRZ Bearing	DL Bearing	FA Bearing	PN Bearing	MO Bearing	WS Bearing	MG Bearing	Full Compleme Ceramic Ball Bea (angular contact ball be	ing Hybrid Coromic Boorin	Ceramic Bearing	Corrosion Resistant Ceramic Bearing	High Corrosion Resistance Ceramic Bearing	Non-magnetic Hybrid Ceramic Bearing	Hybrid Ceramic Bearing	K Series Full Complement Hybrid Ceramic Ball Bearing
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Š.	Prefix	SK	SE	SE	SE	sv	SE	SE	SE	SE	SE	NC	3NC	NC	NCT	NCZ	ЗNС	ЗNС	SNC
ing	Suffix	ZZST	ZZSTPR	ZZSTPRB	ZZSTPRZ	ZZST	ZZST	ZZST	ZZSTMSA7	ZZST	ZZSTMG3	V	ZZMD4	(None)	(None)	(None)	YH4	ZZ	VST-1
Bear	Cage code	YS	YS	YS	YS	YS	FA	PN	YS	ws	YS	(No cage)	FA	FA	FA	FA	FA	FG	(No cage)
Oı	uter ring					Martensitic s	tainless steel					Silicon nitrid ceramic (standard)	Precipitation hardening stainless steel	Silicon nitride ceramic (standard)	Silicon nitride ceramic (corrosion resistant)	Silicon carbide ceramic	Non-magnetic stainless steel	High carbon chromium bearing steel	Martensitic stainless steel
ln	ner ring					Martensitic s	tainless steel					Silicon nitrid ceramic (standard)	Precipitation hardening stainless steel	Silicon nitride ceramic (standard)	Silicon nitride ceramic (corrosion resistant)	Silicon carbide ceramic	Non-magnetic stainless steel	High carbon chromium bearing steel	Martensitic stainless steel
	Rolling ements					Martensitic s	tainless steel					s	con nitride ceramic (s	tandard)	Silicon nitride ceramic (corrosion resistant)	Silicon carbide ceramic	Silicor	n nitride ceramic (sta	ndard)
C se	age or parator		Aust	enitic stainless	steel		Fluorocarbon resin	PEEK resin	Austenitic stainless steel	(separator) Composite material including tungsten disulfide	Austenitic stainless steel	(None)			Fluorocarbon resin			Reinforced polyamide resin	(separators) Martensitic stainless steel
;	Shield					Austenitic s	ainless steel					(None)	Austenitic stainless steel		(No	one)		Carbon steel	(None)
cation	Lubricant	KHD	Clean pro coating	High temperature clean pro coating	Clean pro PRZ coating	KDL	Fluorocarbon polymer	Molybdenum disulfide, etc.	Molybdenum disulfide	Tungsten disulfide	Silver	(None)		Fluorocart	oon polymer		Fluorocarbon polymer	Grease or oil	KDL grease
Lubrio	Component coated with or including lubricant	grease	Entire surface of all components		s and balls	grease		Cage		Separators	Balls	(NOILE)			Cage			Grease of on	NDL grouse
				Cle	ean environme	nts									Clean environments				Clean environments
						Vac	cuum environm	ents						Vacuum e	nvironments				Vacuum environments
		Corrosive environments												Corrosive e	environments				2
Ap	plicable ronments			High temperature				F	l High temperatur	e environmen	ts	High temperat							
CIIV	Juliuents			environments								Magnetic fiel environment			Magnetic field	environments			
												environment		El	ectric field environme				
																		High speed applications	
																		applications	

2 Ceramic Bearings and EXSEV Bearings: Table of Characteristics (1)

					Applicable	Environ	ments										_ ,				
Majo	r Uses	Products	Limiting	Speeds		Op	perating Temp. (°	C)				Vacuum	(Pa)	Clear	nliness (cla	ass) ²⁾	Performance and	Bearing Number 3)	(Cage Code)	Corresponding Catalog Pages	Available
			dn value 1)	Max. (min ⁻¹)	< 120 < 200	< 260	< 300 < 350	< 400	< 500	< 800	Atmosphe air	ric 10 ⁻⁵	10-10	10	100	1000	Functions				from Stock
		FA Bearing	< 10 000	1 000												•	Low	SE	(FA)	39-40	0
		DL Bearing	< 40 000	-											•			SV	(YS)	37-38	
		Clean Pro Bearing	< 10 000	1 000										•				SE	(YS)	31-32	0
	Vacuum	High Temperature Clean Pro Bearing	< 10 000	1 000										•				SE	(YS)	33-34	
	environment	Clean Pro PRZ Bearing	< 10 000	1 000										•				SE	(YS)	35-36	
		Corrosion Resistant Hybrid Ceramic Bearing	< 10 000	1 000												•		3NC ZZMD4	(FA)	53-54	0
		Non-magnetic Hybrid Ceramic Bearing	< 10 000	1 000												•		3NC DDDYH4	(FA)	61-62	
		Ceramic Bearing	< 10 000	1 000												•	High	NC	(FA)	55-56	0
Clean		Corrosion Resistant Hybrid Ceramic Bearing	< 10 000	1 000												•	Low	3NC ZZMD4	(FA)	53-54	0
environment	Corrosive	Ceramic Bearing	< 10 000	1 000												•		NC DDD	(FA)	55-56	0
	environment	Corrosion Resistant Ceramic Bearing	< 10 000	1 000												•		NCT	(FA)	57-58	0
		High Corrosion Resistant Ceramic Bearing	< 10 000	1 000												•	High	NCZ	(FA)	59-60	
	High temperature environment	High Temperature Clean Pro Bearing	< 10 000	1 000										•				SE ZZSTPRB	(YS)	33-34	
	Magnetic field environment	Non-magnetic Hybrid Ceramic Bearing	< 10 000	1 000												•	Low	3NC□□□□YH4	(FA)	61-62	
			< 10 000	1 000												•	High	NC	(FA)	55-56	0
	Electric field	Corrosion Resistant Hybrid Ceramic Bearing	< 10 000	1 000												•	Low	3NC ZZMD4	(FA)	53-54	0
		Non-magnetic Hybrid Ceramic Bearing	< 10 000	1 000												•		3NC□□□□YH4	(FA)	61-62	
		Ceramic Bearing	< 10 000	1 000												•	High	NC	(FA)	55-56	0
		FA Bearing	< 10 000	1 000												•	Low	SE ZZST	(FA)	39-40	0
		DL Bearing	< 40 000	-											•			SV□□□□ZZST	(YS)	37-38	
		PN Bearing	< 10 000	1 000														SE	(PN)	41-42	0
		Clean Pro Bearing	< 10 000	1 000										•				SE ZZSTPR	(YS)	31-32	0
		MO Bearing	< 10 000	1 000														SE ZZSTMSA7	(YS)	45-46	
		MG Bearing	< 10 000	1 000							Cannot bused under	he						SE ZZSTMG3	(YS)	47-48	0
		High Temperature Clean Pro Bearing	< 10 000	1 000							atmospher	9.		•				SE ZZSTPRB	(YS)	33-34	
Vacuum e	nvironment	Clean Pro PRZ Bearing	< 10 000	1 000										•				SE ZZSTPRZ	(YS)	35-36	
		WS Bearing	< 4 000	500														SE ZZST	(WS)	43-44	0
		Corrosion Resistant Hybrid Ceramic Bearing	< 10 000	1 000												•		3NC ZZMD4	(FA)	53-54	0
		Non-magnetic Hybrid Ceramic Bearing	< 10 000	1 000												•		3NC□□□□YH4	(FA)	61-62	
		Ceramic Bearing Ceramic Bearing	< 10 000	1 000														NC DDD	(FA)	55-56	0
		Corrosion Resistant Ceramic	< 10 000	1 000												•		NCT	(FA)	57-58	0
		Bearing High Corrosion Resistance	< 10 000	1 000												•	High	NCZ	(FA)	59-60	
1) dayalını D		Ceramic Bearing													on operating				(. 7)		

¹⁾ *dn* value: Bearing bore diameter (mm) × Rotational speed (min⁻¹)

²⁾ The cleanliness classes may vary depending on operating conditions.

³⁾ The four blank boxes represent the basic number of the bearing. A basic number consists of three or four alphanumeric characters. A bearing number may be used as a convenience in the case of any queries to JTEKT.

Ceramic Bearings and **EXSEV** Bearings: Table of Characteristics (2)

				Ар	plicable	Environm	nents											Denfermen				Llaa Cia
Major Uses	Products	Limiting	Speeds			Оре	erating ⁻	Temp. (°C)			Va	acuum (Pa	a)	Clear	nliness (cla	ss) ²⁾	Performance and	Bearing Number 3)	(Cage Code)	Corresponding Catalog Pages	Available
		dn value 1)	Max. (min ⁻¹)	< 120	< 200	< 260	< 300	< 350	< 400	< 500	< 800	Atmospheric air	10-5	10-10	10	100	1000	Functions				from Stock
	SK Bearing	Equal to the dn value of normal bearings	1															Low	SK	(YS)	51-52	0
	Corrosion Resistant Hybrid Ceramic Bearing	< 10 000	1 000														•		3NC ZZMD4	(FA)	53-54	0
	Ceramic Bearing	< 10 000	1 000														•		NC	(FA)	55-56	0
Corrosive environment	Full Complement Ceramic Ball Bearing	< 4 000	500																NC	(-)	49-50	
	Corrosion Resistant Ceramic Bearing	< 10 000	1 000														•		NCT	(FA)	57-58	0
	High Corrosion Resistance Ceramic Bearing	< 10 000	1 000														•	High	NCZ	(FA)	59-60	
	PN Bearing	< 10 000	1 000															Low	SE	(PN)	41-42	0
	MO Bearing	< 10 000	1 000																SE ZZSTMSA7	(YS)	45-46	
High temperature	MG Bearing	< 10 000	1 000																SE ZZSTMG3	(YS)	47-48	0
environment	High Temperature Clean Pro Bearing	< 10 000	1 000												•				SE ZZSTPRB	(YS)	33-34	
	WS Bearing	< 4 000	500																SE ZZST	(WS)	43-44	0
	Full Complement Ceramic Ball Bearing	< 4 000	500															High	NC	(-)	49-50	
	Non-magnetic Hybrid Ceramic Bearing	< 10 000	1 000														•	Low	3NC YH4	(FA)	61-62	
	Ceramic Bearing	< 10 000	1 000														•		NC	(FA)	55-56	0
Magnetic field environment	Full Complement Ceramic Ball Bearing	< 4 000	500																NC	(-)	49-50	
Givinoriii	Corrosion Resistant Ceramic Bearing	< 10 000	1 000														•		NCT	(FA)	57-58	0
	High Corrosion Resistance Ceramic Bearing	< 10 000	1 000														•	High	NCZ	(FA)	59-60	
	Hybrid Ceramic Bearing	No less than 1.2 times that of steel bearings	1															Low	3NC D ZZ	(FG)	63-64	0
	Corrosion Resistant Hybrid Ceramic Bearing	< 10 000	1 000														•		3NC ZZMD4	(FA)	53-54	0
	Non-magnetic Hybrid Ceramic Bearing	< 10 000	1 000														•		3NC DDDYH4	(FA)	61-62	
Electric field environment	Ceramic Bearing	< 10 000	1 000														•		NC	(FA)	55-56	0
	Full Complement Ceramic Ball Bearing	< 4 000	500																NCDDDV	(-)	49-50	
	Corrosion Resistant Ceramic Bearing	< 10 000	1 000														•		NCT	(FA)	57-58	0
	High Corrosion Resistance Ceramic Bearing	< 10 000	1 000														•	High	NCZ 🗆 🗆 🗆	(FA)	59-60	
High speed application	Hybrid Ceramic Bearing	No less than 1.2 times that of steel bearings	 																3NC ZZ	(FG)	63-64	0

¹⁾ dn value: Bearing bore diameter (mm) × Rotational speed (min⁻¹)

²⁾ The cleanliness classes may vary depending on operating conditions.

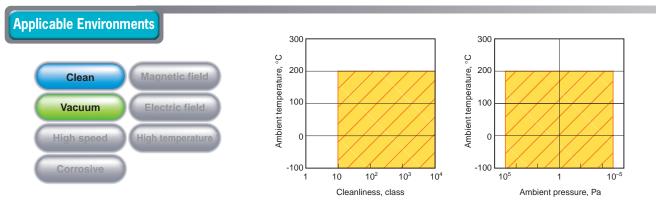
³⁾ The four blank boxes represent the basic number of the bearing. A basic number consists of three or four alphanumeric characters. A bearing number may be used as a convenience in the case of any queries to JTEKT.

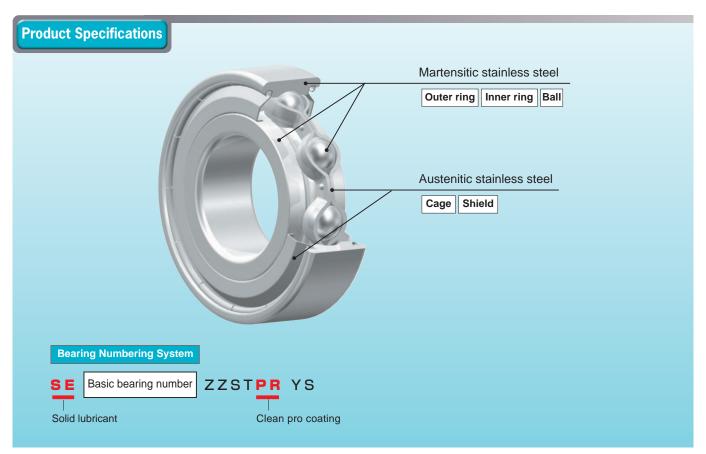
3 Radial Ball Bearings

Clean Pro Bearings

For Clean Rooms, Vacuum Equipment

This bearing is lubricated with a fluoropolymer coating over the entire surface of all bearing components.



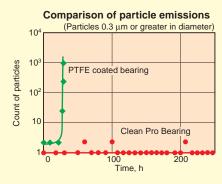


Applications

- Semiconductor manufacturing equipment LCD manufacturing equipment Vacuum equipment
- Lithography equipment
 Sputtering equipment
 Vacuum motors

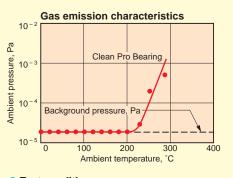
Performance

 Suitable for use in clean environments due to low particle emissions.



Test conditions

Bearing No.: 608 Temperature: Atmosphere / room temperature Rotational speed: 200min⁻¹, Load: Axial 20 N • Stable performance up to 200°C in a vacuum.



Test conditions

Bearing No.: 608

Lubricant service life expectancy equation

The average service life of clean pro coated bearings can be estimated by the following equation:

$$L_{\text{av}} = b_2 \cdot \left(\frac{C_{\text{r}} \times 0.85}{P_{\text{r}}} \right)^q \times 0.016667/n$$

 L_{av} : Average life, h b₂ : Lubrication factor

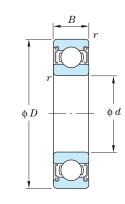
 $b_2 = 42$: Basic dynamic load rating, N

: Dynamic equivalent radial load, N : Exponential coefficient, q = 3

: Rotational speed, min-1

For the service life of solid lubricants, refer to page 13.

Dimensions Table



Dynamic equivalent load $P_{\rm r} = XF_{\rm r} + YF_{\rm a}$

 $P_{0r} = 0.6F_r + 0.5F_a$

(X and Y are as shown below.) Static equivalent load

 $P_{0r} = F_r$

f_0F_a	e	$\frac{F_{ m a}}{F_{ m r}}$	≤ <i>e</i>	$\frac{F_{\rm a}}{F_{\rm r}} > e$				
$C_{0\mathrm{r}}$		X	Y	X	Y			
0.172 0.345 0.689	0.19 0.22 0.26				2.30 1.99 1.71			
1.03 1.38 2.07	0.28 0.30 0.34	1	0	0.56	1.55 1.45 1.31			
3.45 5.17 6.89	0.38 0.42 0.44				1.15 1.04 1.00			

* Colors in the "Bearing No." column indicate the classification of the periods for delivery as shown below

Available from stock 30 days after receiving an order 45 days after receiving an order

Determined after consultation on each inquiry

	Воц	ındary d mr			Bearing No.	Basic load kN		Factor	Permissible radial load	Limiting speed
	d	D	B	r (min.)		$C_{ m r}$	$C_{0\mathrm{r}}$	f_0	N	min ⁻¹
	4	12	4	0.2	SE604ZZSTPRC3 YS	0.97	0.36	12.4	30	1 000
		13	5	0.2	SE624ZZSTPRC3 YS	1.30	0.49	12.3	40	1 000
	5	14	5	0.2	SE605ZZSTPRC3 YS	1.30	0.49	12.3	40	1 000
		16	5	0.3	SE625-5ZZSTPRC3 YS	1.75	0.67	12.4	55	1 000
	6	17	6	0.3	SE606ZZSTPRC3 YS	1.95	0.74	12.2	60	1 000
		19	6	0.3	SE626ZZSTPRC3 YS	2.60	1.05	12.3	80	1 000
	7	19	6	0.3	SE607ZZSTPRC3 YS	2.60	1.05	12.3	80	1 000
		22	7	0.3	SE627ZZSTPRC3 YS	3.30	1.35	12.4	100	1 000
	8	22	7	0.3	SE608ZZSTPRC3 YS	3.30	1.35	12.4	100	1 000
		24	8	0.3	SE628ZZSTPRC3 YS	3.35	1.40	12.8	100	1 000
	9	24	7	0.3	SE609ZZSTPRC3 YS	3.35	1.40	12.8	100	1 000
		26	8	0.6	SE629ZZSTPRC3 YS	4.55	1.95	12.4	135	970
	9.525	22.225	7.142	0.5	SEEE3SZZSTPRC3 YS	3.35	1.40	12.8	100	1 000
	10	26	8	0.3	SE6000ZZSTPRC3 YS	4.55	1.95	12.3	135	1 000
		30	9	0.6	SE6200ZZSTPRC3 YS	5.10	2.40	13.2	155	860
	12	28	8	0.3	SE6001ZZSTPRC3 YS	5.10	2.40	13.2	155	830
		32	10	0.6	SE6201ZZSTPRC3 YS	6.80	3.05	12.3	205	770
	15	32	9	0.3	SE6002ZZSTPRC3 YS	5.60	2.85	13.9	170	660
		35	11	0.6	SE6202ZZSTPRC3 YS	7.65	3.75	13.2	230	610
	17	35	10	0.3	SE6003ZZSTPRC3 YS	6.00	3.25	14.4	180	580
		40	12	0.6	SE6203ZZSTPRC3 YS	9.55	4.80	13.2	285	530
	20	42	12	0.6	SE6004ZZSTPRC3 YS	9.40	5.05	13.9	280	500
		47	14	1	SE6204ZZSTPRC3 YS	12.8	6.65	13.2	385	450
	25	47	12	0.6	SE6005ZZSTPRC3 YS	10.1	5.85	14.5	305	400
		52	15	1	SE6205ZZSTPRC3 YS	14.0	7.85	13.9	420	360
	30	55	13	1	SE6006ZZSTPRC3 YS	13.2	8.25	14.7	395	330
		62	16	1	SE6206ZZSTPRC3 YS	19.5	11.3	13.9	585	300
	35	62	14	1	SE6007ZZSTPRC3 YS	15.9	10.3	14.9	475	280
		72	17	1.1	SE6207ZZSTPRC3 YS	25.7	15.4	13.9	770	250
<i>/</i> .	40	68	15	1	SE6008ZZSTPRC3 YS	16.7	11.5	15.2	500	250
		80	18	1.1	SE6208ZZSTPRC3 YS	29.1	17.8	14.0	875	220
	Notes 1)	The basic	load ratir	ngs are th	nose of normal bearing (used t	o calculate	lubricatio	n life).		

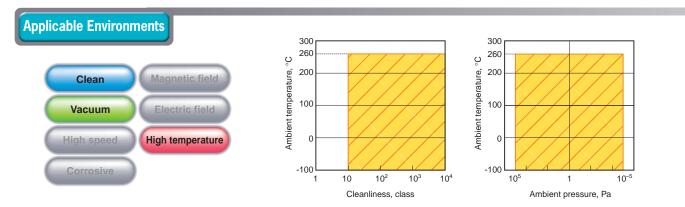
2) The permissible radial loads can be regarded as the maximum loads applicable to individual bearings. When an axial load is applied to the bearing, convert this axial load to a dynamic equivalent radial load, and then compare this value to the permissible radial load.

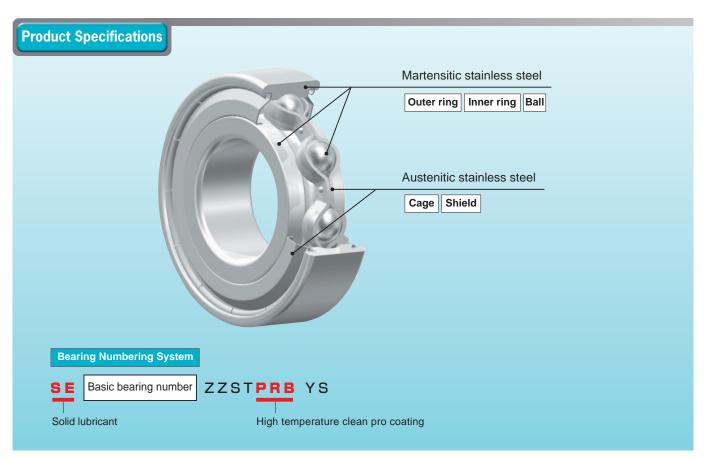
[Remark] When other sizes are used, consult with JTEKT.

High Temperature Clean Pro Bearings

Supports 260°C Clean, Vacuum Environments

This bearing has a fluoropolymer coating on its rolling surface as the lubricant.



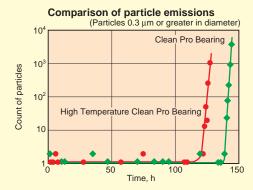


Applications

- Semiconductor manufacturing equipment LCD manufacturing equipment Transfer systems
- Vacuum equipment
 Sputtering equipment

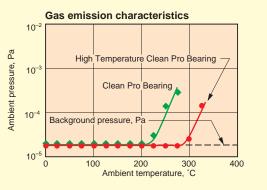
Performance

 Comparable to the Clean Pro Bearing in low particle emissions.



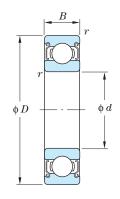
Test conditions

Bearing No.: 608 Temperature: Atmosphere / room temperature Rotational speed: 200min⁻¹, Load: Axial 100 N Compatible with temperatures of up to 260°C in a vacuum.



Test conditions Bearing No.: 608

Dimensions Table



Dynamic equivalent load $P_r = XF_r + YF_a$ (X and Y are as shown below.) Static equivalent load $P_{0r} = 0.6F_r + 0.5F_a$ When P_{0r} is smaller than F_r .

f_0F_a	e	$\frac{F_{ m a}}{F_{ m r}}$	· ≤ <i>e</i>	$\frac{F_{\rm a}}{F_{\rm r}} > e$			
C_{0r}		X	Y	X	Y		
0.172 0.345 0.689	0.19 0.22 0.26				2.30 1.99 1.71		
1.03 1.38 2.07	0.28 0.30 0.34	1	0	0.56	1.55 1.45 1.31		
3.45 5.17 6.89	0.38 0.42 0.44				1.15 1.04 1.00		

* Colors in the "Bearing No." column indicate the classification of the periods for delivery as shown below.

Available from stock

	30 days after receiving an order
	45 days after receiving an order
	Determined after consultation on each in

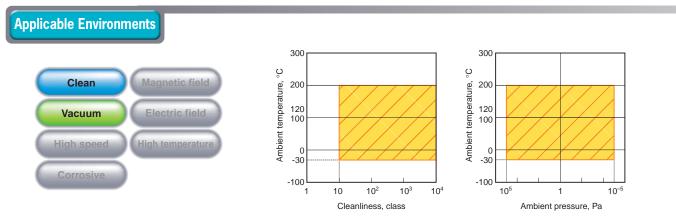
Бои	ndary d mr		ons	Bearing No.	Factor	Permissible radial load	Limiting speed
d	D	В	$r \pmod{n}$		f_0	N	min ⁻¹
4	12	4	0.2	SE604ZZSTPRBC3 YS	12.4	30	1 000
	13	5	0.2	SE624ZZSTPRBC3 YS	12.3	40	1 000
5	14	5	0.2	SE605ZZSTPRBC3 YS	12.3	40	1 000
	16	5	0.3	SE625-5ZZSTPRBC3 YS	12.4	55	1 000
6	17	6	0.3	SE606ZZSTPRBC3 YS	12.2	60	1 000
	19	6	0.3	SE626ZZSTPRBC3 YS	12.3	80	1 000
7	19	6	0.3	SE607ZZSTPRBC3 YS	12.3	80	1 000
	22	7	0.3	SE627ZZSTPRBC3 YS	12.4	100	1 000
8	22	7	0.3	SE608ZZSTPRBC3 YS	12.4	100	1 000
	24	8	0.3	SE628ZZSTPRBC3 YS	12.8	100	1 000
9	24	7	0.3	SE609ZZSTPRBC3 YS	12.8	100	1 000
	26	8	0.6	SE629ZZSTPRBC3 YS	12.4	135	970
9.525	22.225	7.142	0.5	SEEE3SZZSTPRBC3 YS	12.8	100	1 000
10	26	8	0.3	SE6000ZZSTPRBC3 YS	12.3	135	1 000
	30	9	0.6	SE6200ZZSTPRBC3 YS	13.2	155	860
12	28	8	0.3	SE6001ZZSTPRBC3 YS	13.2	155	830
	32	10	0.6	SE6201ZZSTPRBC3 YS	12.3	205	770
15	32	9	0.3	SE6002ZZSTPRBC3 YS	13.9	170	660
	35	11	0.6	SE6202ZZSTPRBC3 YS	13.2	230	610
17	35	10	0.3	SE6003ZZSTPRBC3 YS	14.4	180	580
	40	12	0.6	SE6203ZZSTPRBC3 YS	13.2	285	530
20	42	12	0.6	SE6004ZZSTPRBC3 YS	13.9	280	500
	47	14	1	SE6204ZZSTPRBC3 YS	13.2	385	450
25	47	12	0.6	SE6005ZZSTPRBC3 YS	14.5	305	400
	52	15	1	SE6205ZZSTPRBC3 YS	13.9	420	360
30	55	13	1	SE6006ZZSTPRBC3 YS	14.7	395	330
	62	16	1	SE6206ZZSTPRBC3 YS	13.9	585	300
35	62	14	1	SE6007ZZSTPRBC3 YS	14.9	475	280
	72	17	1.1	SE6207ZZSTPRBC3 YS	13.9	770	250
40	68	15	1	SE6008ZZSTPRBC3 YS	15.2	500	250
	80	18	1.1	SE6208ZZSTPRBC3 YS	14.0	875	220

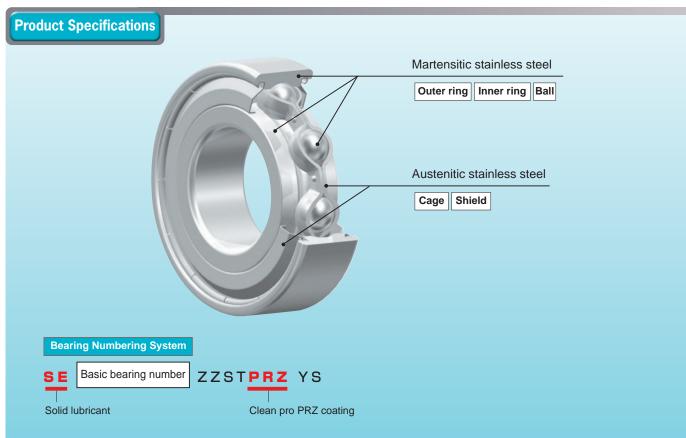
2) When other sizes are used, consult with JTEKT.

Clean Pro PRZ Bearings

10-times The Service Life of Clean Pro Bearings

This bearing has a fluoropolymer gel coating on its rolling surfaces as the lubricant.



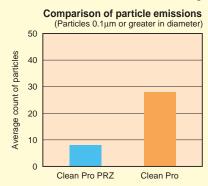


Applications

- Semiconductor manufacturing equipment Transfer systems Lithography equipment
- Vacuum motors
 Vacuum equipment

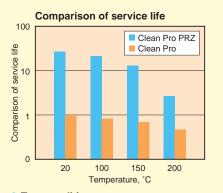
Performance

Clean Pro PRZ has better characteristics in low particle emissions than Clean Pro Bearings.



Test conditions

Bearing No.: 6000 Temperature: Atmosphere / room temperature Rotational speed: 200min⁻¹, Load: Axial 30 N Clean Pro PRZ has longer service life than Clean Pro Bearings.



Test conditions

Bearing No.: 6000, Rotational speed: 1200min⁻¹ Load: Axial 147 N, Atmosphere pressure: 10⁻³ Pa

 Clean Pro PRZ has better characteristics in low gas emission than Clean Pro Bearings.

Lubricant service life expectancy equation

The average service life of bearings with the Clean Pro PRZ coating can be estimated with the following equation.

$$L_{\rm av} = b_2 \cdot \left(\frac{C_{\rm r} \times 0.85}{P_{\rm r}} \right)^q \times 0.016667/n$$

Where,

: Average life, h b₂ : Lubrication factor

 $b_2 = 420$

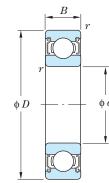
: Basic dynamic load rating, N

: Dynamic equivalent radial load, N : Exponential coefficient, q = 3

: Rotational speed, min-1

For the service life of solid lubricants, refer

Dimensions Table



Dynamic equivalent load

 $P_r = XF_r + YF_a$ (X and Y are as shown below.)

Static equivalent load

 $P_{0x} = 0.6F_x + 0.5F_0$

When P_{0r} is smaller than F_r .

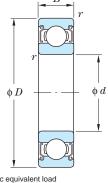
f_0F_a	e	$\frac{F_{ m a}}{F_{ m r}}$	≤ <i>e</i>	$\frac{F_{\rm a}}{F_{\rm r}} > e$				
$C_{0\mathrm{r}}$		X	Y	X	Y			
0.172 0.345 0.689	0.19 0.22 0.26				2.30 1.99 1.71			
1.03 1.38 2.07	0.28 0.30 0.34	1	0	0.56	1.55 1.45 1.31			
3.45 5.17 6.89	0.38 0.42 0.44				1.15 1.04 1.00			

 $\ensuremath{\mbox{\ensuremath{\$}}}$ Colors in the "Bearing No." column indicate the

Available from stock

30 days after receiving an order

Determined after consultation on each inquiry



classification of the periods for delivery as shown below.

45 days after receiving an order

Вои	indary d mr			Bearing No.	Factor	Permissible radial load ²⁾	Limiting speed
d	D	B	$r \pmod{1}$		f_0	N	min ⁻¹
5	14	5	0.2	SE605ZZSTPRZC3 YS	12.3	40	1 000
	16	5	0.3	SE625-5ZZSTPRZC3 YS	12.4	55	1 000
6	17	6	0.3	SE606ZZSTPRZC3 YS	12.2	60	1 000
	19	6	0.3	SE626ZZSTPRZC3 YS	12.3	80	1 000
7	19	6	0.3	SE607ZZSTPRZC3 YS	12.3	80	1 000
	22	7	0.3	SE627ZZSTPRZC3 YS	12.4	100	1 000
8	22	7	0.3	SE608ZZSTPRZC3 YS	12.4	100	1 000
	24	8	0.3	SE628ZZSTPRZC3 YS	12.8	100	1 000
9	24	7	0.3	SE609ZZSTPRZC3 YS	12.8	100	1 000
	26	8	0.6	SE629ZZSTPRZC3 YS	12.4	135	970
9.525	22.225	7.142	0.5	SEEE3SZZSTPRZC3 YS	12.8	100	1 000
10	26	8	0.3	SE6000ZZSTPRZC3 YS	12.3	135	1 000
	30	9	0.6	SE6200ZZSTPRZC3 YS	13.2	155	860
12	28	8	0.3	SE6001ZZSTPRZC3 YS	13.2	155	830
	32	10	0.6	SE6201ZZSTPRZC3 YS	12.3	205	770
15	32	9	0.3	SE6002ZZSTPRZC3 YS	13.9	170	660
	35	11	0.6	SE6202ZZSTPRZC3 YS	13.2	230	610
17	35	10	0.3	SE6003ZZSTPRZC3 YS	14.4	180	580
	40	12	0.6	SE6203ZZSTPRZC3 YS	13.2	285	530
20	42	12	0.6	SE6004ZZSTPRZC3 YS	13.9	280	500
	47	14	1	SE6204ZZSTPRZC3 YS	13.2	385	450
25	47	12	0.6	SE6005ZZSTPRZC3 YS	14.5	305	400
	52	15	1	SE6205ZZSTPRZC3 YS	13.9	420	360
30	55	13	1	SE6006ZZSTPRZC3 YS	14.7	395	330
	62	16	1	SE6206ZZSTPRZC3 YS	13.9	585	300
35	62	14	1	SE6007ZZSTPRZC3 YS	14.9	475	280
	72	17	1.1	SE6207ZZSTPRZC3 YS	13.9	770	250
40	68	15	1	SE6008ZZSTPRZC3 YS	15.2	500	250
	80	18	1.1	SE6208ZZSTPRZC3 YS	14.0	875	220

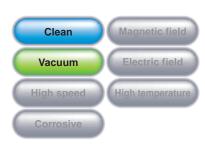
2) The permissible radial loads can be regarded as the maximum loads applicable to individual bearings. When an axial load is applied to the bearing, convert this axial load to a dynamic equivalent radial load, and then compare this value to the permissible radial load.

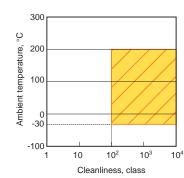
[Remark] When other sizes are used, consult with JTEKT.

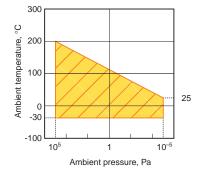
The Lubricating Properties of Grease in Clean / Vacuum Applications

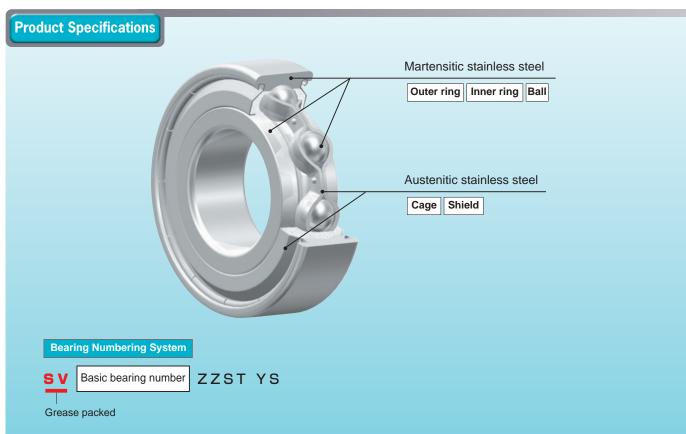
This bearing is lubricated with the packed fluorinated KDL grease, which is suitable for use in clean environments and vacuum environments.

Applicable Environments







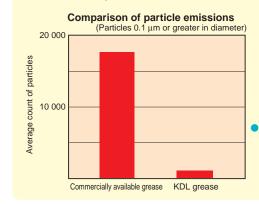


Applications

- Semiconductor manufacturing equipment LCD manufacturing equipment Transfer robots
- Vacuum pumps

Performance

 Suitable for clean and vacuum applications thanks to low particle emissions.



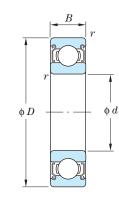
Test conditions

Bearing No.: 6205 Temperature: Atmosphere / room temperature Rotational speed: 450min⁻¹ Load: Radial 10 N

Grease properties

		KDL grease
Thicl	kener	PTFE
Bas	e oil	PFPE
Droppii	ng point	None
Evaporation	(200°C×22h)	0.1wt%max.
Oil separation	n (100°C×24h)	2wt%max.
Operating	In atmospheric air	−30 to 200°C
emperature range	In vacuum	−30 to 100°C

Dimensions Table



Dynamic equivalent load $P_r = XF_r + YF_a$ (X and Y are as shown below.) Static equivalent load $P_{0r} = 0.6F_r + 0.5F_a$ When P_{0r} is smaller than F_r . $P_{0r} = F_r$

f_0F_a	e	$\frac{F_{ m a}}{F_{ m r}}$	<i>≤ e</i>	$\frac{F_{\varepsilon}}{F_{1}}$	<u>-</u> >e
C_{0r}		X	Y	X	Y
0.172 0.345 0.689	0.19 0.22 0.26				2.30 1.99 1.71
1.03 1.38 2.07	0.28 0.30 0.34	1	0	0.56	1.55 1.45 1.31
3.45 5.17 6.89	0.38 0.42 0.44				1.15 1.04 1.00

* Colors in the "Bearing No." column indicate the classification of the periods for delivery as shown below.

Available from stock 30 days after receiving an order 45 days after receiving an order

Determined after consultation on each inquiry

Bou	ndary d mr	imensio n	ons	Bearing No.		l ratings ¹⁾ N	Factor	Limiting ²⁾ speed
d	D	В	r (min.)		$C_{ m r}$	$C_{0\mathrm{r}}$	f_0	min ⁻¹
4	12	4	0.2	SV604ZZSTC3 YS	0.80	0.30	12.4	10 000
	13	5	0.2	SV624ZZSTC3 YS	1.10	0.40	12.3	9 000
5	14	5	0.2	SV605ZZSTC3 YS	1.10	0.40	12.3	8 000
	16	5	0.3	SV625-5ZZSTC3 YS	1.45	0.55	12.4	6 700
6	17	6	0.3	SV606ZZSTC3 YS	1.65	0.60	12.2	6 600
	19	6	0.3	SV626ZZSTC3 YS	2.20	0.85	12.3	5 900
7	19	6	0.3	SV607ZZSTC3 YS	2.20	0.85	12.3	5 700
	22	7	0.3	SV627ZZSTC3 YS	2.80	1.10	12.4	4 900
8	22	7	0.3	SV608ZZSTC3 YS	2.80	1.10	12.4	5 000
	24	8	0.3	SV628ZZSTC3 YS	2.85	1.10	12.8	4 700
9	24	7	0.3	SV609ZZSTC3 YS	2.85	1.10	12.8	4 400
	26	8	0.6	SV629ZZSTC3 YS	3.90	1.55	12.4	3 900
9.525	22.225	7.142	0.5	SVEE3SZZSTC3 YS	2.85	1.10	12.8	5 600
10	26	8	0.3	SV6000ZZSTC3 YS	3.85	1.55	12.3	4 000
	30	9	0.6	SV6200ZZSTC3 YS	4.35	1.90	13.2	3 400
12	28	8	0.3	SV6001ZZSTC3 YS	4.35	1.90	13.2	3 300
	32	10	0.6	SV6201ZZSTC3 YS	5.75	2.45	12.3	3 100
15	32	9	0.3	SV6002ZZSTC3 YS	4.75	2.25	13.9	2 600
	35	11	0.6	SV6202ZZSTC3 YS	6.50	3.00	13.2	2 400
17	35	10	0.3	SV6003ZZSTC3 YS	5.10	2.60	14.4	2 300
	40	12	0.6	SV6203ZZSTC3 YS	8.15	3.85	13.2	2 100
20	42	12	0.6	SV6004ZZSTC3 YS	8.00	4.05	13.9	2 000
	47	14	1	SV6204ZZSTC3 YS	10.9	5.35	13.2	1 800
25	47	12	0.6	SV6005ZZSTC3 YS	8.55	4.65	14.5	1 600
	52	15	1	SV6205ZZSTC3 YS	11.9	6.30	13.9	1 400
30	55	13	1	SV6006ZZSTC3 YS	11.2	6.60	14.7	1 300
	62	16	1	SV6206ZZSTC3 YS	16.5	9.05	13.9	1 200
35	62	14	1	SV6007ZZSTC3 YS	13.5	8.25	14.9	1 100
	72	17	1.1	SV6207ZZSTC3 YS	21.8	12.3	13.9	1 000
40	68	15	1	SV6008ZZSTC3 YS	14.2	9.20	15.2	1 000
	80	18	1.1	SV6208ZZSTC3 YS	24.8	14.3	14.0	900

To calculate dynamic equivalent radial loads, multiply the C_{0r} value in this table by 1.25.

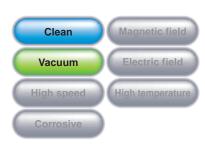
2) The limiting speed is that determined based on the condition that the cleanliness requirement is class 100. [Remark] When other sizes are used, consult with JTEKT.

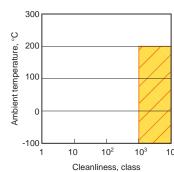
FA Bearings

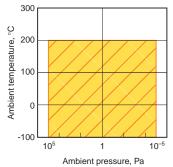
Basic Specification for Supporting Clean, Vacuum Environments

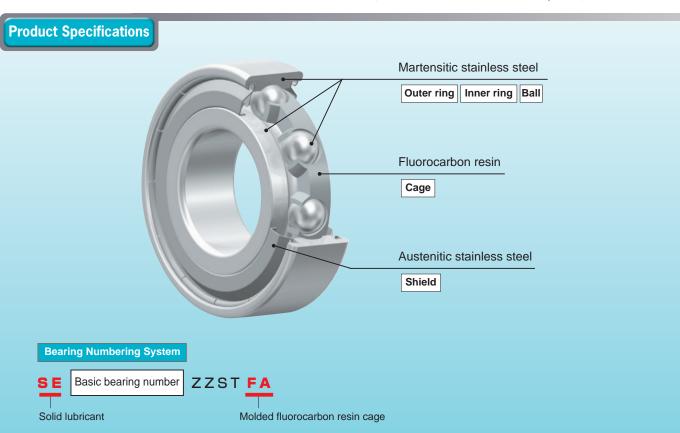
This bearing is lubricated with a solid fluoropolymer lubricant, which offers superior lubrication performance. The cage is made from a low-particle-emission fluorocarbon resin.











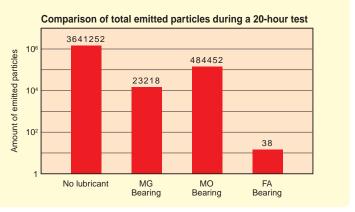
Applications

- Semiconductor manufacturing equipment LCD manufacturing equipment Transfer systems
- Inspection systems

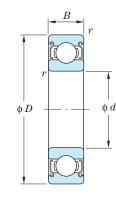
Performance

Test conditions

Tested bearing	ML6012 equivalent (ϕ 6×12×3)			
Rotational speed	200min ⁻¹			
Radial load	2.9 N/2 bearings			
Ambience	In Class 10 clean bench, room temperature			
Test time	20h			
Measured particle size	Particle size 0.3 μm or larger			



Dimensions Table



 $\begin{aligned} & \text{Dynamic equivalent load} \\ & P_r = XF_r + YF_a \\ & (X \text{ and } Y \text{ are as shown below.}) \end{aligned}$ $& \text{Static equivalent load} \\ & P_{0r} = 0.6F_r + 0.5F_a \\ & \text{When } P_{0r} \text{ is smaller than } F_r \,. \\ & P_{0r} = F_r \end{aligned}$

$\frac{f_0 F_a}{C_{0r}}$	e	$\frac{F_{ m a}}{F_{ m r}}$	≤ e	$\frac{F_{\rm a}}{F_{\rm r}} > e$		
$C_{0\mathrm{r}}$		X	Y	X	Y	
0.172 0.345 0.689	0.19 0.22 0.26				2.30 1.99 1.71	
1.03 1.38 2.07	0.28 0.30 0.34	1	0	0.56	1.55 1.45 1.31	
3.45 5.17 6.89	0.38 0.42 0.44				1.15 1.04 1.00	

- * Colors in the "Bearing No." column indicate the classification of the periods for delivery as shown below.
- Available from stock

 30 days after receiving an order

 45 days after receiving an order
- Determined after consultation on each inquiry

Bou	ndary d mr		ons	Bearing No.	Factor	Permissible radial load	Limiting speed	
d	D	В	r (min.)		f_0	N	min ⁻¹	
4	12	4	0.2	SE604ZZSTFA	12.4	7.5	1000	
	13	5	0.2	SE624ZZSTFA	12.3	10	1000	
5	14	5	0.2	SE605ZZSTFA	12.3	10	1000	
	16	5	0.3	SE625-5ZZSTFA	12.4	15	1000	
6	17	6	0.3	SE606ZZSTFA	12.2	15	1000	
	19	6	0.3	SE626ZZSTFA	12.3	20	1000	
7	19	6	0.3	SE607ZZSTFA	12.3	20	1000	
	22	7	0.3	SE627ZZSTFA	12.4	25	1000	
8	22	7	0.3	SE608ZZSTC3FA	12.4	25	1000	
	24	8	0.3	SE628ZZSTFA	12.8	25	1000	
9	24	7	0.3	SE609ZZSTFA	12.8	25	1000	
	26	8	0.6	SE629ZZSTFA	12.4	35	970	
9.525	22.225	7.142	0.5	SEEE3SZZSTFA	12.8	35	1000	
10	26	8	0.3	SE6000ZZSTFA	12.3	35	1000	
	30	9	0.6	SE6200ZZSTFA	13.2	50	860	
12	28	8	0.3	SE6001ZZSTFA	13.2	40	830	
	32	10	0.6	SE6201ZZSTFA	12.3	70	770	
15	32	9	0.3	SE6002ZZSTFA	13.9	45	660	
	35	11	0.6	SE6202ZZSTFA	13.2	75	610	
17	35	10	0.3	SE6003ZZSTFA	14.4	50	580	
	40	12	0.6	SE6203ZZSTFA	13.2	95	530	
20	42	12	0.6	SE6004ZZSTFA	13.9	70	500	
	47	14	1	SE6204ZZSTFA	13.2	130	450	
25	47	12	0.6	SE6005ZZSTFA	14.5	75	400	
	52	15	1	SE6205ZZSTFA	13.9	140	360	
30	55	13	1	SE6006ZZSTC3FA	14.7	95	330	
	62	16	1	SE6206ZZSTFA	13.9	195	300	
35	62	14	1	SE6007ZZSTFA	14.9	110	280	
	72	17	1.1	SE6207ZZSTFA	13.9	210	250	
40	68	15	1	SE6008ZZSTFA	15.2	135	250	
	80	18	1.1	SE6208ZZSTFA	14.0	230	220	

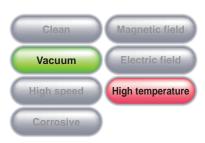
3

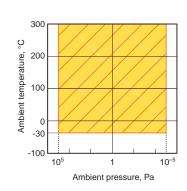
PN Bearings

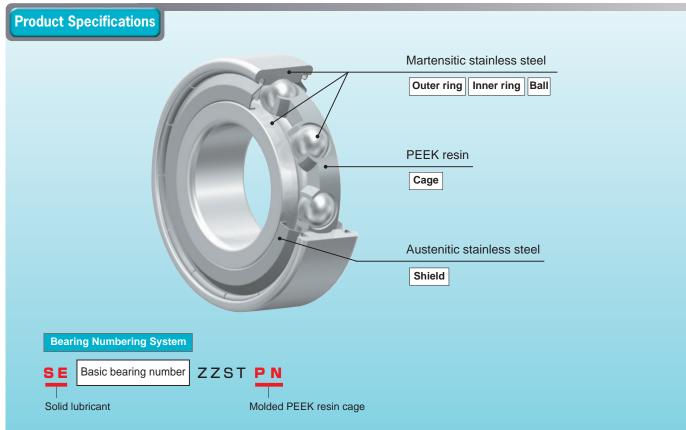
Superior Heat Resistance Supporting 300°C

This bearing has a highly heat resistant solid lubricant, such as molybdenum disulfide included in the cage material.

Applicable Environments





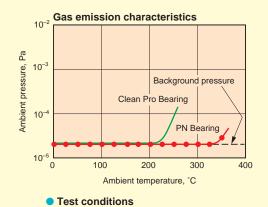


Applications

■ Carton manufacturing equipment ■ LCD cleaning equipment

Performance

Useful up to 300°C in a vacuum.



Bearing No.: 608

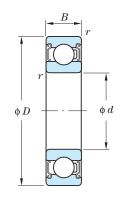
 Excellent in lubricant service life in temperatures from room temp. to 300°C.



Test conditions

Bearing No.: 608 Rotational speed: 200min⁻¹, Load: Axial 100 N

Dimensions Table



Dynamic equivalent load
$$\begin{split} P_r &= XF_r + YF_a \\ &\quad (X \text{ and } Y \text{ are as shown below.}) \end{split}$$
 Static equivalent load $P_{0r} = 0.6F_r + 0.5F_a \\ \text{When } P_{0r} \text{ is smaller than } F_r. \\ P_{0r} &= F_r \end{split}$

f_0F_a	e	$\frac{F_{ m a}}{F_{ m r}}$	· ≤ <i>e</i>	$\frac{F_s}{F_1}$	<u>-</u> >e
$C_{0\mathrm{r}}$		X	Y	X	Y
0.172 0.345 0.689	0.19 0.22 0.26				2.30 1.99 1.71
1.03 1.38 2.07	0.28 0.30 0.34	1	0	0.56	1.55 1.45 1.31
3.45 5.17 6.89	0.38 0.42 0.44				1.15 1.04 1.00
2.07 3.45 5.17	0.34 0.38 0.42	·	Ĵ	0.56	

- * Colors in the "Bearing No." column indicate the classification of the periods for delivery as shown below.

 Available from stock
- 30 days after receiving an order
 45 days after receiving an order
- 45 days after receiving an order

 Determined after consultation on each inquiry

Bou	ndary d i mn	imensio n	ns	Bearing No.	Factor	Permissible radial load	Limiting speed
d	D	В	r (min.)		f_0	N	min ⁻¹
4	12	4	0.2	SE604ZZSTC3 PN	12.4	30	1 000
	13	5	0.2	SE624ZZSTC3 PN	12.3	40	1 000
5	14	5	0.2	SE605ZZSTC3 PN	12.3	40	1 000
	16	5	0.3	SE625-5ZZSTC3 PN	12.4	55	1 000
6	17	6	0.3	SE606ZZSTC3 PN	12.2	60	1 000
	19	6	0.3	SE626ZZSTC3 PN	12.3	80	1 000
7	19	6	0.3	SE607ZZSTC3 PN	12.3	80	1 000
	22	7	0.3	SE627ZZSTC3 PN	12.4	100	1 000
8	22	7	0.3	SE608ZZSTC3 PN	12.4	100	1 000
	24	8	0.3	SE628ZZSTC3 PN	12.8	100	1 000
9	24	7	0.3	SE609ZZSTC3 PN	12.8	100	1 000
	26	8	0.6	SE629ZZSTC3 PN	12.4	135	970
9.525	22.225	7.142	0.5	SEEE3SZZSTC3 PN	12.8	100	1 000
10	26	8	0.3	SE6000ZZSTC3 PN	12.3	135	1 000
	30	9	0.6	SE6200ZZSTC3 PN	13.2	155	860
12	28	8	0.3	SE6001ZZSTC3 PN	13.2	155	830
	32	10	0.6	SE6201ZZSTC3 PN	12.3	205	770
15	32	9	0.3	SE6002ZZSTC3 PN	13.9	170	660
	35	11	0.6	SE6202ZZSTC3 PN	13.2	230	610
17	35	10	0.3	SE6003ZZSTC3 PN	14.4	180	580
	40	12	0.6	SE6203ZZSTC3 PN	13.2	285	530
20	42	12	0.6	SE6004ZZSTC3 PN	13.9	280	500
	47	14	1	SE6204ZZSTC3 PN	13.2	385	450
25	47	12	0.6	SE6005ZZSTC3 PN	14.5	305	400
	52	15	1	SE6205ZZSTC3 PN	13.9	420	360
30	55	13	1	SE6006ZZSTC3 PN	14.7	395	330
	62	16	1	SE6206ZZSTC3 PN	13.9	585	300
35	62	14	1	SE6007ZZSTC3 PN	14.9	475	280
	72	17	1.1	SE6207ZZSTC3 PN	13.9	770	250
40	68	15	1	SE6008ZZSTC3 PN	15.2	500	250
	80	18	1.1	SE6208ZZSTC3 PN	14.0	875	220

[Remark] When other sizes are used, consult with JTEKT.

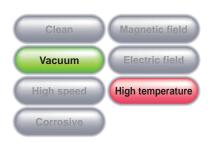
Radial Ball Bearings

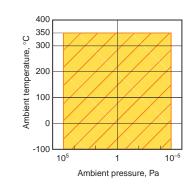
3-7 WS Bearings

Combines 350°C Heat Resistance and Load Carrying Capability

This bearing has extremely heat resistant tungsten disulfide included in the separator material as the lubricant.

Applicable Environments





*We recommend that this bearing is used with horizontal axes.

For information on using this bearing with items other than horizontal axes, consult JTEKT.

Martensitic stainless steel Outer ring Inner ring Ball Sintered composite material including tungsten disulfide Separator Austenitic stainless steel Shield Bearing Numbering System SE Basic bearing number ZZST WS

Applications

Solid lubricant

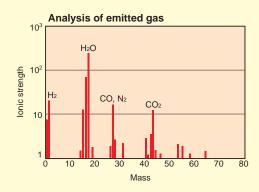
■ Semiconductor manufacturing equipment ■ LCD manufacturing equipment ■ Vacuum evaporation

Separators including tungsten disulfide

■ Plasma display panel manufacturing equipment

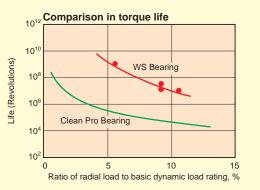
Performance

• Free from problematic gas emissions under the conditions of up to 10⁻⁵ Pa and up to 350°C.



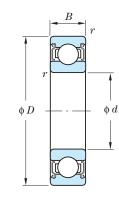
Test conditionsBearing No.: 608

 Highly heat resistant and superior to the Clean Pro Bearing in lubrication life.



Test conditions
 Bearing No.: 608, Rotational speed: 500min⁻¹
 Atmosphere pressure: 10⁻³ Pa

Dimensions Table



Dynamic equivalent load
$$\begin{split} P_r &= XF_r + YF_a \\ &\quad (X \text{ and } Y \text{ are as shown below.}) \end{split}$$
 Static equivalent load $P_{0r} = 0.6F_r + 0.5F_a \\ &\quad \text{When } P_{0r} \text{ is smaller than } F_r. \\ P_{0r} &= F_r \end{split}$

f_0F_a	e	$\frac{F_{ m a}}{F_{ m r}}$	· ≤ <i>e</i>	$\frac{F_{\rm a}}{F_{\rm r}} > e$		
C_{0r}		X	Y	X	Y	
0.172 0.345 0.689	0.19 0.22 0.26				2.30 1.99 1.71	
1.03 1.38 2.07	0.28 0.30 0.34	1	0	0.56	1.55 1.45 1.31	
3.45 5.17 6.89	0.38 0.42 0.44				1.15 1.04 1.00	

* Colors in the "Bearing No." column indicate the classification of the periods for delivery as shown below.

Available from stock

30 days after receiving an order 45 days after receiving an order

Determined after consultation on each inquiry

Bou	ndary d mr		ons	Bearing No.	Factor	Permissible radial load	Limiting speed
d	D	В	$r \pmod{1}$		f_0	N	min ⁻¹
6	17	6	0.3	SE606ZZSTC4 WS	12.2	100	500
	19	6	0.3	SE626ZZSTC4 WS	12.3	130	500
7	19	6	0.3	SE607ZZSTC4 WS	12.3	130	500
	22	7	0.3	SE627ZZSTC4 WS	12.4	165	490
8	22	7	0.3	SE608ZZSTC4 WS	12.4	165	500
	24	8	0.3	SE628ZZSTC4 WS	12.8	170	470
9	24	7	0.3	SE609ZZSTC4 WS	12.8	170	440
	26	8	0.6	SE629ZZSTC4 WS	12.4	230	390
9.525	22.225	7.142	0.5	SEEE3SZZSTC4 WS	12.8	165	410
10	26	8	0.3	SE6000ZZSTC4 WS	12.3	230	400
	30	9	0.6	SE6200ZZSTC4 WS	13.2	255	340
12	28	8	0.3	SE6001ZZSTC4 WS	13.2	255	330
	32	10	0.6	SE6201ZZSTC4 WS	12.3	340	310
15	32	9	0.3	SE6002ZZSTC4 WS	13.9	280	260
	35	11	0.6	SE6202ZZSTC4 WS	13.2	385	240
17	35	10	0.3	SE6003ZZSTC4 WS	14.4	300	230
	40	12	0.6	SE6203ZZSTC4 WS	13.2	480	210
20	42	12	0.6	SE6004ZZSTC4 WS	13.9	470	200
	47	14	1	SE6204ZZSTC4 WS	13.2	640	180
25	47	12	0.6	SE6005ZZSTC4 WS	14.5	505	160
	52	15	1	SE6205ZZSTC4 WS	13.9	700	140
30	55	13	1	SE6006ZZSTC4 WS	14.7	660	130
	62	16	1	SE6206ZZSTC4 WS	13.9	975	120
35	62	14	1	SE6007ZZSTC4 WS	14.9	795	110
	72	17	1.1	SE6207ZZSTC4 WS	13.9	1 285	100
40	68	15	1	SE6008ZZSTC4 WS	15.2	835	100
	80	18	1.1	SE6208ZZSTC4 WS	14.0	1 455	90

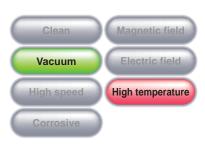
3

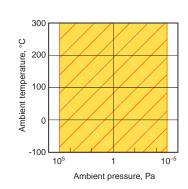
MO Bearings

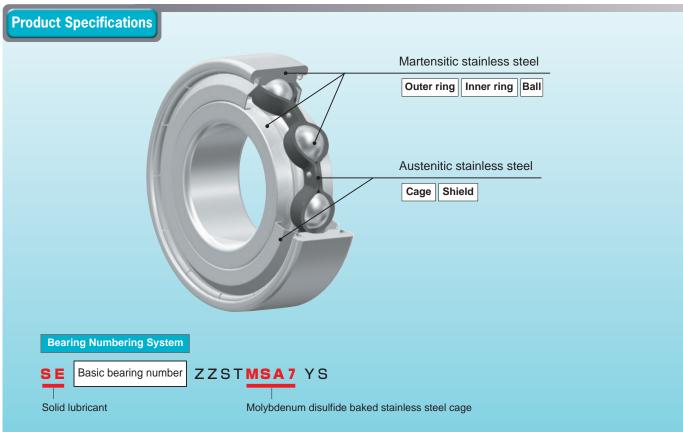
Basic Specification for 300°C Support

This bearing has molybdenum disulfide baked on the surface of the stainless steel cage, as the lubricant.

Applicable Environments





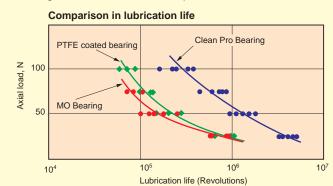


Applications

- Semiconductor manufacturing equipment LCD manufacturing equipment Vacuum evaporator
- Turbo molecular pump
 Rotary furnaces

Performance

 Molybdenum disulfide compares to the common PTFE coating in lubrication life but is superior in heat resistance.



Test conditions Bearing No.: 608

Lubricant service life expectancy equation

The average service life of EXSEV bearings with the cage coated with molybdenum disulfide (MO bearings) can be estimated with the following equation.

$$L_{\text{av}} = b_2 \cdot \left(\frac{C_{\text{r}} \times 0.85}{P_{\text{r}}} \right)^q \times 0.016667/n$$

: Average life, h

: Lubrication factor

 $b_2 = 6$

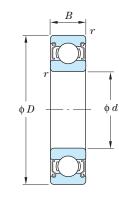
: Basic dynamic load rating, N

: Dynamic equivalent radial load, N : Exponential coefficient, q = 3

: Rotational speed, min-1

For the service life of solid lubricants, refer to page 13.

Dimensions Table



Dynamic equivalent load $P_r = XF_r + YF_a$ (X and Y are as shown below.) Static equivalent load $P_{0x} = 0.6F_x + 0.5F_0$ When P_{0r} is smaller than F_r .

$\frac{f_0 F_a}{C_{0r}}$	e	$\frac{F_{ m a}}{F_{ m r}}$	≤ <i>e</i>	$\frac{F_a}{F_r} > e$		
C_{0r}		X	Y	X	Y	
0.172 0.345 0.689	0.19 0.22 0.26				2.30 1.99 1.71	
1.03 1.38 2.07	0.28 0.30 0.34	1	0	0.56	1.55 1.45 1.31	
3.45 5.17 6.89	0.38 0.42 0.44				1.15 1.04 1.00	

* Colors in the "Bearing No." column indicate the classification of the periods for delivery as shown below

Available from stock 30 days after receiving an order 45 days after receiving an order

Determined after consultation on each inquiry

	Dou	ndary d mr	imensio n	ons	Bearing No.	Basic load ratings 1) kN		Factor	Permissible radial load 2)	Limiting speed
	d	D	В	r (min.)	, and the second se	$C_{ m r}$	$C_{0\mathrm{r}}$	f_0	N	min ⁻¹
_	4	12	4	0.2	SE604ZZSTMSA7C3 YS	0.97	0.36	12.4	30	1 000
		13	5	0.2	SE624ZZSTMSA7C3 YS	1.30	0.49	12.3	40	1 000
	5	14	5	0.2	SE605ZZSTMSA7C3 YS	1.30	0.49	12.3	40	1 000
		16	5	0.3	SE625-5ZZSTMSA7C3 YS	1.75	0.67	12.4	55	1 000
	6	17	6	0.3	SE606ZZSTMSA7C3 YS	1.95	0.74	12.2	60	1 000
		19	6	0.3	SE626ZZSTMSA7C3 YS	2.60	1.05	12.3	80	1 000
	7	19	6	0.3	SE607ZZSTMSA7C3 YS	2.60	1.05	12.3	80	1 000
_		22	7	0.3	SE627ZZSTMSA7C3 YS	3.30	1.35	12.4	100	1 000
	8	22	7	0.3	SE608ZZSTMSA7C3 YS	3.30	1.35	12.4	100	1 000
		24	8	0.3	SE628ZZSTMSA7C3 YS	3.35	1.40	12.8	100	1 000
	9	24	7	0.3	SE609ZZSTMSA7C3 YS	3.35	1.40	12.8	100	1 000
_		26	8	0.6	SE629ZZSTMSA7C3 YS	4.55	1.95	12.4	135	970
	9.525	22.225	7.142	0.5	SEEE3SZZSTMSA7C3 YS	3.35	1.40	12.8	100	1 000
	10	26	8	0.3	SE6000ZZSTMSA7C3 YS	4.55	1.95	12.3	135	1 000
		30	9	0.6	SE6200ZZSTMSA7C3 YS	5.10	2.40	13.2	155	860
	12	28	8	0.3	SE6001ZZSTMSA7C3 YS	5.10	2.40	13.2	155	830
_		32	10	0.6	SE6201ZZSTMSA7C3 YS	6.80	3.05	12.3	205	770
	15	32	9	0.3	SE6002ZZSTMSA7C3 YS	5.60	2.85	13.9	170	660
_		35	11	0.6	SE6202ZZSTMSA7C3 YS	7.65	3.75	13.2	230	610
	17	35	10	0.3	SE6003ZZSTMSA7C3 YS	6.00	3.25	14.4	180	580
		40	12	0.6	SE6203ZZSTMSA7C3 YS	9.55	4.80	13.2	285	530
	20	42	12	0.6	SE6004ZZSTMSA7C3 YS	9.40	5.05	13.9	280	500
		47	14	1	SE6204ZZSTMSA7C3 YS	12.8	6.65	13.2	385	450
	25	47	12	0.6	SE6005ZZSTMSA7C3 YS	10.1	5.85	14.5	305	400
_		52	15	1	SE6205ZZSTMSA7C3 YS	14.0	7.85	13.9	420	360
	30	55	13	1	SE6006ZZSTMSA7C3 YS	13.2	8.25	14.7	395	330
_		62	16	1	SE6206ZZSTMSA7C3 YS	19.5	11.3	13.9	585	300
	35	62	14	1	SE6007ZZSTMSA7C3 YS	15.9	10.3	14.9	475	280
_		72	17	1.1	SE6207ZZSTMSA7C3 YS	25.7	15.4	13.9	770	250
<i>1</i> .	40	68	15	1	SE6008ZZSTMSA7C3 YS	16.7	11.5	15.2	500	250
		80	18	1.1	SE6208ZZSTMSA7C3 YS	29.1	17.8	14.0	875	220

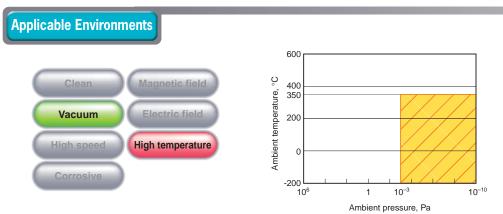
2) The permissible radial loads can be regarded as the maximum loads applicable to individual bearings. When an axial load is applied to the bearing, convert this axial load to a dynamic equivalent radial load, and then compare this value to the permissible radial load.

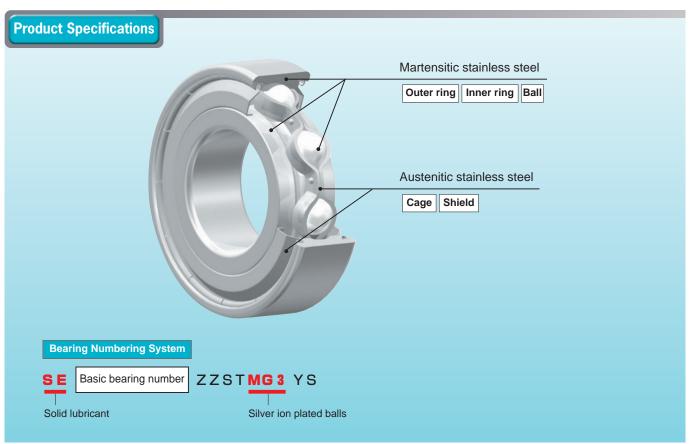
[Remark] When other sizes are used, consult with JTEKT.

MG Bearings

Supports Ultra-high Temperature Vacuums

This bearing has silver ion plated on the stainless steel balls, as the lubricant.



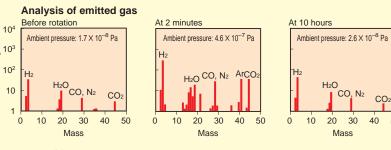


Applications

- Semiconductor manufacturing equipment LCD manufacturing equipment Vacuum evaporator
- Medical equipment Vacuum motors

Performance

 Useful in an ultrahigh vacuum environment of 10⁻¹⁰ Pa thanks to low gas emissions in an ultrahigh vacuum.



Test conditions

Temperature: Atmosphere / room temperature, Load: Radial 3 N \cdot Axial 98 N Ambient pressure: 1.3 \times 10⁻⁸ Pa (1.0 \times 10⁻¹⁰ Torr), Rotational speed: 140min

Lubricant service life expectancy equation

The average service life of bearings with silver ion-plated balls (MG bearings) can be estimated with the following

$$L_{\rm vh} = b_1 \cdot b_2 \cdot b_3 \left(\frac{C_{\rm r}}{13 \times P_{\rm r}} \right)^q \times 16 \ 667/n$$

: 90% confidence service life, h : Basic dynamic load rating, N $C_{\rm r}$

: Dynamic equivalent radial load, N : Exponential coefficient, q = 1

: Rotational speed, min⁻¹ However, 10≦n≦10 000

 $b_1 = 1.5510^{-3} n + 1$

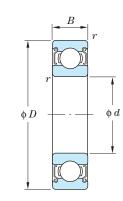
: Lubrication factor

 $b_2 = 1$

: Atmosphere pressure/temperature dependency coefficient $b_3 = 1$ (when 10^{-3} Pa, room temperature)

For the service life of solid lubricants, refer to page 13.

Dimensions Table



Dynamic equivalent load $P_{\rm r} = XF_{\rm r} + YF_{\rm a}$ (X and Y are as shown below.) Static equivalent load $P_{0r} = 0.6F_r + 0.5F_a$

> When P_{0r} is smaller than F_r . $P_{0r} = F_r$

f_0F_a	e	$rac{F_{ m a}}{F_{ m r}}$	· ≤ e	$\frac{F_s}{F_1}$	$\frac{1}{2} > e$
$C_{0\mathrm{r}}$		X	Y	X	Y
0.172 0.345 0.689	0.19 0.22 0.26				2.30 1.99 1.71
1.03 1.38 2.07	0.28 0.30 0.34	1	0	0.56	1.55 1.45 1.31
3.45 5.17 6.89	0.38 0.42 0.44				1.15 1.04 1.00

* Colors in the "Bearing No." column indicate the classification of the periods for delivery as shown below

30 days after receiving an order 45 days after receiving an order

Available from stock

Determined after consultation on each inquiry

	Bou	ndary d mr		ns	Bearing No.	Basic load kN		Factor	Permissible radial load 2)	Limiting speed
	d	D	В	$r \pmod{1}$	J	$C_{ m r}$	$C_{0\mathrm{r}}$	f_0	N	min ⁻¹
	4	12	4	0.2	SE604ZZSTMG3C4 YS	0.97	0.36	12.4	30	1 000
		13	5	0.2	SE624ZZSTMG3C4 YS	1.30	0.49	12.3	40	1 000
	5	14	5	0.2	SE605ZZSTMG3C4 YS	1.30	0.49	12.3	40	1 000
		16	5	0.3	SE625-5ZZSTMG3C4 YS	1.75	0.67	12.4	55	1 000
	6	17	6	0.3	SE606ZZSTMG3C4 YS	1.95	0.74	12.2	60	1 000
		19	6	0.3	SE626ZZSTMG3C4 YS	2.60	1.05	12.3	80	1 000
	7	19	6	0.3	SE607ZZSTMG3C4 YS	2.60	1.05	12.3	80	1 000
		22	7	0.3	SE627ZZSTMG3C4 YS	3.30	1.35	12.4	100	1 000
	8	22	7	0.3	SE608ZZSTMG3C4 YS	3.30	1.35	12.4	100	1 000
		24	8	0.3	SE628ZZSTMG3C4 YS	3.35	1.40	12.8	100	1 000
	9	24	7	0.3	SE609ZZSTMG3C4 YS	3.35	1.40	12.8	100	1 000
		26	8	0.6	SE629ZZSTMG3C4 YS	4.55	1.95	12.4	135	970
	9.525	22.225	7.142	0.5	SEEE3SZZSTMG3C4 YS	3.35	1.40	12.8	100	1 000
	10	26	8	0.3	SE6000ZZSTMG3C4 YS	4.55	1.95	12.3	135	1 000
		30	9	0.6	SE6200ZZSTMG3C4 YS	5.10	2.40	13.2	155	860
	12	28	8	0.3	SE6001ZZSTMG3C4 YS	5.10	2.40	13.2	155	830
		32	10	0.6	SE6201ZZSTMG3C4 YS	6.80	3.05	12.3	205	770
	15	32	9	0.3	SE6002ZZSTMG3C4 YS	5.60	2.85	13.9	170	660
		35	11	0.6	SE6202ZZSTMG3C4 YS	7.65	3.75	13.2	230	610
-	17	35	10	0.3	SE6003ZZSTMG3C4 YS	6.00	3.25	14.4	180	580
		40	12	0.6	SE6203ZZSTMG3C4 YS	9.55	4.80	13.2	285	530
	20	42	12	0.6	SE6004ZZSTMG3C4 YS	9.40	5.05	13.9	280	500
		47	14	1	SE6204ZZSTMG3C4 YS	12.8	6.65	13.2	385	450
	25	47	12	0.6	SE6005ZZSTMG3C4 YS	10.1	5.85	14.5	305	400
		52	15	1	SE6205ZZSTMG3C4 YS	14.0	7.85	13.9	420	360
_	30	55	13	1	SE6006ZZSTMG3C4 YS	13.2	8.25	14.7	395	330
_		62	16	1	SE6206ZZSTMG3C4 YS	19.5	11.3	13.9	585	300
W.	35	62	14	1	SE6007ZZSTMG3C4 YS	15.9	10.3	14.9	475	280
		72	17	1.1	SE6207ZZSTMG3C4 YS	25.7	15.4	13.9	770	250
	40	68	15	1	SE6008ZZSTMG3C4 YS	16.7	11.5	15.2	500	250
		80	18	1.1	SE6208ZZSTMG3C4 YS	29.1	17.8	14.0	875	220

Notes 1) The basic load ratings are those of normal bearing (used to calculate lubrication life).

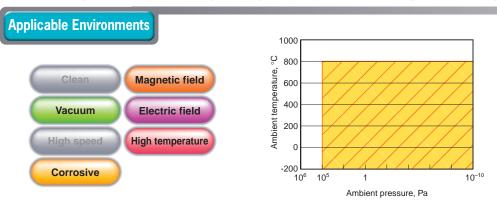
2) The permissible radial loads can be regarded as the maximum loads applicable to individual bearings. When an axial load is applied to the bearing, convert this axial load to a dynamic equivalent radial load, and then compare this value to the permissible radial load.

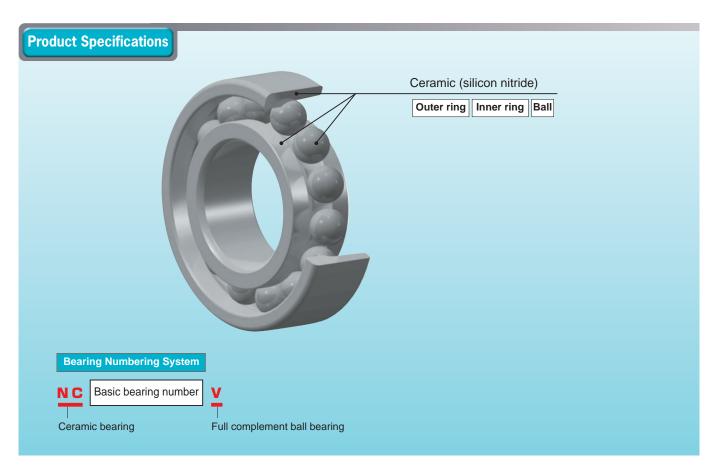
[Remark] Bearings not listed in the Dimensions Table are also available, so contact JTEKT for information on these

Full Complement Ceramic Ball Bearings

Ultra-high Temperature 800°C

This bearing has all components made of ceramic for use in an ultrahigh temperature environments. No cage is provided. Being an angular contact ball bearing, this bearing is normally used in pairs.

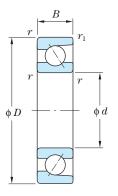




Applications

■ Baking Furnace cars ■ Fans in furnaces

Dimensions Table



Dynamic equivalent load $P_r = XF_r + YF_a$ (X and Y are as shown below.) Static equivalent load $P_{0r} = 0.6F_r + 0.5F_a$ When P_{0r} is smaller than F_r . $P_{0r} = F_r$

algie	e	Single row or tandem mounting				Back to back or face to face			
contact angle		$\frac{F_{\mathrm{a}}}{F_{\mathrm{r}}}$	$\frac{F_{\rm a}}{F_{\rm r}} \le e$ $\frac{I}{I}$		> <i>e</i>	$\frac{F_a}{F_r} \leq e$		$\frac{F_{\rm a}}{F_{\rm r}} > e$	
Cor		X	Y	X	Y	X	Y	X	Y
30°	0.80	1	0	0.39	0.76	1	0.78	0.63	1.24

 * In the case of back-to-back duplex bearings and face-to-face duplex bearings, apply 2 to i. As for single row bearings and tandem duplex bearings, apply 1 to i.

	Sontact angle	Single tandem r	row or mounting	Back to back or face to face		
	න් රි	X_0	Y_0	X_0	Y_0	
	30°	0.5	0.33	1	0.66	

	Bound	ary dim mm	ensions		Bearing No.	Permissible radial load	Limiting speed
d	D	B	<i>r</i> (min.)	r_1 (min.)		N	min ⁻¹
4	12	4	0.2	0.1	NC704V	10	500
	13	5	0.2	0.1	NC724V	15	500
5	14	5	0.2	0.1	NC705V	15	500
	16	5	0.2	0.1	NC725V	25	500
6	17	6	0.3	0.15	NC706V	20	500
	19	6	0.3	0.15	NC726V	35	500
7	19	6	0.3	0.15	NC707V	30	500
	22	7	0.3	0.15	NC727V	40	490
8	22	7	0.3	0.15	NC708V	40	500
	24	8	0.3	0.15	NC728V	40	470
9	24	7	0.3	0.15	NC709V	40	440
	26	8	0.3	0.15	NC729V	50	390
10	26	8	0.3	0.15	NC7000V	55	400
	30	9	0.6	0.3	NC7200V	60	340
12	28	8	0.3	0.15	NC7001V	60	330
	32	10	0.6	0.3	NC7201V	85	310
15	32	9	0.3	0.15	NC7002V	70	260
	35	11	0.6	0.3	NC7202V	90	240
17	35	10	0.3	0.15	NC7003V	75	230
	40	12	0.6	0.3	NC7203V	115	210
20	42	12	0.6	0.3	NC7004V	115	200
	47	14	1	0.6	NC7204V	160	180
25	47	12	1	0.6	NC7005V	125	160
	52	15	1	0.6	NC7205V	170	140
30	55	13	1	0.6	NC7006V	160	130
	62	16	1	0.6	NC7206V	235	120
35	62	14	1	0.6	NC7007V	195	110
	72	17	1.1	0.6	NC7207V	310	100
40	68	15	1	0.6	NC7008V	195	100
	80	18	1.1	0.6	NC7208V	370	90

*Colors in the "Bearing No." column indicate the classification of the periods for delivery as shown below.

Available from stock

30 days after receiving an order
45 days after receiving an order

Determined after consultation on each inquiry

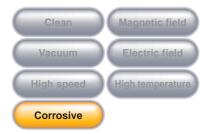
49

SK Bearings

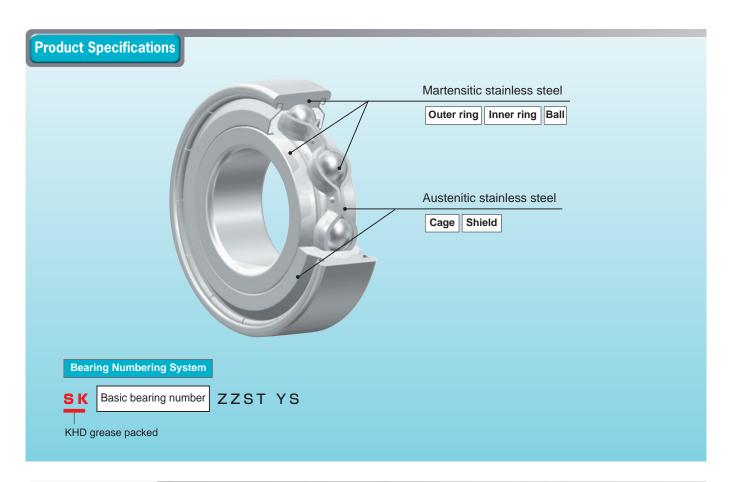
The Standard for Stainless Steel Bearings

This bearing has its components made of stainless steel, and is lubricated with lithium containing KHD grease, which is packed in adequate amounts. This bearing is suitable for use in slightly corrosive environments.

Applicable Environments



- Temperature: 30 to 120°C
- Ambient pressure: Atmospheric pressure
- Unsuitable for clean environments due to anticorrosive treatment.



Applications

■ Chemical equipment ■ Transfer systems

Grease Properties

Grease properties

	KHD grease
Thickener	Lithium soap
Base oil	Poly - α - olefin
Dropping point	203°C
Evaporation (99°C × 22h)	0.14wt%
Oil separation (100°C × 24 h)	0.1wt%
Operating temperature range	−30 to 120°C

Grease life can be estimated by the following equation.

$$\log L = 6.10 - 4.40 \times 10^{-6} d_m n - 2.50 \left(\frac{P_{\rm r}}{C_{\rm r}} - 0.05 \right) - \left(0.021 - 1.80 \times 10^{-8} d_m n \right) T$$

where

greater life $\frac{D+d}{2}$ (D: outside diameter, d: bore diameter) mm: rotational speed min⁻¹: dynamic equivalent radial load N: basic dynamic radial load rating N: operating temperature of bearing °C

The conditions for applying equation are as follows:

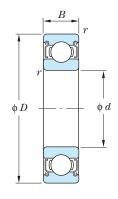
- a) Operating temperature of bearing : T °C Applicable when $T \le 120$ (when T < 50, T = 50) When T > 120, please contact with JTEKT.
- b) Value of $d_m n$ Applicable when $d_m n \le 500 \times 10^3$ (when $d_m n < 125 \times 10^3$, $d_m n = 125 \times 10^3$) When $d_m n > 500 \times 10^3$, please contact with
- c) Load condition : $\frac{P_{\rm r}}{C_{\rm r}}$

Applicable when $\frac{P_{\rm r}}{C} \leq 0.2$

(when $\frac{P_{\mathrm{r}}}{C_{\mathrm{r}}}$ < 0.05, $\frac{P_{\mathrm{r}}}{C_{\mathrm{r}}}$ = 0.05)

When $\frac{P_{\mathrm{r}}}{C_{\mathrm{r}}}$ >0.2, please contact with JTEKT.

Dimensions Table



 $\begin{aligned} \text{Dynamic equivalent load} \\ P_{\text{r}} = XF_{\text{r}} \ + \ YF_{\text{a}} \end{aligned}$

 $P_r = AP_r + P_a$ (X and Y are as shown below.)
Static equivalent load

 $P_{0\mathrm{r}}$ = 0.6 F_{r} + 0.5 F_{a} When $P_{0\mathrm{r}}$ is smaller than F_{r} .

$\frac{f_0 F_a}{C_{0r}}$	e	$rac{F_{ m a}}{F_{ m r}}$	<i>≤ e</i>	$\frac{F_{\varepsilon}}{F_{1}}$	<u>-</u> >e
C_{0r}		X	Y	X	Y
0.172 0.345 0.689	0.19 0.22 0.26				2.30 1.99 1.71
1.03 1.38 2.07	0.28 0.30 0.34	1	0	0.56	1.55 1.45 1.31
3.45 5.17 6.89	0.38 0.42 0.44				1.15 1.04 1.00

* Colors in the "Bearing No." column indicate the classification of the periods for delivery as shown below.

Available from stock

30 days after receiving an order

45 days after receiving an order

Determined after consultation on each inquiry

Bou	ndary d		ons	Bearing No.		d ratings 1) N	Factor		speeds ²⁾ n ⁻¹
d	D	B	r (min.)	g	$C_{ m r}$	$C_{0\mathrm{r}}$	f_0	Grease lubrication	Oil lubrication
10	22	6	0.3	SK6900ZZST YS	2.30	1.00	14.0	34 000	41 000
	26	8	0.3	SK6000ZZST YS	3.85	1.55	12.3	31 000	36 000
	30	9	0.6	SK6200ZZST YS	4.35	1.90	13.2	24 000	29 000
12	24	6	0.3	SK6901ZZST YS	2.45	1.15	14.5	31 000	36 000
	28	8	0.3	SK6001ZZST YS	4.35	1.90	13.2	27 000	32 000
	32	10	0.6	SK6201ZZST YS	5.75	2.45	12.3	22 000	27 000
15	28	7	0.3	SK6902ZZST YS	3.65	1.80	14.3	26 000	30 000
	32	9	0.3	SK6002ZZST YS	4.75	2.25	13.9	23 000	27 000
	35	11	0.6	SK6202ZZST YS	6.50	3.00	13.2	20 000	24 000
17	30	7	0.3	SK6903ZZST YS	3.90	2.05	14.7	23 000	28 000
	35	10	0.3	SK6003ZZST YS	5.10	2.60	14.4	21 000	25 000
	40	12	0.6	SK6203ZZST YS	8.15	3.85	13.2	17 000	21 000
20	37	9	0.3	SK6904ZZST YS	5.40	2.95	14.7	19 000	23 000
	42	12	0.6	SK6004ZZST YS	8.00	4.05	13.9	17 000	21 000
	47	14	1	SK6204ZZST YS	10.9	5.35	13.2	15 000	17 000
25	42	9	0.3	SK6905ZZST YS	5.95	3.65	15.4	16 000	19 000
	47	12	0.6	SK6005ZZST YS	8.55	4.65	14.5	15 000	18 000
	52	15	1	SK6205ZZST YS	11.9	6.30	13.9	13 000	15 000
30	47	9	0.3	SK6906ZZST YS	6.15	4.00	15.8	14 000	17 000
	55	13	1	SK6006ZZST YS	11.2	6.60	14.7	13 000	15 000
	62	16	1	SK6206ZZST YS	16.5	9.05	13.9	11 000	13 000
35	55	10	0.6	SK6907ZZST YS	9.25	6.20	15.7	12 000	14 000
	62	14	1	SK6007ZZST YS	13.5	8.25	14.9	11 000	13 000
	72	17	1.1	SK6207ZZST YS	21.8	12.3	13.9	9 200	11 000
40	68	15	1	SK6008ZZST YS	14.2	9.20	15.2	10 000	12 000
	80	18	1.1	SK6208ZZST YS	24.8	14.3	14.0	8 300	10 000

Notes 1) The basic load ratings are those of bearing made from SUS440C.

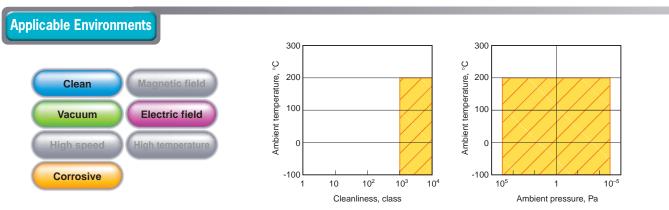
To calculate the dynamic equivalent radial loads, multiply the C_{0r} value in this table by 1.25.

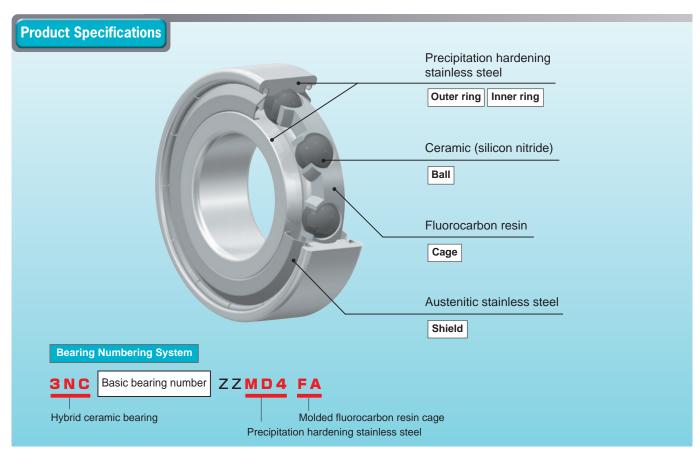
2) Bearings with a contact seal (2RS) are also available.

Corrosion Resistant Hybrid **Ceramic Bearings**

For Salt Water and Chemical **Environments**

This bearing uses a stainless steel variety that has excellent corrosion resistance. As the lubricant, fluoropolymer is used. It is compatible with underwater use.



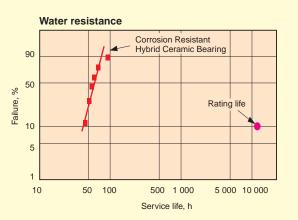


Applications

- Semiconductor manufacturing equipment Chemical manufacturing equipment
- Food machinery
 Cleaning equipment

Performance

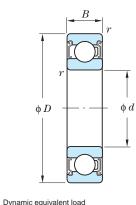
- When this Corrosion Resistant Hybrid Ceramic Bearing is used under water, its service life is determined depending on the rust and/or wear of bearing rings. The service life cannot be estimated correctly from the rating life.
- When this Corrosion Resistant Hybrid Ceramic Bearing is not used under water, select one based on the allowable radial load and limiting speed specified in the Dimensions Table.



Test conditions

Bearing No.: 6206 equivalent Rotational speed: 1500min⁻¹ Load: Radial 196 N

Dimensions Table



 $P_{\rm r} = XF_{\rm r} + YF_{\rm a}$ (X and Y are as shown below.) Static equivalent load $P_{0r} = 0.6F_r + 0.5F_a$ When P_{0r} is smaller than F_r .

$\frac{f_0F_a}{g}$ e		$\frac{F_{ m a}}{F_{ m r}}$	<i>≤ e</i>	$\frac{F_{\rm a}}{F_{\rm r}} > e$		
C_{0r}		X	Y	X	Y	
0.172 0.345 0.689	0.19 0.22 0.26				2.30 1.99 1.71	
1.03 1.38 2.07	0.28 0.30 0.34	1	0	0.56	1.55 1.45 1.31	
3.45 5.17 6.89	0.38 0.42 0.44				1.15 1.04 1.00	

* Colors in the "Bearing No." column indicate the classification of the periods for delivery as shown below.

Determined after consultation on each inquiry

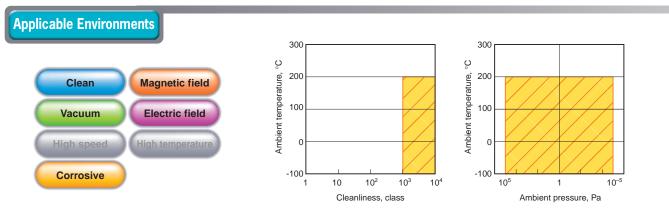
Available from stock 30 days after receiving an order 45 days after receiving an order

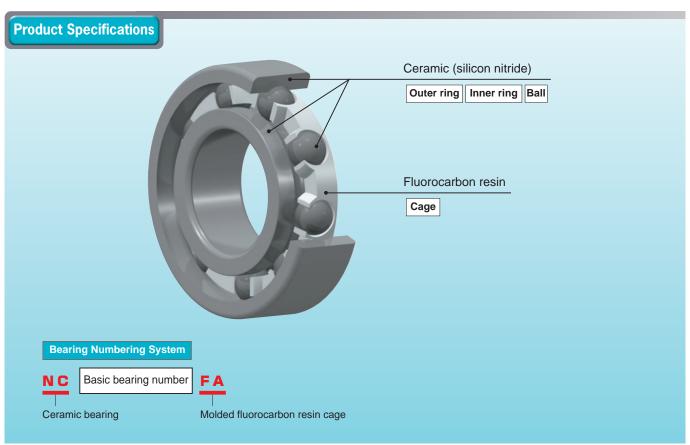
Bou	ndary d mr			Bearing No.	Factor	Permissible radial load	Limiting speed
d	D	В	r (min.)		f_0	N	min ⁻¹
4	12	4	0.2	3NC604ZZMD4 FA	12.4	7.5	1 000
	13	5	0.2	3NC624ZZMD4 FA	12.3	10	1 000
5	14	5	0.2	3NC605ZZMD4 FA	12.3	10	1 000
	16	5	0.3	3NC625-5ZZMD4 FA	12.4	15	1 000
6	17	6	0.3	3NC606ZZMD4 FA	12.2	15	1 000
	19	6	0.3	3NC626ZZMD4 FA	12.3	20	1 000
7	19	6	0.3	3NC607ZZMD4 FA	12.3	20	1 000
	22	7	0.3	3NC627ZZMD4 FA	12.4	25	1 000
8	22	7	0.3	3NC608ZZMD4C3 FA	12.4	25	1 000
	24	8	0.3	3NC628ZZMD4 FA	12.8	25	1 000
9	24	7	0.3	3NC609ZZMD4 FA	12.8	25	1 000
	26	8	0.6	3NC629ZZMD4 FA	12.4	35	970
9.525	22.225	7.142	0.5	3NCEE3SZZMD4 FA	12.8	35	1 000
10	26	8	0.3	3NC6000ZZMD4 FA	12.3	35	1 000
	30	9	0.6	3NC6200ZZMD4 FA	13.2	50	860
12	28	8	0.3	3NC6001ZZMD4 FA	13.2	40	830
	32	10	0.6	3NC6201ZZMD4 FA	12.3	70	770
15	32	9	0.3	3NC6002ZZMD4 FA	13.9	45	660
	35	11	0.6	3NC6202ZZMD4 FA	13.2	75	610
17	35	10	0.3	3NC6003ZZMD4 FA	14.4	50	580
	40	12	0.6	3NC6203ZZMD4 FA	13.2	95	530
20	42	12	0.6	3NC6004ZZMD4 FA	13.9	70	500
	47	14	1	3NC6204ZZMD4 FA	13.2	130	450
25	47	12	0.6	3NC6005ZZMD4 FA	14.5	75	400
	52	15	1	3NC6205ZZMD4 FA	13.9	140	360
30	55	13	1	3NC6006ZZMD4C3 FA	14.7	95	330
	62	16	1	3NC6206ZZMD4 FA	13.9	195	300
35	62	14	1	3NC6007ZZMD4 FA	14.9	110	280
	72	17	1.1	3NC6207ZZMD4 FA	13.9	210	250
40	68	15	1	3NC6008ZZMD4 FA	15.2	135	250
	80	18	1.1	3NC6208ZZMD4 FA	14.0	230	220

³⁻¹³ Ceramic Bearings

Using Ceramics for Various Applications

This bearing has its components made of silicon nitride ceramic and uses fluoropolymer as the lubricant. It is typically used in vacuum and corrosive environments.



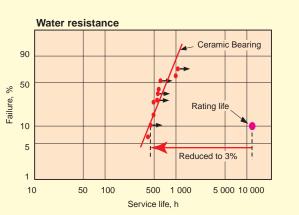


Applications

- Semiconductor manufacturing equipment LCD manufacturing equipment Semiconductor inspection equipment
- Synthetic fiber manufacturing equipment Canning machinery Ultrasonic motors

Performance

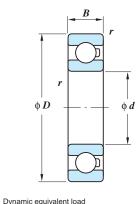
- This Ceramic Bearing can be used under water; however, when used in a liquid with poor lubrication characteristics, the load exerted on the bearing should be no higher than 10% of the bearing's basic dynamic load rating. Also note that the fatigue life of the bearing is 3% of its rating life under water.
- When this Ceramic Bearing is not used under water, select one based on the permissible radial load and limiting speed specified in the Dimensions Table.



Test conditions

Bearing No.: 6206 equivalent Rotational speed: 1500min⁻¹ Load: Radial 1470 N

Dimensions Table



 $P_{\rm r} = XF_{\rm r} + YF_{\rm a}$ (X and Y are as shown below.)Static equivalent load $P_{0r} = 0.6F_r + 0.5F_s$

When P_{0r} is smaller than F_r .

$\frac{f_0F_a}{g}$ e		$\frac{F_{\mathrm{a}}}{F_{\mathrm{r}}}$	≤ e	$\frac{F_{\rm a}}{F_{\rm r}} > e$		
C_{0r}		X	Y	X	Y	
0.172 0.345 0.689	0.19 0.22 0.26				2.30 1.99 1.71	
1.03 1.38 2.07	0.28 0.30 0.34	1	0	0.56	1.55 1.45 1.31	
3.45 5.17 6.89	0.38 0.42 0.44				1.15 1.04 1.00	

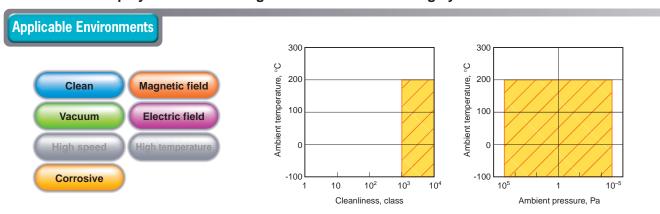
- * Colors in the "Bearing No." column indicate the classification of the periods for delivery as shown below.
- Available from stock 30 days after receiving an order
- 45 days after receiving an order Determined after consultation on each inquiry

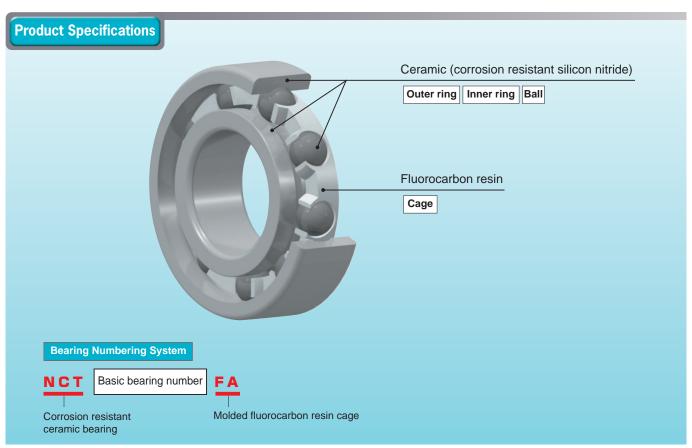
Bou	ndary d mr	imensio n	ns			ad ratings :N	Factor	Permissible	Limiting
			r	Bearing No.				radial load	speed
d	D	B	(min.)		$C_{\rm r}$	$C_{0{ m r}}$	f_0	N	min ⁻¹
4	12	4	0.2	NC604 FA	0.97	0.36	12.4	7.5	1 000
	13	5	0.2	NC624 FA	1.30	0.49	12.3	10	1 000
5	14	5	0.2	NC605 FA	1.30	0.49	12.3	10	1 000
	16	5	0.3	NC625-5 FA	1.75	0.67	12.4	15	1 000
6	17	6	0.3	NC606 FA	1.95	0.74	12.2	15	1 000
	19	6	0.3	NC626 FA	2.60	1.05	12.3	20	1 000
7	19	6	0.3	NC607 FA	2.60	1.05	12.3	20	1 000
	22	7	0.3	NC627 FA	3.30	1.35	12.4	25	1 000
8	22	7	0.3	NC608 FA	3.30	1.35	12.4	25	1 000
	24	8	0.3	NC628 FA	3.35	1.40	12.8	25	1 000
9	24	7	0.3	NC609 FA	3.35	1.40	12.8	25	1 000
	26	8	0.6	NC629 FA	4.55	1.95	12.4	35	970
9.525	22.225	7.142	0.5	NCEE3S FA	3.35	1.40	12.8	35	1 000
10	26	8	0.3	NC6000 FA	4.55	1.95	12.3	35	1 000
	30	9	0.6	NC6200 FA	5.10	2.40	13.2	50	860
12	28	8	0.3	NC6001 FA	5.10	2.40	13.2	40	830
	32	10	0.6	NC6201 FA	6.80	3.05	12.3	70	770
15	32	9	0.3	NC6002 FA	5.60	2.85	13.9	45	660
	35	11	0.6	NC6202 FA	7.65	3.75	13.2	75	610
17	35	10	0.3	NC6003 FA	6.00	3.25	14.4	50	580
	40	12	0.6	NC6203 FA	9.55	4.80	13.2	95	530
20	42	12	0.6	NC6004 FA	9.40	5.05	13.9	70	500
	47	14	1	NC6204 FA	12.8	6.65	13.2	130	450
25	47	12	0.6	NC6005 FA	10.1	5.85	14.5	75	400
	52	15	1	NC6205 FA	14.0	7.85	13.9	140	360
30	55	13	1	NC6006 FA	13.2	8.25	14.7	95	330
	62	16	1	NC6206 FA	19.5	11.3	13.9	195	300
35	62	14	1	NC6007 FA	15.9	10.3	14.9	110	280
	72	17	1.1	NC6207 FA	25.7	15.4	13.9	210	250
40	68	15	1	NC6008 FA	16.7	11.5	15.2	135	250
	80	18	1.1	NC6208 FA	29.1	17.8	14.0	230	220
									5

Ceramic Bearings

Ceramics with Increased Corrosion Resistance

This bearing has its components made of corrosion resistant silicon nitride and is lubricated with fluoropolymer. This bearing can be used even in a highly corrosive solution.



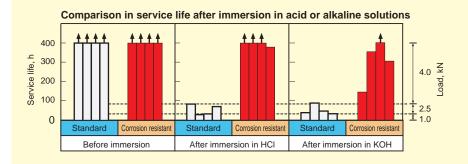


Applications

- Liquid crystal film manufacturing equipment Aluminum electrolytic capacitor manufacturing equipment
- Plating equipment Synthetic fiber manufacturing equipment Food container washing machine

Performance

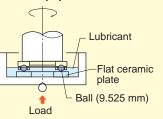
 In an acid or alkaline solution, this bearing has a longer service life than bearings made from standard silicone nitride.



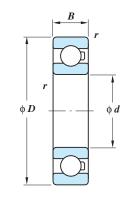
Test conditions

Lubricant : Spindle oil
Ball : Bearing steel
Load : Increased in stages at every
1.08 × 10⁷ cycles
Rotational speed : 1 200 min⁻¹

Test equipment



Dimensions Table



Dynamic equivalent load
$$\begin{split} P_r &= XF_r + YF_a \\ &\quad (X \text{ and } Y \text{ are as shown below.}) \end{split}$$
 Static equivalent load $P_{0r} = 0.6F_r + 0.5F_a \\ &\quad \text{When } P_{0r} \text{ is smaller than } F_r. \\ P_{0r} &= F_r \end{split}$

f_0F_a	е	$\frac{F_{ m a}}{F_{ m r}}$	≤ <i>e</i>	$\frac{F_{ m a}}{F_{ m r}}$	->e
$C_{0\mathrm{r}}$		X	Y	X	Y
0.172 0.345 0.689	0.19 0.22 0.26				2.30 1.99 1.71
1.03 1.38 2.07	0.28 0.30 0.34	1	0	0.56	1.55 1.45 1.31
3.45 5.17 6.89	0.38 0.42 0.44				1.15 1.04 1.00

*Colors in the "Bearing No." column indicate the classification of the periods for delivery as shown below.

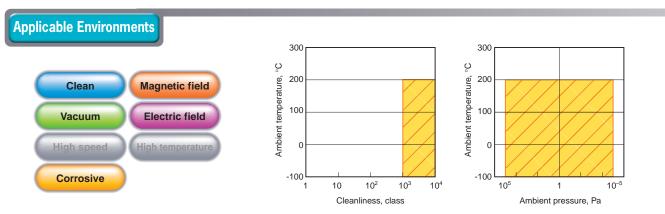
Available from stock
30 days after receiving an order
45 days after receiving an order
Determined after consultation on each inquiry

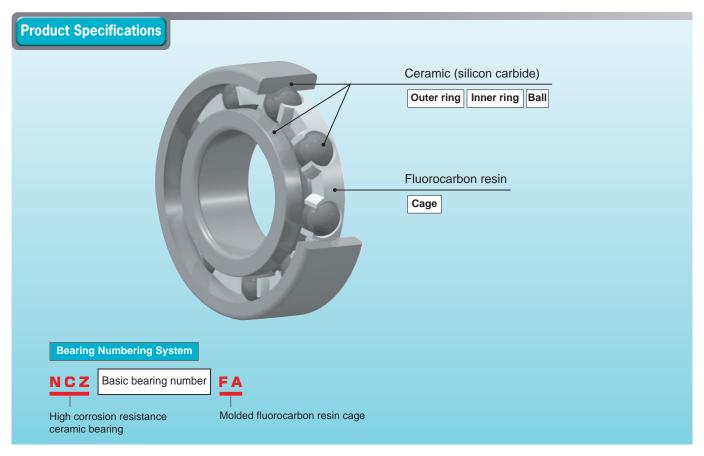
Bou	ndary d mr		ns	Bearing No.	Factor	Permissible radial load	Limiting speed
d	D	В	r (min.)		f_0	N	min ⁻¹
4	12	4	0.2	NCT604 FA	12.4	7.5	1 000
	13	5	0.2	NCT624 FA	12.3	10	1 000
5	14	5	0.2	NCT605 FA	12.3	10	1 000
	16	5	0.3	NCT625-5 FA	12.4	15	1 000
6	17	6	0.3	NCT606 FA	12.2	15	1 000
	19	6	0.3	NCT626 FA	12.3	20	1 000
7	19	8	0.3	NCT607 FA	12.3	20	1 000
	22	7	0.3	NCT627 FA	12.4	25	1 000
8	22	7	0.3	NCT608 FA	12.4	25	1 000
	24	8	0.3	NCT628 FA	12.8	25	1 000
9	24	7	0.3	NCT609 FA	12.8	25	1 000
	26	8	0.6	NCT629 FA	12.4	35	970
9.525	22.225	7.142	0.5	NCTEE3S FA	12.8	35	1 000
10	26	8	0.3	NCT6000 FA	12.3	35	1 000
	30	9	0.6	NCT6200 FA	13.2	50	860
12	28	8	0.3	NCT6001 FA	13.2	40	830
	32	10	0.6	NCT6201 FA	12.3	70	770
15	32	9	0.3	NCT6002 FA	13.9	45	660
	35	11	0.6	NCT6202 FA	13.2	75	610
17	35	10	0.3	NCT6003 FA	14.4	50	580
	40	12	0.6	NCT6203 FA	13.2	95	530
20	42	12	0.6	NCT6004 FA	13.9	70	500
	47	14	1	NCT6204 FA	13.2	130	450
25	47	12	0.6	NCT6005 FA	14.5	75	400
	52	15	1	NCT6205 FA	13.9	140	360
30	55	13	1	NCT6006 FA	14.7	95	330
	62	16	1	NCT6206 FA	13.9	195	300
35	62	14	1	NCT6007 FA	14.9	110	280
	72	17	1.1	NCT6207 FA	13.9	210	250
40	68	15	1	NCT6008 FA	15.2	135	250
	80	18	1.1	NCT6208 FA	14.0	230	220

High Corrosion Resistant Ceramic Bearings

For Extreme Corrosive Environments

This bearing uses a silicon carbide ceramic material, which is resistant to strong acids and alkalis.



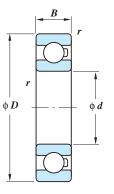


Applications

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■ Aluminum electrolytic capacitor manufacturing equipment

Dimensions Table



Dynamic equivalent load
$$\begin{split} P_{\mathrm{r}} &= XF_{\mathrm{r}} + YF_{\mathrm{a}} \\ &\quad (X \text{ and } Y \text{ are as shown below.}) \end{split}$$
 Static equivalent load $P_{0\mathrm{r}} = 0.6F_{\mathrm{r}} + 0.5F_{\mathrm{a}} \\ &\quad \text{When } P_{0\mathrm{r}} \text{ is smaller than } F_{\mathrm{r}}. \end{split}$

f_0F_a	e	$\frac{F_{ m a}}{F_{ m r}}$	≤ <i>e</i>	$\frac{F_{\rm a}}{F_{\rm r}} > e$		
C_{0r}		X	Y	X	Y	
0.172 0.345 0.689	0.19 0.22 0.26		0	0.56	2.30 1.99 1.71	
1.03 1.38 2.07	0.28 0.30 0.34	1			1.55 1.45 1.31	
3.45 5.17 6.89	0.38 0.42 0.44				1.15 1.04 1.00	

Bou	ndary d mr			Bearing No.	Factor	Permissible radial load	Limiting speed
d	D	В	r (min.)		f_0	N	min ⁻¹
4	12	4	0.2	NCZ604 FA	12.4	7.5	1 000
	13	5	0.2	NCZ624 FA	12.3	10	1 000
5	14	5	0.2	NCZ605 FA	12.3	10	1 000
	16	5	0.2	NCZ625 FA	12.4	15	1 000
6	17	6	0.3	NCZ606 FA	12.2	15	1 000
	19	6	0.3	NCZ626 FA	12.3	20	1 000
7	19	6	0.3	NCZ607 FA	12.3	20	1 000
	22	7	0.3	NCZ627 FA	12.4	25	1 000
8	22	7	0.3	NCZ608 FA	12.4	25	1 000
	24	8	0.3	NCZ628 FA	12.8	25	1 000
9	24	7	0.3	NCZ609 FA	12.8	25	1 000
	26	8	0.6	NCZ629 FA	12.4	35	970
9.525	22.225	7.142	0.5	NCZEE3S FA	12.8	35	1 000
10	26	8	0.3	NCZ6000 FA	12.3	35	1 000
	30	9	0.6	NCZ6200 FA	13.2	50	860
12	28	8	0.3	NCZ6001 FA	13.2	40	830
	32	10	0.6	NCZ6201 FA	12.3	70	770
15	32	9	0.3	NCZ6002 FA	13.9	45	660
	35	11	0.6	NCZ6202 FA	13.2	75	610
17	35	10	0.3	NCZ6003 FA	14.4	50	580
	40	12	0.6	NCZ6203 FA	13.2	95	530
20	42	12	1	NCZ6004 FA	13.9	70	500
	47	14	0.6	NCZ6204 FA	13.2	130	450
25	47	12	1	NCZ6005 FA	14.5	75	400
	52	15	1	NCZ6205 FA	13.9	140	360
30	55	13	1	NCZ6006 FA	14.7	95	330
	62	16	1	NCZ6206 FA	13.9	195	300
35	62	14	1	NCZ6007 FA	14.9	110	280
	72	17	1.1	NCZ6207 FA	13.9	210	250
40	68	15	1	NCZ6008 FA	15.2	135	250
	80	18	1.1	NCZ6208 FA	14.0	230	220

* Colors in the "Bearing No." column indicate the classification of the periods for delivery as shown below.

Available from stock

30 days after receiving an order

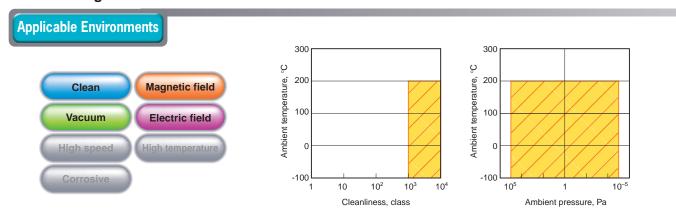
45 days after receiving an order

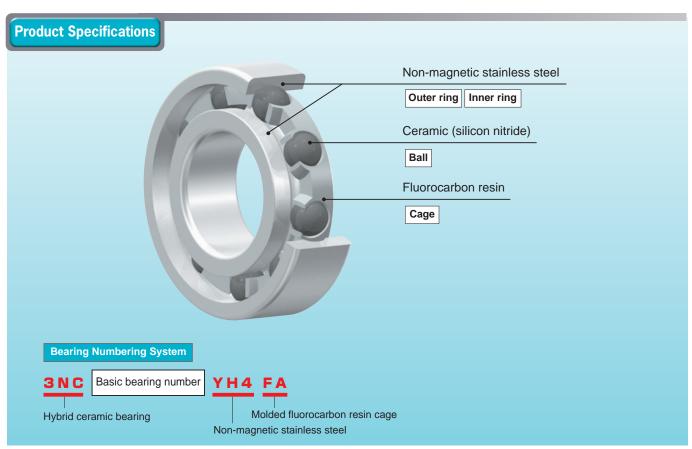
Determined after consultation on each inquiry

Non-magnetic Hybrid Ceramic Bearings

Non-magnetic Support in Stainless Steel

This bearing uses non-magnetic stainless steel. It includes fluoropolymer as the lubricant. This bearing can be used in a vacuum environment.



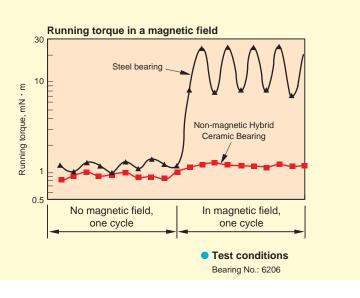


Applications

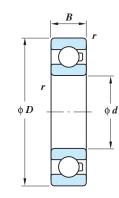
- Semiconductor manufacturing equipment Semiconductor inspection equipment Canning machinery
- Superconductivity-related equipment Welder

Performance

 While steel bearings experience fluctuating running torque, caused by magnetic fields, this bearing rotates at a stable torque.



Dimensions Table



Dynamic equivalent load
$$\begin{split} P_r &= XF_r + YF_a \\ &\quad (X \text{ and } Y \text{ are as shown below.}) \end{split}$$
 Static equivalent load $P_{0r} = 0.6F_r + 0.5F_a \\ &\quad \text{When } P_{0r} \text{ is smaller than } F_r. \\ P_{0r} &= F_r \end{split}$

f_0F_a	e	$\frac{F_{ m a}}{F_{ m r}}$	· ≤ <i>e</i>	$\frac{F_{\rm a}}{F_{\rm r}} > e$	
C_{0r}		X	Y	X	Y
0.172 0.345 0.689	0.19 0.22 0.26				2.30 1.99 1.71
1.03 1.38 2.07	0.28 0.30 0.34	1	0	0.56	1.55 1.45 1.31
3.45 5.17 6.89	0.38 0.42 0.44				1.15 1.04 1.00

* Colors in the "Bearing No." column indicate the classification of the periods for delivery as shown below.

	Available from stock
	30 days after receiving an order
	45 days after receiving an order
	Determined after consultation on each inc

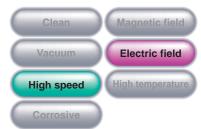
Boundary dimensions							
Бои	mm			Da selas Ma	Factor	Permissible radial load	Limiting speed
d	D	В	r	Bearing No.	£	l adiai ioad	specu
a	D	D	(min.)		f_0	N	min ⁻¹
4	12	4	0.2	3NC604YH4 FA	12.4	7.5	1 000
	13	5	0.2	3NC624YH4 FA	12.3	10	1 000
5	14	5	0.2	3NC605YH4 FA	12.3	10	1 000
	16	5	0.3	3NC625-5YH4 FA	12.4	15	1 000
6	17	6	0.3	3NC606YH4 FA	12.2	15	1 000
	19	6	0.3	3NC626YH4 FA	12.3	20	1 000
7	19	6	0.3	3NC607YH4 FA	12.3	20	1 000
	22	7	0.3	3NC627YH4 FA	12.4	25	1 000
8	22	7	0.3	3NC608YH4 FA	12.4	25	1 000
	24	8	0.3	3NC628YH4 FA	12.8	25	1 000
9	24	7	0.3	3NC609YH4 FA	12.8	25	1 000
	26	8	0.6	3NC629YH4 FA	12.4	35	970
9.525	22.225	7.142	0.5	3NCEE3SYH4 FA	12.8	35	1 000
10	26	8	0.3	3NC6000YH4 FA	12.3	35	1 000
	30	9	0.6	3NC6200YH4 FA	13.2	50	860
12	28	8	0.3	3NC6001YH4 FA	13.2	40	830
	32	10	0.6	3NC6201YH4 FA	12.3	70	770
15	32	9	0.3	3NC6002YH4 FA	13.9	45	660
	35	11	0.6	3NC6202YH4 FA	13.2	75	610
17	35	10	0.3	3NC6003YH4 FA	14.4	50	580
	40	12	0.6	3NC6203YH4 FA	13.2	95	530
20	42	12	0.6	3NC6004YH4 FA	13.9	70	500
	47	14	1	3NC6204YH4 FA	13.2	130	450
25	47	12	0.6	3NC6005YH4 FA	14.5	75	400
	52	15	1	3NC6205YH4 FA	13.9	140	360
30	55	13	1	3NC6006YH4 FA	14.7	95	330
	62	16	1	3NC6206YH4 FA	13.9	195	300
35	62	14	1	3NC6007YH4 FA	14.9	110	280
	72	17	1.1	3NC6207YH4 FA	13.9	210	250
40	68	15	1	3NC6008YH4 FA	15.2	135	250
	80	18	1.1	3NC6208YH4 FA	14.0	230	220

Hybrid Ceramic Bearings

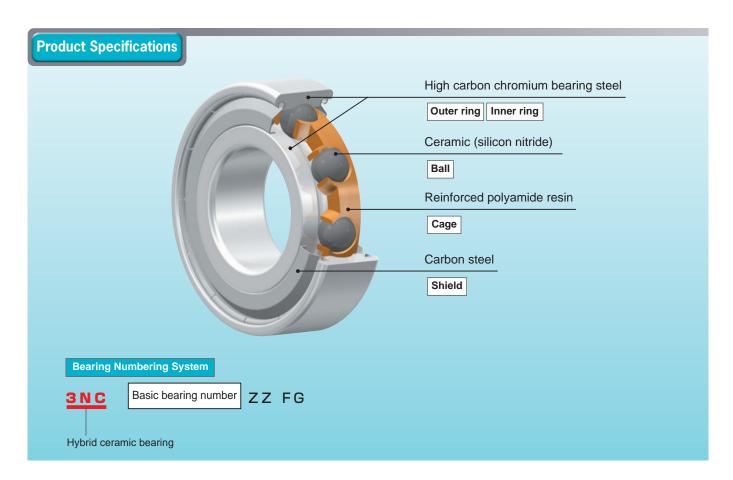
For Insulation and **High-speed Applications**

This bearing is a standard hybrid ceramic bearing. Lubricated with grease or oil, it can be used as an insulating bearing or high speed bearing.

Applicable Environments



- Temperature: 30 to 120°C
- Ambient pressure: Atmospheric pressure

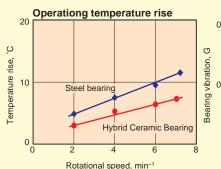


Applications

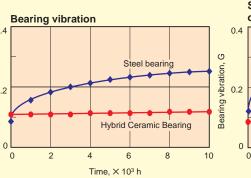
■ High speed stranding machine guide rollers ■ Motors ■ Generators

Performance

Reduced temperature rises.



Reduced bearing vibration.



Good antiseizure characteristics.



Test conditions

Bearing No.: 696 Temperature: 70°C Rotational speed: 15000 min⁻¹ Load (Preload) : 14.2 N (Position preloading)

Test conditions

Bearing No.: 695 Temperature: 70°C Rotational speed: 7200 min-1 Load (Preload): 14.7 N (Constant pressure preloading)

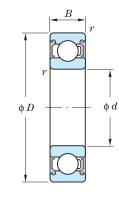
Dimensions Table

Load: Radial 2.94 kN

Test conditions

Bearing No.: 6312

Rotational speed: 2000~7000 min⁻¹



Dynamic equivalent load $P_{\rm r} = XF_{\rm r} + YF_{\rm a}$ (X and Y are as shown below.)

Static equivalent load $P_{0r} = 0.6F_r + 0.5F_a$

When P_{0r} is smaller than F_r . $P_{0r} = F_r$

f_0F_a	е	$\frac{F_{ m a}}{F_{ m r}}$	≤ <i>e</i>	$\frac{F_z}{F_z}$	->e
C_{0r}		X	Y	X	Y
0.172 0.345 0.689	0.19 0.22 0.26				2.30 1.99 1.71
1.03 1.38 2.07	0.28 0.30 0.34	1	0	0.56	1.55 1.45 1.31
3.45 5.17 6.89	0.38 0.42 0.44				1.15 1.04 1.00

- * Colors in the "Bearing No." column indicate the classification of the periods for delivery as shown below
- Available from stock 30 days after receiving an order 45 days after receiving an order
- Determined after consultation on each inquiry

	Boui	ndary di mn		ns	December No.		d ratings ¹⁾ :N	Factor	Limitin ç mir	
	d	D	В	r (min.)	Bearing No.	$C_{ m r}$	$C_{0{ m r}}$	f_0	Grease lubrication	Oil lubrication
	4	12	4	0.2	3NC604ZZC3 FG	0.97	0.30	12.4	63 000	75 000
		13	5	0.2	3NC624ZZC3 FG	1.30	0.40	12.3	52 000	64 000
	5	14	5	0.2	3NC605ZZC3 FG	1.30	0.40	12.3	60 000	72 000
		16	5	0.3	3NC625-5ZZC3 FG	1.75	0.55	12.4	48 000	58 000
	6	17	6	0.3	3NC606ZZC3 FG	1.95	0.60	12.2	51 000	61 000
		19	6	0.3	3NC626ZZC3 FG	2.60	0.90	12.3	42 000	51 000
	7	19	6	0.3	3NC607ZZC3 FG	2.60	0.90	12.3	48 000	56 000
		22	7	0.3	3NC627ZZC3 FG	3.30	1.15	12.4	37 000	44 000
	8	22	7	0.3	3NC608ZZC3 FG	3.30	1.15	12.4	40 000	49 000
		24	8	0.3	3NC628ZZC3 FG	3.35	1.20	12.8	33 000	42 000
	9	24	7	0.3	3NC609ZZC3 FG	3.35	1.20	12.8	39 000	48 000
		26	8	0.6	3NC629ZZC3 FG	4.55	1.65	12.4	32 000	39 000
	9.525	22.225	7.142	0.5	3NCEE3SZZC3 FG	3.35	1.20	12.8	39 000	48 000
	10	26	8	0.3	3NC6000ZZC3 FG	4.55	1.65	12.3	37 000	43 000
		30	9	0.6	3NC6200ZZC3 FG	5.10	2.05	13.2	28 000	34 000
_	12	28	8	0.3	3NC6001ZZC3 FG	5.10	2.05	13.2	32 000	38 000
		32	10	0.6	3NC6201ZZC3 FG	6.80	2.60	12.3	26 000	32 000
	15	32	9	0.3	3NC6002ZZC3 FG	5.60	2.40	13.9	27 000	32 000
		35	11	0.6	3NC6202ZZC3 FG	7.65	3.15	13.2	24 000	28 000
_	17	35	10	0.3	3NC6003ZZC3 FG	6.00	2.75	14.4	25 000	30 000
		40	12	0.6	3NC6203ZZC3 FG	9.55	4.10	13.2	20 000	25 000
_	20	42	12	0.6	3NC6004ZZC3 FG	9.40	4.30	13.9	20 000	25 000
		47	14	1	3NC6204ZZC3 FG	12.8	5.65	13.2	18 000	20 000
	25	47	12	0.6	3NC6005ZZC3 FG	10.1	4.95	14.5	18 000	21 000
		52	15	1	3NC6205ZZC3 FG	14.0	6.70	13.9	15 000	18 000
	30	55	13	1	3NC6006ZZC3 FG	13.2	7.00	14.7	15 000	18 000
		62	16	1	3NC6206ZZC3 FG	19.5	9.60	13.9	13 000	15 000
_	35	62	14	1	3NC6007ZZC3 FG	15.9	8.75	14.9	13 000	15 000
		72	17	1.1	3NC6207ZZC3 FG	25.7	13.1	13.9	11 000	13 000
_	40	68	15	1	3NC6008ZZC3 FG	16.7	9.80	15.2	12 000	14 000
		80	18	1.1	3NC6208ZZC3 FG	29.1	15.2	14.0	9 900	12 000
١	Note 1) Th	e basic le	oad rating	gs are the	ose of the Hybrid Ceramic	Bearing.				

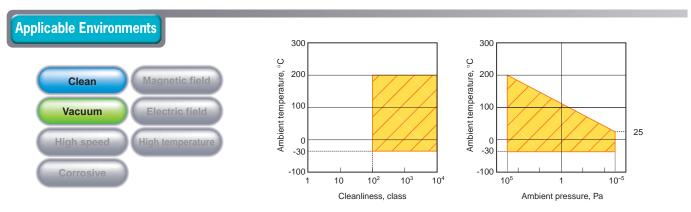
To calculate its dynamic equivalent radial load, multiply the C_{0r} values in this table by 1.176.

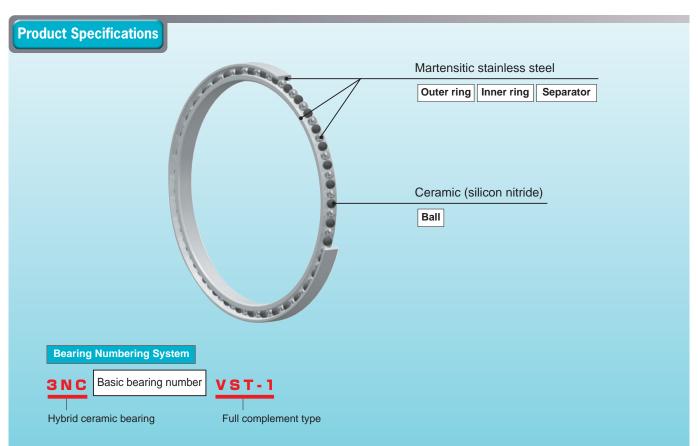
65

4 K Series Full Complement **Hybrid Ceramic Ball Bearings**

Clean Specification for Super Thin Section Ball Bearings

This bearing is based on the K series super thin section ball bearing, which is widely used in industrial robots. Provided with some adaptations, this bearing is compatible with clean or vacuum environments. It uses fluorinated KDL grease as the standard lubricant. However, please consult with us regarding Clean Pro and other solid lubricants.





Applications ■ Wafer transfer robot ■ Semiconductor manufacturing equipment ■ LCD manufacturing equipment

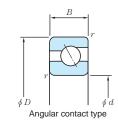
Types and Dimension Series

- The K series super thin section ball bearing is available in three types: deep groove type, angular contact type and four point contact type.
- The cross section can be selected from among three sizes: 4.762, 6.35 and 7.938 (mm).
- For use in a clean or vacuum environment, the angular contact type, which has stainless steel balls and ceramic balls alternately, is available in

Products not listed in the Dimensions Table are available to order. Please consult JTEKT.

		Ве	earing type co	de	
		C (Deep groove type)	A (Angular contact type)	X (4 point contact type)	
Dimension series code	Cross sectional dimension $B = E$ mm				Bore dia. mm
т	4.762	ктс	KTA	KTX	25.4, 38.1
Α	6.35	KAC	KAA	KAX	50.8 to
В	7.938	KBC	KBA	KBX	88.9

Dimensions Table



Dynamic equivalent load $P_{\rm r} = XF_{\rm r} + YF_{\rm a}$

(X and Y are as shown below.) Static equivalent load $P_{0r} = 0.6F_r + 0.5F_a$

When P_{0r} is smaller than F_r . $P_{0r} = F_r$

algi		Single	row or ta	ndem m	ounting	Back t	o back	or face t	to face	
Sontact angle	e	$\frac{F_{ m a}}{F_{ m r}}$	≤ <i>e</i>	$\frac{F_{\mathrm{a}}}{F_{\mathrm{r}}}$	> <i>e</i>	$\frac{F_{ m a}}{F_{ m r}}$	≤ <i>e</i>	$\frac{F_{ m a}}{F_{ m r}}$	> <i>e</i>	
Cor		X	$\frac{F_{\rm a}}{F_{\rm r}} \le e$ $X \qquad Y$		Y	X	Y	X	Y	
30°	0.80	1	0	0.39	0.76	1	0.78	0.63 1.24		

Sontact angle	Single tandem i	row or mounting	Back to face to	
න් රි	X_0	Y_0	X_0	Y_0
30°	0.5	0.33	1	0.66

Во	oundary di mn		ns	Bearing No.	Basic load	_
d	D	В	r (min.)	bearing No.	$C_{ m r}$	$C_{0\mathrm{r}}$
25.4	34.925	4.762	0.4	3NCKTA010VST-1	2.05	1.20
38.1	47.625	4.762	0.4	3NCKTA015VST-1	2.35	1.65
50.8	63.5	6.35	0.6	3NCKAA020VST-1	3.90	2.95
	63.5 6.35 66.675 7.938	7.938	1	3NCKBA020VST-1	5.40	3.80
63.5	76.2	6.35 0.6 3NCKAA025VST- 1	3NCKAA025VST-1	4.20	3.55	
	79.375	7.938	1	3NCKBA025VST-1	5.85	4.60
76.2	88.9	6.35	0.6	3NCKAA030VST-1	4.50	4.20
	92.075	7.938	1	3NCKBA030VST-1	6.25	5.45
88.9	101.6 6.35	6.35	0.6	3NCKAA035VST-1	4.80	4.90
	104.775	7.938	1	3NCKBA035VST-1	6.60	6.25

Note 1) The basic load ratings are those of bearing made from SUS440C.

*Colors in the "Bearing No." column indicate the classification of the periods for delivery as shown below.

Available from stock

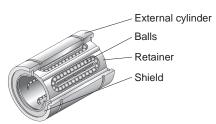
45 days after receiving an order

5

5 Linear Motion Bearings

Linear Motion Ball Bearings for Use in Extreme Special Environments

The linear motion ball bearings are a high precision product that moves linearly in axial directions while having rolling contact with the shaft. Having balls, retainer and shields housed in an external cylinder, this compact bearing moves linearly without limit to the stroke distance.





Bearing Types

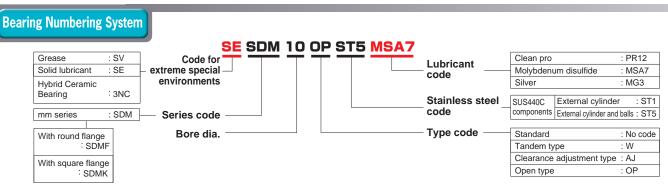
		DL Linear Motion Ball Bearing	Clean Pro Linear Motion Ball Bearing	MG Linear Motion Ball Bearing	MO Linear Motion Ball Bearing	Hybrid Ceramic Linear Motion Ball Bearing	
	External cylinder		Martensitic s	tainless steel		Martensitic stainless steel	
Material	Balls		Walteriside	tairiicaa ateer		Silicon nitride	
Mat	Retainer		Austenitic st	ainless steel		Austenitic stainless steel	
	Shields		Precipitation harde	ned stainless steel		Precipitation hardened stainless steel	
	Lubricant	KDL grease	Clean pro coating over the entire surface of all components	Silver ion plated balls	Molybdenum disulfide coated on the retainer surface	(Remark)	

Remark) Hybrid Ceramic Linear Motion Ball Bearings with grease lubrication or with Clean Pro coating are also available. Consult JTEKT regarding the applications of these bearings.

Applicable Environments

	DL Linear Motion Ball Bearing	Clean Pro Linear Motion Ball Bearing	MG Linear Motion Ball Bearing	MO Linear Motion Ball Bearing	Hybrid Ceramic Linear Motion Ball Bearing
Cleanliness	Class 100	Class 10	-	_	_
Temperature °C	- 30 to 200	- 100 to 200	- 200 to 300	- 100 to 300	- 30 to 300
Ambient pressure Pa	Normal to 10 ⁻⁵	Normal to 10 ⁻⁵	10 ⁻³ to 10 ⁻¹⁰	Normal to 10 ⁻⁵	Normal pressure

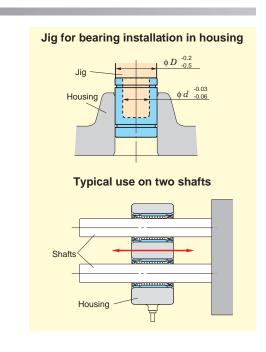
Performance Comparison in lubrication life **Test conditions** ϕ 10 \times ϕ 19 \times 29mm Tested bearing (bore dia. X outside dia. X width) Ambience Atmospheric air, class 10 Temperature Room temp 50N Load Speed 30mm/s No lubrication Clean Pro Linear MG Linear Motion Ball Bearing



- Note 1) This catalogue does not contain the dimensions tables of mm-series linear motion ball bearings (for Europe). Contact JTEKT for the dimensions.
 - 2) The clearance adjustment type (AJ) and open type (OP) are not compatible with tandem type and flanged type.

Bearing Mounting

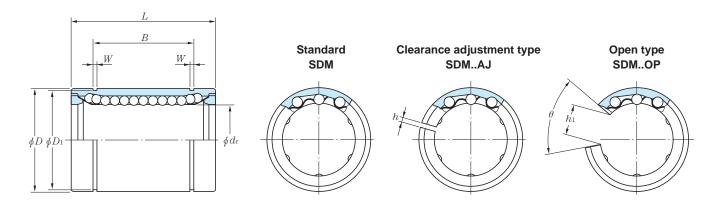
- 1) Linear motion ball bearings are constructed not to allow rotary motion but allow linear motion only.
- These bearings should carry loads evenly throughout their entire stroke; therefore, when the bearing is subjected to bending loads, mount two bearings at a distance on a shaft, or use a tandem type linear motion ball bearing.
- 2) When installing a linear motion bearing in a housing, press one end face of the external cylinder into the housing, taking care not to push or hit the shield, or insert the bearing softly using a jig as shown in the figure at right. When inserting a shaft, check the shaft for burrs or indentations in advance and insert it slowly so as not to deform the shaft. Chamfer the shaft end faces.
- 3) To support linear motion bearings built in a single housing on a set of two or more shafts, adjust the parallelism of the shafts while checking the smooth motion of the bearings. Imperfectly paralleled shafts may disturb smooth motion of the bearings or shorten their service life.



Linear Motion Bearings 61

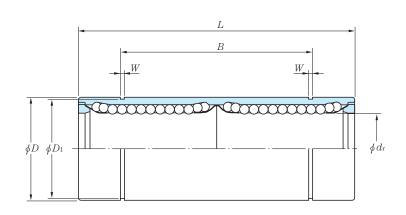
Dimensions Table

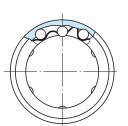
SDM Series



Shaft	Sta	andar	d	Clea adjustmer			Open ty	/pe (0	OP)				ı	Bour	ndary	dime	nsions	, mm						c load
$d_{ m r}$ mm	Basic bearing No.	No. of ball rows	Mass g	Basic bearing No.	No. of ball rows	Mass g	Basic bearing No.	No. of ball rows	Mass g	$d_{ m r}$	Tolerance µm	D	Tolerance µm	L	Tolerance µm	В	Tolerance µm	W	D_1	h	h_1	θ (degree)	rat C N	ing $egin{array}{c} C_0 \ N \end{array}$
3	SDM 3		1.4	-	-	-	-	-	-	3		7		10		-		-	-	-	-	-	69	105
4	SDM 4		2	-	-	-	-	-	-	4	0 -8	8	0 -9	12	0 -120	-	-	-	-	-	-	-	88	127
5	SDM 5		4	-	-	-	-	-	-	5		10		15		10.2		1.1	9.6	-	-	-	167	206
6	SDM 6		8.5	-	-	-	-	-	-	6		12		19		13.5		1.1	11.5	-	-	-	206	265
8	SDM 8S	4	11	-	-	-	-	-	-	8		15	0 -11	17		11.5		1.1	14.3	-	-	-	176	216
8	SDM 8	4	17	-	-	-	-	-	-	8		15		24		17.5		1.1	14.3	-	-	-	274	392
10	SDM10		36	-	-	-	-	-	-	10	0 -9	19		29	0	22	0 -200	1.3	18	-	-	-	372	549
12	SDM12		42	SDM12 AJ		41	SDM12 OP		32	12		21	0	30	-200	23		1.3	20	1.5	8	80	510	784
13	SDM13		49	SDM13 AJ	4	48	SDM13 OP	3	37	13		23	-13	32		23		1.3	22	1.5	9	80	510	784
16	SDM16		76	SDM16 AJ		75	SDM16 OP		58	16		28		37		26.5		1.6	27	1.5	11	80	774	1 180
20	SDM20	5	100	SDM20 AJ	5	98	SDM20 OP	4	79	20		32		42		30.5		1.6	30.5	1.5	11	60	882	1 370
25	SDM25		240	SDM25 AJ		237	SDM25 OP		203	25	0 -10	40	0 -16	59		41		1.85	38	2	12	50	980	1 570
30	SDM30		270	SDM30 AJ		262	SDM30 OP		228	30		45		64		44.5		1.85	43	2.5	15	50	1 570	2 740
35	SDM35		425	SDM35 AJ		420	SDM35 OP		355	35		52		70		49.5		2.1	49	2.5	17	50	1 670	3 140
40	SDM40	6	654	SDM40 AJ	6	640	SDM40 OP	5	546	40	0 -12	60	0 -19	80	-300	60.5	-300	2.1	57	3	20	50	2 160	4 020
50	SDM50		1 700	SDM50 AJ		1 680	SDM50 OP		1 420	50		80		100		74		2.6	76.5	3	25	50	3 820	7 940
60	SDM60		2 000	SDM60 AJ		1 980	SDM60 OP		1 650	60	0 -15	90	0 -22	110		85		3.15	86.5	3	30	50	4 700	10 000

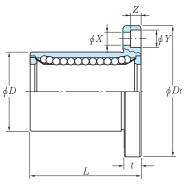
SDM..W series (Tandem type)

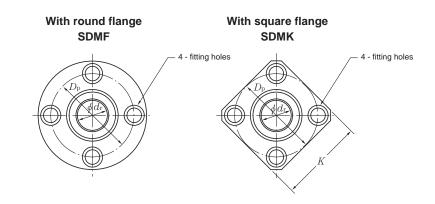




Shaft						Bour	ndary din	nensions	, mm				Pagia la	ad rating
$d_{ m r}$ mm	Basic bearing No.	Mass g	$d_{ m r}$	Tolerance	D	Tolerance	L	Tolerance	В	Tolerance µm	W	D_1	C	$ig C_0$
				μm		μm		μπ		μπ			N	N
5	SDM 5W	11	5		10	0 -11	28		20.4		1.1	9.6	265	412
6	SDM 6W	16	6		12	0	35		27		1.1	11.5	323	530
8	SDM 8W	31	8	0	15	-13	45		35		1.1	14.3	431	784
10	SDM10W	62	10	-10	19 21 0 23 -16	55	0 -300	44	0 -300	1.3	18	588	1 100	
12	SDM12W	80	12			0	57		46		1.3	20	813	1 570
13	SDM13W	90	13			61		46		1.3	22	813	1 570	
16	SDM16W	145	16		28		70		53		1.6	27	1 230	2 350
20	SDM20W	180	20		32		80		61		1.6	30.5	1 400	2 740
25	SDM25W	440	25	0 -12	40	0 -19	112		82		1.85	38	1 560	3 140
30	SDM30W	480	30		45		123		89		1.85	43	2 490	5 490
35	SDM35W	795	35		52		135		99		2.1	49	2 650	6 270
40	SDM40W	1 170	40	0 -15	60	0 -22	151	0 -400	121	0 -400	2.1	57	3 430	8 040
50	SDM50W	3 100	50		80	-22	192	-400	148	-400	2.6	76.5	6 080	15 900
60	SDM60W	3 500	60	0 -20	90	0 -25	209		170		3.15	86.5	7 550	20 000

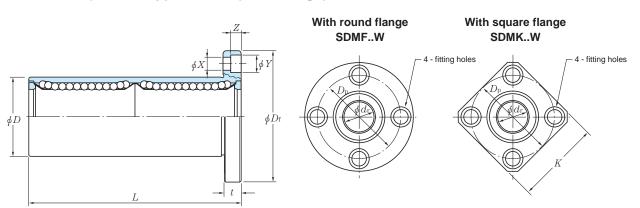
SDMF series (with round flange) SDMK series (with square flange)





Shaft							Boi	undary	dimen	sions,	mm					Eccen-	Square -	Basic lo	ad rating
$d_{ m r}$ mm	Basic bearing No.	Mass g	$d_{ m r}$	Tolerance µm	D	Tolerance µm	L	Tolerance µm	$D_{ m f}$	K	t	$D_{ m p}$	X	Y	Z	tricity (max.) µm	ness (max.) µ m	C N	C ₀
6	SDMF 6 SDMK 6	24 18	6		12		19		28	22	5	20	3.5	6	3.1			206	265
8	SDMF 8S SDMK 8S	32 24	8		15	0 -13	17		32	25	5	24	3.5	6	3.1			176	216
8	SDMF 8 SDMK 8	37 29	8		15		24		32	25	5	24	3.5	6	3.1			274	392
10	SDMF10 SDMK10	72 52	10	0 -9	19		29		40	30	6	29	4.5	7.5	4.1	12	12	372	549
12	SDMF12 SDMK12	76 57	12		21	0	30		42	32	6	32	4.5	7.5	4.1			510	784
13	SDMF13 SDMK13	88 72	13		23	-16	32		43	34	6	33	4.5	7.5	4.1			510	784
16	SDMF16 SDMK16	120 104	16		28		37	000	48	37	6	38	4.5	7.5	4.1			774	1 180
20	SDMF20 SDMK20	180 145	20		32		42	± 300	54	42	8	43	5.5	9	5.1			882	1 370
25	SDMF25 SDMK25	340 300	25	0 -10	40	0 -19	59		62	50	8	51	5.5	9	5.1	15	15	980	1 570
30	SDMF30 SDMK30	470 375	30		45		64		74	58	10	60	6.6	11	6.1			1 570	2 740
35	SDMF35 SDMK35	650 560	35		52		70		82	64	10	67	6.6	11	6.1			1 670	3 140
40	SDMF40 SDMK40	1 060 880	40	0 -12	60	0 -22	80		96	75	13	78	9	14	8.1	20	20	2 160	4 020
50	SDMF50 SDMK50	2 200 2 000	50		80		100		116	92	13	98	9	14	8.1			3 820	7 940
60	SDMF60 SDMK60	3 000 2 560	60	0 -15	90	0 -25	110		134	106	18	112	11	17	11.1	25	25	4 700	10 000

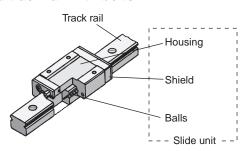
SDMF..W series (tandem type, with round flange) SDMK..W series (tandem type, with square flange)



Shaft							Bo	undary	dimen	sions,	mm					Eccen-		Basic lo	ad rating
$d_{ m r}$ mm	Basic bearing No.	Mass g	$d_{ m r}$	Tolerance µm	D	Tolerance µm	L	Tolerance µm	$D_{ m f}$	K	t	$D_{ m p}$	X	Y	Z	tricity (max.) µm	ness (max.) µ m	C N	C ₀
6	SDMF 6W SDMK 6W	31 25	6		12	0	35		28	22	5	20	3.5	6	3.1			323	530
8	SDMF 8W SDMK 8W	51 43	8		15	-13	45		32	25	5	24	3.5	6	3.1			431	784
10	SDMF10W SDMK10W	98 78	10	0	19		55		40	30	6	29	4.5	7.5	4.1	15	15	588	1 100
12	SDMF12W SDMK12W	110 90	12	-10	21	0	57		42	32	6	32	4.5	7.5	4.1	15	15	813	1 570
13	SDMF13W SDMK13W	130 108	13		23	-16	61		43	34	6	33	4.5	7.5	4.1			813	1 570
16	SDMF16W SDMK16W	190 165	16		28		70		48	37	6	38	4.5	7.5	4.1			1 230	2 350
20	SDMF20W SDMK20W	260 225	20		32		80	± 300	54	42	8	43	5.5	9	5.1			1 400	2 740
25	SDMF25W SDMK25W	540 500	25	0 -12	40	0 -19	112		62	50	8	51	5.5	9	5.1	20	20	1 560	3 140
30	SDMF30W SDMK30W	680 590	30		45		123		74	58	10	60	6.6	11	6.1			2 490	5 490
35	SDMF35W SDMK35W	1 020 930	35		52		135		82	64	10	67	6.6	11	6.1			2 650	6 270
40	SDMF40W SDMK40W	1 570 1 380	40	0 -15	60	0 -22	151		96	75	13	78	9	14	8.1	25	25	3 430	8 040
50	SDMF50W SDMK50W	3 600 3 400	50		80		192		116	92	13	98	9	14	8.1			6 080	15 900
60	SDMF60W SDMK60W	4 500 4 060	60	0 -20	90	0 -25	209		134	106	18	112	11	17	11.1	30	30	7 550	20 000

Linear Way Bearing Units for Use in Extreme Special Environments

The Linear Way Bearing Units have a slide unit in which balls circulate, allowing the slide unit to move linearly on the track rail without limit. High precision linear motion can be obtained easily by fixing the slide unit and track rail with bolts.





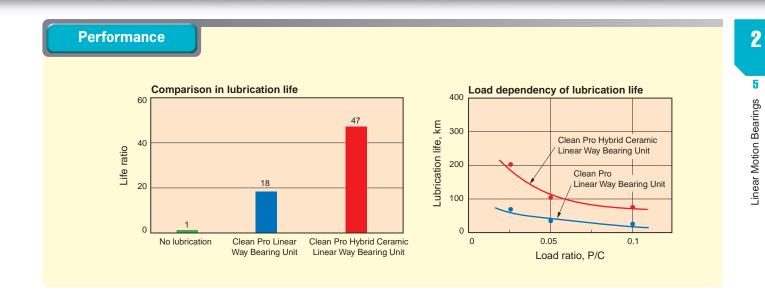
Bearing Types

		DL Linear Way Bearing Unit	Clean Pro Linear Way Bearing Unit	Hybrid Ceramic Linear Way Bearing Unit
	Housing			Martensitic stainless steel
Material	Track rail	Martensitic s	tainless steel	Marteristic stairiess steel
Mate	Balls			Silicon nitride
	Shields	Austenitic st	ainless steel	Austenitic stainless steel
	Lubricant	KDL grease	Clean pro coating over the entire surface of all components	(Remark)

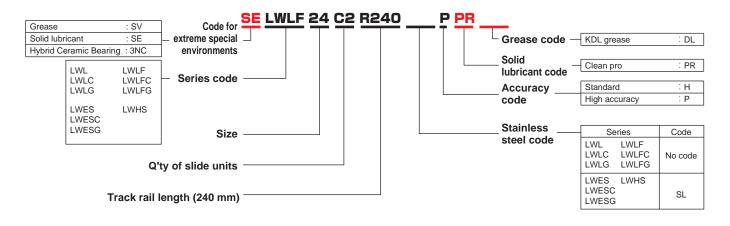
Remark) Hybrid Ceramic Linear Way Bearing Unit with grease lubrication or with Clean Pro coating are also available. Consult JTEKT regarding the use of these bearings.

Applicable Environments

	DL Linear Way Bearing Unit	Clean Pro Linear Way Bearing Unit	Hybrid Ceramic Linear Way Bearing Unit
Cleanliness	Class 100	Class 10	-
Temperature °C	- 30 to 200	- 100 to 200	- 30 to 200
Ambient pressure Pa	Normal to 10 ⁻⁵	Normal to 10 ⁻⁵	Normal pressure



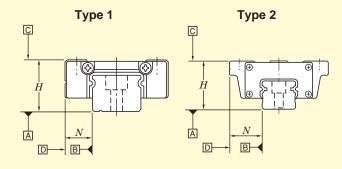
Bearing Numbering System



5

Linear Motion Bearings

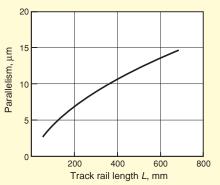
Tolerance (before surface treatmen



		Offic. Hilli
ltem	LWL LWLF LWLC LWLFC LWLG LWLFG (Type 1)	LWES LWHS LWESC LWESG (Type 2)
Tolerance of H Variation of $H^{(1)}$	± 0.020 0.015 max.	± 0.040 0.015 max.
Tolerance of N Variation of $N^{1)}$	± 0.025 0.020 max.	± 0.050 0.020 max.
Degree of running parallelism of plane ${\cal C}$ to plane ${\cal A}$ Degree of running parallelism of plane ${\cal D}$ to plane ${\cal B}$	Fig. 5-1	Fig. 5-2

Note 1) The variation refers to the dimensional difference between the slide units built into the

Remark) The preload is null or negligible.



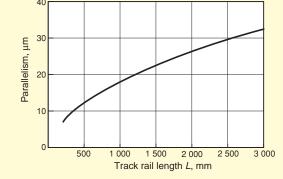


Fig. 5-1 Running parallelism of Linear Way Bearing Unit (Type 1)

Fig. 5-2 Running parallelism of Linear Way Bearing Unit (Type 2)

Bearing Mounting

- 1) Do not change the factory assembled combination of the slide
- Handle the linear way bearing units carefully to keep them out of oil stains and dust.
- 2) Before installing a linear way bearing unit in a machine or equipment, remove burrs and indentations from the contact surface of both the machine and bearing unit. Also remove dust, contamination and oil stains. Clean the recesses of the mounting surface (Fig. 5-3).

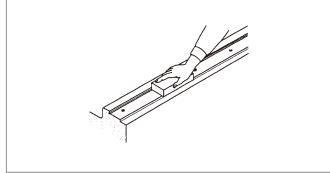


Fig. 5-3 Cleaning of the mounting surface

3) After positioning the mounting reference plane of the track rail correctly to the mounting reference plane of the bed, temporarily fasten the track to the bed (Fig. 5-4). Then bring the two planes into close contact, using a small vice or other suitable tool. Tighten the bolts one by one to securely fasten the drive side track rail to the bed (Fig. 5-5). The driven side track rail of the Linear Way Bearing Unit should be kept temporarily fastened.

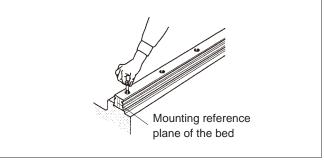


Fig. 5-4 Temporary fastening of the track rail

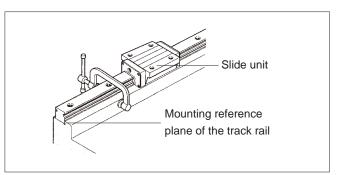


Fig. 5-5 Fastening of the drive side track rail

4) After positioning the slide units of the linear way bearing unit to the table, place the table carefully on the slide units and then temporarily fasten them together. Then align the mounting reference plane of the drive side slide units correctly with that of the table and fasten them together. With one of the driven side slide units positioned and fixed with respect to the moving direction, leave the other slide unit loosely tightened.

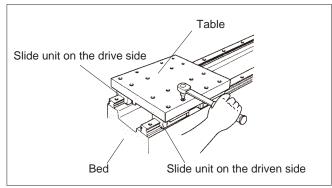


Fig. 5-6 Fastening of the slide unit

- 5) Before securely fastening the temporarily fastened track rail on the driven side, move the table and check that the motion is smooth. Tighten the fastening bolt that has just been passed over by the slide unit, thus fastening the track rail to the bed in a step-by-step manner (Fig. 5-7).
- Securely fasten the slide unit to the table, which has been kept temporarily fastened.

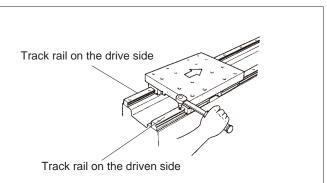
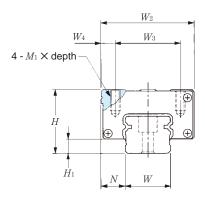
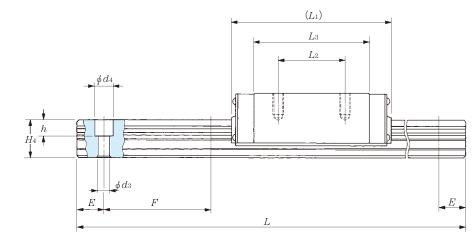


Fig. 5-7 Fastening of the driven side track rail

Dimensions Table

LWHS series

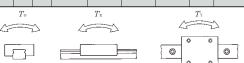




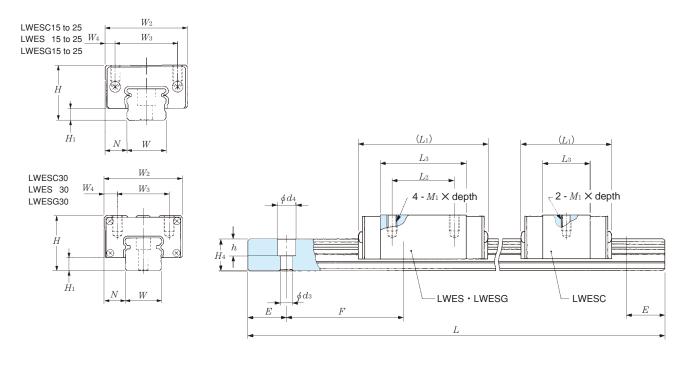
Basic No.	Slide	(refer.) Track		ensio semb mm	,	Rail width mm		Din	nens	ions m		ide u	nit	Di	mens		of tr	ack ı	ail	Track rail fastening bolt mm		Basic rat	load ing		atic beno	-
	unit kg	kg / m	Н	H_1	N	W	W_2	W_3	W_4	L_1	L_2	L_3	$M_1 \times \text{depth}$	H_4	d_3	d_4	h	E	F	$\begin{array}{c} \text{(nominal)} \\ \times \ \ell \end{array}$	mm	C N	$egin{array}{c} C_0 \ N \end{array}$	T_0 N· m	$T_{\rm x}$ N· m	$T_{ m Y}$ N· m
LWHS 15	0.18	1.47	24	6	9.5	15	34	26	4	66	26	44.6	M4× 8	15	4.5	8	6	30	60	M4×16	600	9 350	13 900	116	99.2 577	99.2 577
LWHS 20	0.36	2.56	30	7.5	12	20	44	32	6	83	36	57.2	M5×10	18	6	9.5	8.5	30	60	M5×18	600	14 500	21 900	241	202 1 130	202 1 130
LWHS 25	0.55	3.50	36	9	12.5	23	48	35	6.5	95	35	64.7	M6×12	22	7	11	9	30	60	M6×22	600	20 100	29 800	376	320 1 750	320 1 750
LWHS 30	1.00	4.82	42	10	16	28	60	40	10	113	40	80.6	M8×16	25	9	14	12	40	80	M8×28	600	28 100	42 200	646	556 2 930	556 2 930

Note 1) The illustrations at right show the directions of the static bending moment ratings T_0 , T_X , and T_Y .

Each of the upper values in the T_X and T_Y columns shows the bending moment for a single slide unit, and the lower value shows the bending moment for two slide units kept in close contact.



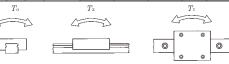
LWES series



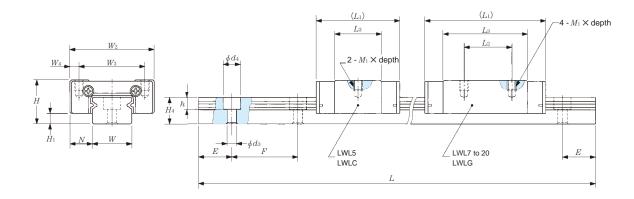
Basic No.	Slide	(refer.)		ensio semb mm	oly	Rail width mm		Dii	mens	sions o		ide u	nit	Di	mens		of tr	ack r	rail	Track rail fastening bolt mm	Max. track rail length	Basic rati			atic ben oment ra	-
	unit kg	rail kg/m	H	H_1	N	W	W_2	W_3	W_4	L_1	L_2	L_3	$M_1 \times depth$	H_4	d_3	d_4	h	E	F	$\begin{array}{c} \text{(nominal)} \\ \times \ \ell \end{array}$	L mm	C N	$egin{array}{c} C_0 \ N \end{array}$	T_0 N· m	$T_{\rm x}$ N· m	$T_{ m Y}$ N· m
LWESC15	0.09									41	-	22.4									600	4 330	5 680	45.4	22.1 155	22.1 155
LWES 15	0.14	1.57	24	5.8	9.5	15	34	26	4	57	26	38.4	M4× 7	14.5	3.6	6.5	4.5	20	60	M3×16	600	6 200	9 740	77.9	59.8 346	59.8 346
LWESG15	0.18									70	36	51.1									600	7 520	13 000	104	103 553	103 553
LWESC20	0.15									47	-	24.5									600	6 250	7 610	81.8	32.6 244	32.6 244
LWES 20	0.25	2.28	28	6	11	20	42	32	5	66.5	32	44	M5× 8	16	6	9.5	8.5	20	60	M5×16	600	9 360	13 900	150	99.2 582	99.2 582
LWESG20	0.33									82	45	59.9									600	11 500	19 000	204	178 952	178 952
LWESC25	0.26									59	-	32									600	10 100	12 800	159	74.5 498	74.5 498
LWES 25	0.42	3.09	33	7	12.5	23	48	35	6.5	83	35	56	M6× 9	19	7	11	9	20	60	M6×20	600	14 500	21 900	272	202 1 130	202 1 130
LWESG25	0.55									102	50	75									600	17 600	29 200	362	348 1 810	348 1 810
LWESC30	0.46									68	-	36									600	16 800	19 500	298	134 887	134 887
LWES 30	0.78	5.09	42	10	16	28	60	40	10	97	40	64.8	M8×12	25	7	11	9	20	80	M6×25	600	23 600	32 500	497	340 1 990	340 1 990
LWESG30	1.13									128.5	60	96.5									600	30 900	48 700	745	730 3 810	730 3 810

Note 1) The illustrations at right show the directions of the static bending moment ratings T_0 , T_x , and T_y .

Each of the upper values in the T_x and T_y columns shows the bending moment for a single slide unit, and the lower value shows the bending moment for two slide units kept in close contact.

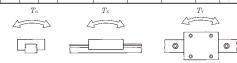


LWL series

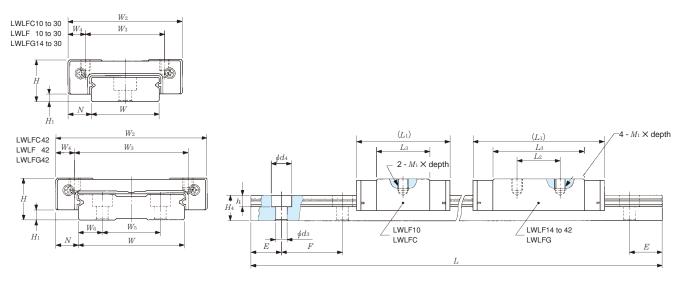


Basic No.	Mass (Track		nensi Issen mm	nbly	Rail width mm		Din	nens	ions mi		ide u	nit	Dii	mens		of ti	ack ı	rail	Track rail fastening bolt mm	Max. track rail length		load		atic ben	•
NO.	unit g	rail g/100mm	H	H_1	N	W	W_2	W_3	W_4	L_1	L_2	L_3	$M_1 \times \text{depth}$	H_4	d_3	d_4	h	$\mid E \mid$	$\mid F \mid$	(nominal) × ℓ	L mm	C N	C ₀	T_0 N· m	$T_{\rm x}$ N· m	T _Y N⋅ m
LWLC 5	3.4	12	6		3.5	5	12	8	2	16	-	9.6	M2×1.5	3.7	2.4	3.6	0.8	7.5	15	Cross recessed round head	210	514	872	2.3	1.4 8.9	1.2 7.4
LWL 5	4.4	12	О		3.5	5	12	0	2	19	-	12.6	IVIZAT.J	3.7	2.4	3.0	0.8	7.5	15	screw M2×6	210	612	1 130	3.0	2.4 13.3	2.0 11.2
LWLC 7	7.1									19	-	9.6								Hexagon		856	1 180	4.3	1.9 15.4	1.6 12.9
LWL 7	10	22	8	1.5	5	7	17	12	2.5	23.5	8	14.3	M2×2.5	5	2.4	4.2	2.3	7.5	15	socket head cap bolt	300	1 200	1 960	7.2	4.9 29.2	4.1 24.5
LWLG 7	14									31	12	21.6								M2×6		1 510	2 750	10.0	9.1 52.6	7.7 44.1
LWLC 9	11									21.5	-	11.9								Hexagon socket		1 070	1 540	7.2	3.0 22.2	2.5 18.6
LWL 9	19	35	10	2	5.5	9	20	15	2.5	30	10	20.8	M3×3	6	3.5	6	3.5	10	20	head cap	600	1 610	2 860	13.3	9.4 53.0	7.9 44.5
LWLG 9	28									40.5	15	30.9								M3×8		2 080	4 180	19.4	19.4 102	16.3 85.6
LWLC12	22									25	-	13								Hexagon socket		2 000	2 470	15.3	5.5 43.3	4.7 36.3
LWL 12	35	65	13	3	7.5	12	27	20	3.5	34	15	21.6	M3×3.5	8	3.5	6.5	4.5	12.5	25	head cap	600	2 960	4 450	27.6	16.0 96.6	13.4 81.1
LWLG12	51									44	20	32								M3×8		3 780	6 430	39.9	31.8 174	26.7 146
LWLC15	42									32	-	17.7								Hexagon		3 120	4 040	31.1	12.1 87.6	10.2 73.5
LWL 15	64	107	16	4	8.5	15	32	25	3.5	42	20	27.8	M3×4	10	3.5	6.5	4.5	20	40	socket head cap bolt	600	4 390	6 730	51.8	30.8 178	25.9 149
LWLG15	95									57	25	42.7								M3×10		5 750	10 100	77.7	66.2 351	55.6 294
LWLC20	89									38	-	22.3								Hexagon socket		4 070	5 490	56.0	20.2 138	16.9 116
LWL 20	133	156	20	5	10	20	40	30	5	50	25	34.6	M4×6	11	6	9.5	5.5	30	60	head cap	600	5 830	9 420	96.1	54.6 291	45.8 244
LWLG20	196									68	30	52.3								M5×14		7 350	13 300	136	106 549	88.9 461

Note 1) The illustrations at right show the directions of the static bending moment ratings T_0 , T_X , and T_Y . Each of the upper values in the T_X and T_Y columns shows the bending moment for a single slide unit, and the lower value shows the bending moment for two slide units kept in close contact.

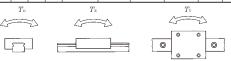


LWLF series



Basic No.	Mass (Track		nensi Isser mm	nbly	Rail width mm		Dir	nens	ions m		ide u	ınit		Dim	nens		of t	rack	rail		Track rail fastening bolt mm	Max. track rail length	Basic rat	load		c benc	-
1101	unit g	rail g/100mm	Н	H_1	N	W	W_2	W_3	W_4	L_1	L_2	L_3	$M_1 \times \text{depth}$	H_4	W_5	W_6	d_3	d_4	h	E	F	$\begin{array}{c} \text{(nominal)} \\ \times \ \ell \end{array}$	L mm	C N	C ₀	T_0 N· m	T _x N⋅ m	T _Y N⋅ m
LWLFC10	5.9	28	6.5	1.5	3.5	10	17	13	2	20.5	-	13.6	M2.5×1.5	1	_	_	2.9	4.8	16	10	20	Cross recessed round head	300	643	1 220	6.3	2.7 15.4	2.3 13.0
LWLF 10	7.5	20	0.5	1.5	0.0	10	17	10		24.5	-	17.6	INIZ.OZ VI.O	7			2.3	4.0	1.0	10	20	screw M2.5×7	300	760	1 570	8.1	4.4 23.3	3.7 19.5
LWLFC14	13									22.5	-	13										Hexagon socket		1 120	1 770	12.6	4.0 25.6	3.3 21.4
LWLF 14	21	54	9	2	5.5	14	25	19	3	31.5	10	22	M3×3	5.5	-	-	3.5	6	3.2	15	30	head cap bolt	300	1 580	2 940	21.0	10.4 56.7	8.7 47.6
LWLFG14	31									42	19	32.5										M3×8		2 040	4 320	30.9	21.8 108	18.3 90.8
LWLFC18	26							21	4.5	26.5	-	16.6										Hexagon socket		1 360	2 200	20.1	5.8 37.2	4.8 31.3
LWLF 18	44	90	12	3	6	18	30			39	12	28.6	M3×3	7	_	-	3.5	6.5	4.5	15	30	head cap bolt	600	2 010	3 960	36.2	17.5 93.4	14.7 78.4
LWLFG18	61							23	3.5	50.5	24	40.4										M3×8		2 500	5 500	50.3	33.0 165	27.7 139
LWLFC24	45									30.5	-	17.7										Hexagon socket		2 500	3 460	42.2	10.1 70.2	8.5 58.9
LWLF 24	76	139	14	3	8	24	40	28	6	44	15	31	M3×3.5	8	-	-	4.5	8	4.5	20	40	head cap bolt	600	3 780	6 430	78.4	31.8 174	26.7 146
LWLFG24	111									59	28	46.3										M4×10		4 870	9 400	115	65.6 333	55.0 280
LWLFC30	70									35.5	-	20.5										Hexagon socket		3 460	4 710	71.6	16.0 111	13.4 93.2
LWLF 30	112	198	15	3	10	30	50	35	7.5	50	18	34.8	M4×4.5	9	-	-	4.5	8	4.5	20	40	head cap bolt	600	5 230	8 750	133	50.5 269	42.4 226
LWLFG30	170									68.5	35	53.8										M4×12		6 730	12 800	194	104 526	87.4 442
LWLFC42	95									41.5	-	25.3										Hexagon socket		4 450	6 280	133	25.7 170	21.6 143
LWLF 42	140	294	16	4	9	42	60	45	7.5	55	20	39	M4×4.5	10	23	9.5	4.5	8	4.5	20	40	head cap bolt	600	6 150	10 200	216	63.6 346	53.3 290
LWLFG42	204									74.5	35	58.3										M4×12		7 910	14 900	316	131 668	110 561

Note 1) The illustrations at right show the directions of the static bending moment ratings T_0 , T_X , and T_Y . Each of the upper values in the T_X and T_Y columns shows the bending moment for a single slide unit, and the lower value shows the bending moment for two slide units kept in close contact.



: No code

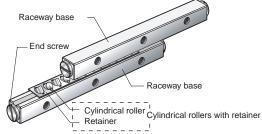
SP

: SL

Cross Roller Way Bearing Units for Use in Extreme Special Environments

The Cross Roller Way Bearing Unit is a linear motion bearing unit consisting of two raceway bases. Each base has one longitudinal plane cut into a V shape, which serves as the rolling surface. Two bases are in contact on each of the other's V-cut surface, and cylindrical rollers with a retainer are placed between the surfaces. Any pair of adjacent cylindrical rollers is directed at right angles to each other, thus enabling smooth and extremely accurate linear motion.





Bearing Types

		DL Cross Roller Way Bearing Unit	Clean Pro Cross Roller Way Bearing Unit	MO Cross Roller Way Bearing Unit
Material	Raceway base Cylindrical rollers		Martensitic stainless steel	
Mate	Retainer		Austenitic stainless steel	
	End screw			
	Lubricant	KDL grease	Clean pro coating over the entire surface of all components	Molybdenum disulfide coating on the raceway bases

Applicable Environments

	DL Cross Roller Way Bearing Unit	Clean Pro Cross Roller Way Bearing Unit	MO Cross Roller Way Bearing Unit
Cleanliness	Class 100	Class 10	_
Temperature °C	- 30 to 200	- 100 to 200	- 100 to 300
Ambient pressure Pa	Normal to 10 ⁻⁵	Normal to 10 ⁻⁵	Normal to 10 ⁻⁵

Grease : SV | Solid lubricant : SE | CRW 3-75 C20 SL SP | PR | Grease code | KDL grease : DL | Clean pro : PR | Grease code | Molybdenum disulfide : MSA | Molybdenum disulfide : MSA | Clean pro : PR | Clean pro : MSA | Clean pro : MS

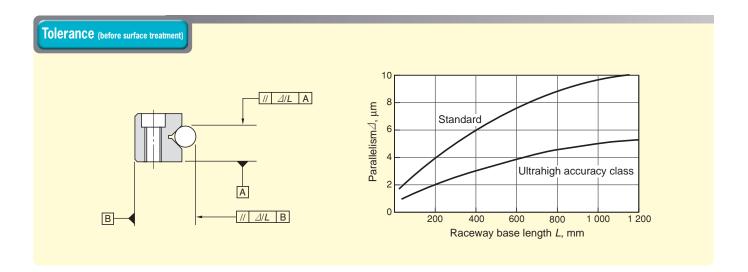
Accuracy

Standard

Material code — Stainless steel

Ultrahigh accuracy

Note) This bearing number represents four raceway bases and two sets cylindrical rollers with retainer.



Bearing Mounting

Bearing Numbering System

Diameter of rollers

Raceway base length

Q'ty of rollers per unit

Fig. 5-8 shows a typical mounting construction of the Cross Roller Way Bearing Unit. Mounting procedures are described on the following page.

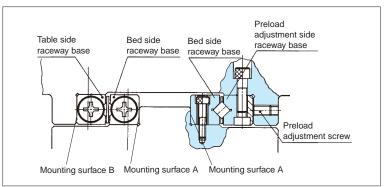


Fig. 5-8 Typical mounting of Cross Roller Way Bearing Unit

5

inear Motion Bearings

- 1) One package includes an entire set of the components of a cross roller way bearing unit (four raceway bases and two sets of cylindrical rollers with retainer). Take care not to mix the components of a set not compatible with those of another set. Treat cross roller way bearing units with extra care to keep them free from oil stains or contamination.
- 2) Remove burrs, indentations and other irregularities from the machine surface on which the cross roller way bearing unit is to be mounted. Also clean off dust, contamination and oil stains. Clean the recesses of the mounting surface as well.
- 3) Place the bed side raceway base and table side raceway base correctly on the each mounting surface, and fasten the bases temporarily by tightening the screws evenly.
- While keeping the bed side raceway base in close contact with surface A and the table side raceway base with surface B, tighten the screws permanently to a specified torque (Fig. 5-9). Table 5-1 shows the tightening torque for individual regular screw sizes.

Table 5-1 Screw tightening torque

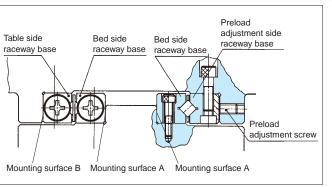
Nominal screw size	Tightening torque N ⋅ m
M2×0.4	0.23
M3×0.5	1.4
M4×0.7	3.2
M5×0.8	6.3
M6×1	10.7

Remark) When screws of different sizes are used for on the table side and bed side, tighten them by applying the torque for the smaller screws.

- 4) Retract the preload adjustment screw in advance. Place the preload adjustment side raceway base into close contact with the mounting surface, and tighten the screws temporarily by applying light, even torque.
- 5) To assemble the table and bed, insert cylindrical rollers with retainer carefully into the space between the table side raceway base and bed side raceway base such that the rollers will be located at the center of the raceway base length. Take care not to deform the cage.

Fasten the end screws and end plates of the raceway bases, press the entire table toward the preload adjustment screw side, and tighten the screw for temporary adjustment until the clearance of the raceways is almost entirely eliminated.

Slowly move the table for one entire stroke and adjust the position of the cylindrical rollers with retainer to the center.



(Fig. 5-8 Typical mounting of Cross Roller Way Bearing Unit)

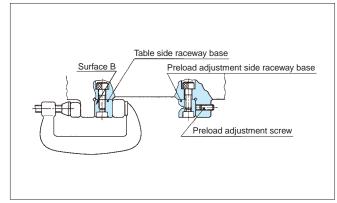


Fig. 5-9 Mounting of table side raceway base

6) Adjust the preload with the preload adjustment side raceway base fastened temporarily.

Firstly adjust the preload adjustment screw at the center of the raceway base length, and adjust the preload adjustment screws on the lengths to both ends alternately. Adjust the clearance on the side face of the table, and tighten the preload adjustment screws one by one until the dial gauge indication becomes stable (Fig. 5-10).

When the indication is stable, determine and record the tightening torque of the preload adjustment screws. To adjust the preload adjustment screws near both ends, stroke the table slowly to check that cylindrical rollers are located at the preload adjustment screw.

After these adjustments, the clearance will be entirely or almost eliminated. However, at this point the preload is not yet even. By repeating the same procedure, re-adjust all the preload adjustment screws by applying the torque recorded.

7) When permanently fastening the preload adjustment side raceway base, make sure the screws have already been lightly tightened to even torque.

In the same manner as the preload adjustment screws were tightened, firstly adjust the preload adjustment screw at the center of the raceway base length, and adjust the preload adjustment screws on the lengths to both ends alternately by applying torque close to the specified torque.

To tighten the fastening screws near the ends, stroke the table slowly to check that the cylindrical rollers are located at the tightened screw position.

In the end, tighten all screws evenly and permanently by applying specified torque. Move the table slowly through the entire stroke and check that it moves smoothly without producing noise.

Check the table upper surface and side faces with a dial gauge to check running accuracy.

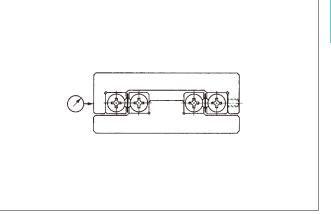


Fig. 5-10 Typical preload adjustment procedure

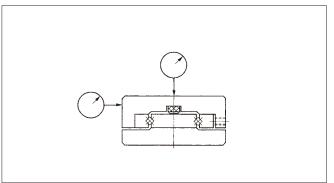
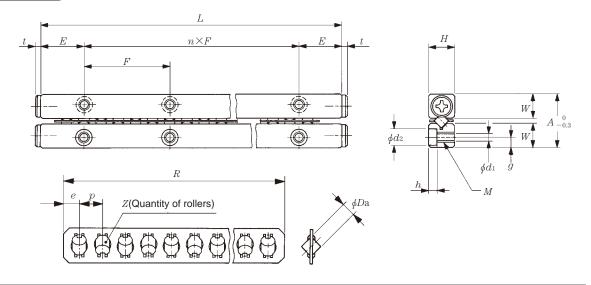


Fig. 5-11 Accuracy check after assembly

CRW series

Dimensions Table



		(refer.) Cylindrical	В	ounc	lary dimension	ıs	D		ns of cyli		al		Мо	untin	_	nensi	ons			load ing	Allowable
Basic No.	Raceway base 1)	rollers with			mm				mm						mm				Cu 3)	C _{0u} 3)	Fu 3)
	kg/m	retainer 2) g	A	Н	$L(n \times F)$	E	$D_{\rm a}$	R	Z	p	e	W	g	M	d_1	d_2	h	t	N	N	N
CRW1 - 20					20 (1×10)			16.5	5												
- 30					30 (2×10)			25.5	8												
- 40					40 (3×10)			31.5	10												
- 50	0.12	0.38	8.5	4	50 (4×10)	5	1.5	37.5	12	3	2.25	3.9	1.8	M2	1.65	3	1.4	1.7	131	119	39.4
- 60					60 (5×10)			43.5	14												
- 70					70 (6×10)			52.5	17												
80					80 (7×10)			61.5	20												
CRW2 - 30					30 (1×15)			29.6	7												
- 45					45 (2×15)			41.6	10												
- 60					60 (3×15)			53.6	13												
- 75					75 (4×15)			65.6	16												
- 90					90 (5×15)			77.6	19												
-105	0.24	0.98	12	6	105 (6×15)	7.5	2	89.6	22	4	2.8	5.5	2.5	M3	2.55	4.4	2	1.5	305	292	97.3
-120					120 (7×15)			101.6	25												
-135					135 (8×15)			113.6	28												
-150					150 (9×15)			125.6	31												
-165					165 (10×15)			137.6	34												
-180					180 (11×15)			149.6	37												
CRW3 - 50					50 (1×25)			42	8												
- 75					75 (2×25)			62	12												
-100					100 (3×25)			82	16												
-125					125 (4×25)			102	20												
-150					150 (5×25)			122	24												
-175	0.50	2.96	18	8	175 (6×25)	12.5	3	142	28	5	3.5	8.3	3.5	M4	3.3	6	3.1	2	664	606	202
-200					200 (7×25)			162	32												
-225					225 (8×25)			182	36												
-250					250 (9×25)			202	40												
-275					275 (10×25)			222	44												
-300					300 (11×25)			242	48												

Notes 1) Mass per meter of raceway base length

Mass of an assembly of a cage and ten cylindrical rollers

3) Load per cylindrical roller

		((·)																			
	Mass ((refer.) Cylindrical	В	ound	ary dimension	าร	D	imension	ns of cyli with reta		al		Мо	untin	g din	nensi	ons			load ing	Allowable load
Basic No.	Raceway	rollers			mm			rollers	mm reta	imer					mm					ı	Fu 3)
	base 1) kg/m	with retainer 2)			_ , ,				l	I	l		I		I	I		l	Cu 3)	C _{0u} 3)	
	kg / III	g	A	H	$L(n \times F)$	E	$D_{\rm a}$	R	Z	p	e	W	g	M	d_1	d_2	h	t	N	N	N
CRW4 - 80					80 (1×40)			73	10												
-120					120 (2×40)			101	14												
-160					160 (3×40)			136	19												
-200					200 (4×40)			164	23												
-240					240 (5×40)			199	28												
-280	0.82	6.91	22	11	280 (6×40)	20	4	227	32	7	5	10	4.5	M5	4.3	7.5	4.1	2	1 290	1 170	389
-320					320 (7×40)			262	37												
-360					360 (8×40)			297	42												
-400					400 (9×40)			325	46												
-440					440 (10×40)			360	51												
-480					480 (11×40)			388	55												
CRW6 -100					100 (1×50)			84	9												
-150					150 (2×50)			129	14												
-200					200 (3×50)			165	18												
-250					250 (4×50)			210	23												
-300					300 (5×50)			246	27												
-350	1.57	20.3	31	15	350 (6×50)	25	6	282	31	9	6	14	6	M6	5.3	9.5	5.2	3	2 680	2 290	764
-400					400 (7×50)			327	36												
-450					450 (8×50)			363	40												
-500					500 (9×50)			408	45												
-550					550 (10×50)			444	49												
-600					600 (11×50)			489	54												

Notes 1) Mass per meter of raceway base length

2) Mass of an assembly of a cage and ten cylindrical rollers

3) Load per cylindrical roller

6 Wigh Ability Angular Contact Ball Bearings

The High Ability Angular Contact Ball Bearings are optimized for the spindle of machine tools. They have superior high speed performance and rapid acceleration/deceleration, and are especially excellent at ultrahigh speeds under oil/air lubrication. They are superior in high speed performance to conventional products under grease lubrication as well.

For practical use of this type of bearings, refer to JTEKT Catalogue "Precision Ball and Roller Bearings for Machine Tools" (CAT. NO. B2005E) for High Ability Angular Contact Ball Bearings.



Types and Applications

The High Ability Angular Contact Ball Bearings are classified as shown in Table 6-1, according to bearing construction and rolling element material.

Select the optimal type best suited for your application needs.

Table 6-1 Classification of High Ability Angular Contact Ball Bearings

Tune		Specifications		Application
Туре	Bearing dimension series No.	Contact angle	Rolling element material	- Application
Type R	10 19	15° 20° 30°	Steel or ceramic	High speed, high rigidity type
Type C	10 19	15° 20°	Ceramic	High speed, high load rating type
Type D	10	20°	Ceramic	Ultrahigh speed, low noise type For oil/air lubrication
Type F	10 19	20°	Ceramic	Ultrahigh speed type For oil/air lubrication

Features

20 to 30% reduction in temperature increase

(compared with JTEKT's conventional products)

JTEKT has conducted various tests and analyses and developed elaborate machining techniques to improve the performance of bearings used with machining tool spindles. The result is a substantial reduction in frictional heat generated in bearings rotating at a high speed.

• 1.2- to 1.5- fold increases in speed limits

(compared with JTEKT's conventional products)

Speed limits have been extended through re-designing for high-speed rotation and heat reduction. Use of ceramic balls as rolling elements enables additional high-speed rotation.

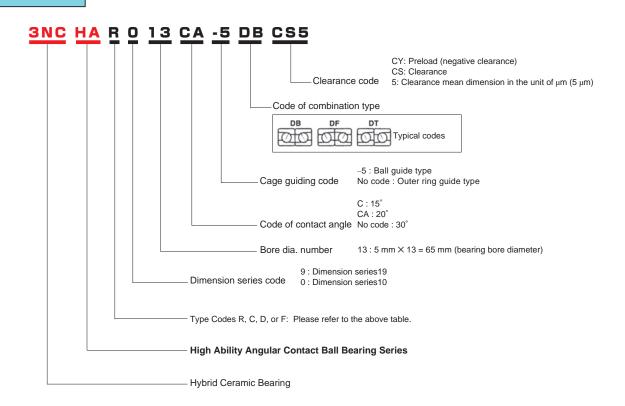
Improved high speed performance achieved by position preloading

Low increases in temperature during operation ensure reduced changes in preload. Preload can be given by position preloading even at high speeds, which has been hitherto unavailable with conventional systems. The result is high-precision machining with stability.

Conventional bearings easily replaced

Dimensions of High Ability bearings conform to ISO standards. Replacement of conventional bearings with High Ability bearings requires minimal geometry changes of the present spindle or housing.

Bearing Numbering System



Performance

High Ability Bearings demonstrate their utmost performance when two or more units are used together and a preload is provided by the position preloading method. The following are the performance of these bearings preloaded by the position preloading method.

High speed performance of Type R and Type C High Ability Bearings

Fig. 6-1 shows the relationship between rotational speed and bearing temperature rises of High Ability Bearings, in comparison with conventional high precision bearings.

In either grease lubrication or oil/air lubrication, the High Ability Bearings are superior to conventional bearings, with lower temperature rise and higher rotational speed limit.

By using High Ability Bearings, it is possible to switch the spindle, which had been running with oil/air lubrication up until now, to grease lubrication.

Fig. 6-2 shows evaluation examples of this.

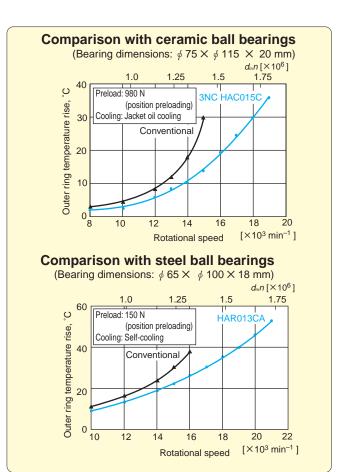


Fig. 6-1 Comparison in bearing temperature rises under oil air lubrication

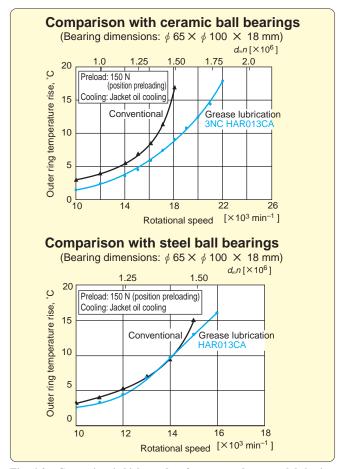


Fig. 6-2 Comparison in high speed performance under grease lubrication

The Type R using ceramic balls, in grease lubrication, improves on high-speed performance over conventional bearings with oil/air lubrication.

The high-speed performance of the Type R using steel balls, in grease lubrication, is the same as or better than that of conventional bearings with oil/air lubrication.

Fig. 6-3 shows the result of the comparison between ceramic balls and bearing steel balls.

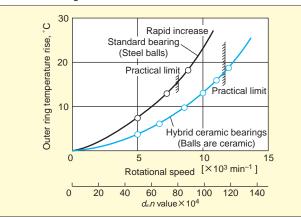


Fig. 6-3 Comparison of temperature rise characteristics between hybrid ceramic bearings and standard bearings

7 Ceramic Balls

JTEKT also supplies Ceramic Balls (silicon nitride), which have excellent resistance to wear and seizure, and are usable in corrosive environments and ultrahigh vacuums. Other major features of these balls are excellent heat resistance (up to 800°C), high rigidity, lightweight (40% compared to bearing steel), non-magnetic, and have insulating characteristics.

The Ceramic Balls are useful in many applications such as jigs, tools, gauges, solenoid valves, check valves, other valve varieties, high grade bicycle parts, automotive parts, and machine components.



Table of Dimensions and Masses

Nominal o	dimension	Nominal outside diameter	Precision	Mass ²⁾
mm	inch	mm	grade 1)	(per piece)
0.8		0.800 00		0.866 mg
1.0		1.000 00		1.691 mg
1.2		1.200 00		2.922 mg
	1/16	1.587 50		6.766 mg
2.0		2.000 00		13.530 mg
	3/32	2.381 25		22.836 mg
	7/64	2.778 12	3 and 5	36.262 mg
	1/8	3.175 00	3 and 5	54.129 mg
3.5		3.500 00		72.511 mg
	5/32	3.968 75		0.105 7 g
	3/16	4.762 50		0.182 7 g
	7/32	5.556 25		0.290 1 g
	15/64	5.953 12		0.356 8 g
	1/4	6.350 00		0.433 0 g
	17/64	6.746 88		0.519 4 g
	9/32	7.143 75		0.616 6 g
	5/16	7.937 50	5	0.845 8 g
	11/32	8.731 25	3	1.125 7 g
	3/8	9.525 00		1.461 5 g
	13/32	10.318 75		1.858 2 g

Notes	1) For	the grades, tho	se specified in JIS	B 1501	shall apply.	
	2) The	massas ara ca	alculated on the ha	eie of 3	23 a/cm ³ in	dancit

Nominal o	limension	Nominal outside diameter	Precision	Mass 2)
mm	inch	mm	grade 1)	(per piece)
	7/16	11.112 75		2.320 8 g
	15/32	11.906 25	5 and 10	2.854 5 g
	1/2	12.700 00	5 and 10	3.46 g
	17/32	13.493 75		4.2 g
	9/16	14.287 50		4.9 g
	19/32	15.081 25		5.8 g
	5/8	15.875 00		6.8 g
	3/4	19.050 00		11.7 g
	13/16	20.637 50	40	14.9 g
	7/8	22.225 00	40	18.6 g
	15/16	23.812 50		22.8 g
	1	25.400 00		27.7 g
	1 1/8	28.575 00		39.5 g
	1 3/16	30.162 50		46.4 g
	1 1/4	31.750 00		54.1 g
	1 5/16	33.337 50	60	62.7 g
	1 1/2	38.100 00		93.5 g

Numbering System

5/32 G5 NCR

Material code: silicon nitride ceramic

Precision grade code

Nominal dimension

Tolerance and Internal Clearance of Ceramic Bearings and **EXSEV** Bearings

8-1 Tolerance of Radial Ball Bearings

Table 8-1(1) Inner ring (bore diameter)

Unit: µm

Nomina diam	eter	Sing	gle plane	mean bo	re diame	ter devia	tion		ŭ	radial p s 7, 8, 9		ore dia eter seri				sp s 2, 3, 4		re diameter $V_{d{ m mp}}$	r variation
m		clas	ss 0	clas	ss 6	clas	ss 5	class 0	class 6	class 5	class 0	class 6	class 5	class 0	class 6	class 5	class 0	class 6	class 5
over	up to	upper	lower	upper	lower	upper	lower		max.			max.			max.	•		max.	
0.61)	2.5	0	- 8	0	- 7	0	– 5	10	9	5	8	7	4	6	5	4	6	5	3
2.5	10	0	- 8	0	- 7	0	- 5	10	9	5	8	7	4	6	5	4	6	5	3
10	18	0	- 8	0	- 7	0	- 5	10	9	5	8	7	4	6	5	4	6	5	3
18	30	0	- 10	0	- 8	0	- 6	13	10	6	10	8	5	8	6	5	8	6	3
30	50	0	- 12	0	- 10	0	- 8	15	13	8	12	10	6	9	8	6	9	8	4

Note 1) Dimension 0.6 mm is included in this category

Table 8-1(2) Inner ring (running tolerance and width)

Unit: µm

-	inal bore meter	assen	ial runc nbled b nner rir $K_{ m ia}$	earing	$S_{ m d}$	S _{ia} 2)	Sing	jle inn	er ring ⊿		n devi	ation	Siı	ngle inr	_	y width	deviat	ion		ner rir h varia $V_{B{ m s}}$	
	mm	class 0	class 6	class 5	class 5	class 5	cla	ss 0	clas	ss 6	cla	ss 5	cla	ss 0	clas	ss 6	cla	ss 5	class 0	class 6	class 5
over	up to		max.		max.	max.	upper	lower	upper	lower	upper	lower	upper	lower	upper	lower	upper	lower		max.	
0.6	¹⁾ 2.5	10	5	4	7	7	0	- 40	0	- 40	-	- 40	-	-	_	-	0	- 250	12	12	5
2.5	10	10	6	4	7	7	0	- 120	0	– 120	0	- 40	0	- 250	0	- 250	0	- 250	15	15	5
10	18	10	7	4	7	7	0	- 120	0	– 120	0	- 80	0	- 250	0	- 250	0	- 250	20	20	5
18	30	13	8	4	8	8	0	– 120	0	– 120	0	- 120	0	- 250	0	- 250	0	- 250	20	20	5
30	50	15	10	5	8	8	0	- 120	0	– 120	0	- 120	0	- 250	0	- 250	0	- 250	20	20	5

 S_d : perpendicularity of inner ring face with respect to the bore Notes 1) Dimension 0.6 mm is included in this category.

Sia: axial runout of assembled bearing inner ring

2) Applicable to deep groove ball bearings and angular contact ball bearings.

3) Applicable to bearing rings made for matched bearings.

Table 8-2(1) Outer ring (outside diameter)

Unit: µm

Nominal diam	outside eter	Single	olane m		side dia _{Dmp}	meter de	eviation		΄.		ı	le dian eter seri		1			Diamete	er series		side diamete $V_{D{ m mp}}$	er variation
<i>D</i> mr	n	clas	ss 0	cla	ss 6	clas	ss 5										2, 3, 4	0, 1, 2, 3, 4 class 6 ²)		class 6 2)	class 5
over	up to	upper	lower	upper	lower	upper	lower		max.			max.			max.		m	ax.		max.	
2.51)	6	0	- 8	0	- 7	0	– 5	10	9	5	8	7	4	6	5	4	10	9	6	5	3
6	18	0	- 8	0	- 7	0	- 5	10	9	5	8	7	4	6	5	4	10	9	6	5	3
18	30	0	- 9	0	- 8	0	-6	12	10	6	9	8	5	7	6	5	12	10	7	6	3
30	50	0	- 11	0	- 9	0	- 7	14	11	7	11	9	5	8	7	5	16	13	8	7	4
50	80	0	- 13	0	- 11	0	- 9	16	14	9	13	11	7	10	8	7	20	16	10	8	5

Notes 1) Dimension 2.5 mm is included in this category.

Table 8-2(2) Outer ring (running tolerance and width)

Unit: µm

Nominal diam	eter		inout of a ring outer $K_{ m ea}$	r ring	$S_{ m D}$	$S_{ m ea}^{ m 2)}$		of a single ng widht Cs	width variation $V_{C{ m s}}$	ation
m	m	class 0	class 6	class 5	class 5	class 5	classes	0,6 & 5	classes 0 & 6	class 5
over	up to		max.		max.	max.	upper	lower	max.	
2.51)	6	15	8	5	8	8			Same as the	5
6	18	15	8	5	8	8	Same as		allowable	5
18	30	15	9	6	8	8			value of V_{Bs} for d of the	5
30	50	20	10	7	8	8	bearing		same	5
50	80	25	13	8	8	10			bearing	6

 S_{D} : perpendicularity of outer ring outside surface with respect to the face Notes 1) Dimension 2.5 mm is included in this category

 S_{ea} : axaial runout of assembled bearing outer ring

D: Nominal outside diameter

2) Applicable to deep groove ball bearings and angular contact ball bearings.

d: Nominal bore diameter

B: Nominal assembled bearing width

8-2 Clearance of Radial Ball Bearings

Table 8-3 Radial internal clearance of deep groove ball bearings (cylindrical bore)

Unit: µm

Nominal bo	re diameter				Radial intern	al clearance				
<i>d</i> , r	mm	C	N	(C3	c	:4	C5		
over	up to	min.	max.	min.	max.	min.	max.	min.	max.	
2.5	6	2	13	8	23	14	29	20	37	
6	10	2	13	8	23	14	29	20	37	
10	18	3	18	11	25	18	33	25	45	
18	24	5	20	13	28	20	36	28	48	
24	30	5	20	13	28	23	41	30	53	
30	40	6	20	15	33	28	46	40	64	
40	50	6	23	18	36	30	51	45	73	

Remark) When the above values are used as clearance measurements, the values should be corrected by adding the increase of the radial internal clearances caused by the measuring load. The values to be added are shown below

Nominal bo d , r		Measuring load		Amounts of clea	rance correction	l
<i>a</i> , ı	11111	N	CN	C3	C4	C5
over	up to			00	04	03
2.5	18	24.5	4	4	4	4
18	50	49	5	6	6	6

Table 8-4 Radial internal clearance of extra small/miniature ball bearings

Unit: µm

Clearance code	N	//3	N	14	N	1 5	N	16
Clearance code	min.	max.	min.	max.	min.	max.	min.	max.
Clearance	5	10	8	13	13	20	20	28

Remark) When the above values are used as clearance measurements, the values should be corrected by adding the increase of the radial internal clearances caused by the Unit: um

measuring load	Α	mounts of clea	rance correctio	n
N	М3	M4	M5	М6
2.3	1	1	1	1

Remark) Miniature ball bearings: bearing with an outside diameter of less than 9 mm

Remark) Consult JTEKT regarding the tolerance and internal clearance of inch series bearings (bearing basic number EE3S).

8-3 Tolerance and Internal Clearance of K Series Full Complement Hybrid Ceramic Ball Bearings

Table 8-5 Tolerance and internal clearance of K Series Full Complement Hybrid Ceramic Ball Bearings

	Single plane mean bore diameter	Single plane mear	outer ring wiath	Radial rur	out of ass	embled bea	ring, max.	S_{ia}	$S_{ m ea}$		internal	
Bore diameter	deviation Δ_{dmp}	deviation $\Delta D_{\rm mp}$	deviation Δ_{Bs} , Δ_{Cs}	Inner r	ing, $K_{ m ia}$	Outer r	ing, $K_{ m ea}$	Inner ring	Outer ring	clear	ance	Bore diameter
No.	class K0	class K0	class K0	clas	s K0	clas	s K0	class K0	class K0	clas	s K0	No.
	category I category II	category I category I		category I	category I	category I	category II	Class No	Class No	Deep groove type	Four point contact type	
010	0 –10			13	8	20	10			25 to 41	25 to 38	010
015	0 -13	0 –13		15	10	20	10	Same as the tolerance for the radial	Same as the	30 to 46	30 to 43	015
020			0		13		13		tolerance for the radial			020
025	0 –15		-127	20	13	25	10	runout of the inner ring	runout of the outer ring	30 to 61	30 to 56	025
030		0										030
035	0 –20	–15		25	15	30	15			41 to 71	41 to 66	035

 $S_{\rm ia}, S_{\rm ea}$: axial runout of assembled bearing inner or outer ring, max.

[Notes] Category I specifications are applied to deep groove ball bearings.

Category I specifications are applied to angular contact bearings and four point contact ball bearings.

²⁾ Applicable when no snap ring is fitted.

Application Examples



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J

1 Clean Environments

Transfer Robot for Semiconductor and LCD Manufacturing Equipment

For application in transfer robots for semiconductor and liquid crystal manufacturing equipment, bearings are required to be low in particle emissions and have a long service life.

Bearings may be delivered incorporated in arm units for improved assemblability and maintainability.

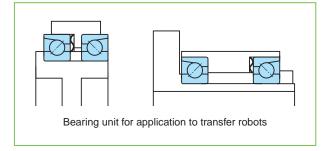


- Applicable to vacuum environments and clean environments
- Optimal for machine size reduction

Product: K Series Full Complement Hybrid Ceramic Ball Bearing

■ Use conditions

Lubrication: Grease or clean pro coating Temperature: Room temp. to 200°C Ambient pressure: 10⁻³ Pa



Gates in Chemical Vapor Deposition Equipment

Hybrid Ceramic Ball Bearings and Clean Pro Linear Motion Ball Bearings are widely used for the doors of the chemical vapor deposition (CVD) equipment.

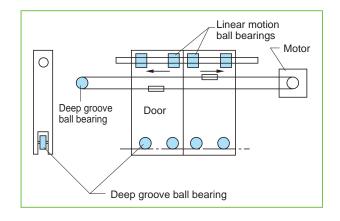
Applicable to high temperature, vacuum and clean environments

Product: Hybrid Ceramic Ball Bearing Clean Pro Linear Motion Ball Bearing

■ Use conditions

Rotational speed: 10 to 200 min⁻¹ Lubrication: Clean pro coating Temperature: 200°C

Ambient pressure: Normal to 10⁻⁴ Pa



1-2

Conveyor for Sputtering Equipment

Clean Pro Linear Motion Ball Bearings are widely used for the conveyers in sputtering equipment.



Applicable to vacuum environments and clean environments

Product: Clean Pro Linear Motion Ball Bearing

■ Use conditions

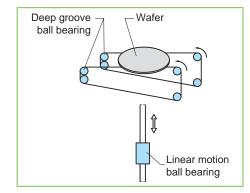
Stroke: 20 mm

Speed: 10 mm/s

Lubrication: Clean pro coating

Temperature: 200°C

Ambient pressure: Normal to 10⁻⁵ Pa



1-4 Chemical Vapor Deposition Machine

Clean Pro Cross Roller Way Bearing Units are widely used in CVD machines due to their low gas and particle emissions.



Applicable to vacuum environments and clean environments

Product: Clean Pro Cross Roller Way Bearing Unit

■ Use conditions

Stroke: 100 mm

Lubrication: Clean pro coating

Temperature: 200°C

Ambient pressure: Normal to 10⁻³ Pa

1 Clean Environments

Etching Equipment

Bearings used in etching machines must be resistant to halogen, hydrofluoric acid, and other corrosive gasses, as well as low in particle emissions. To meet these requirements, PTFE coated Hybrid Ceramic Bearings are used.

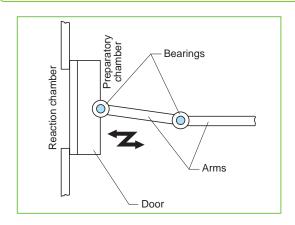
- Resistant to corrosive ambient gases such as halogen and hydrofluoric acid
- Suitable for clean environments thanks to low particle emissions

Product: Hybrid Ceramic Bearing (with special features)

■ Use conditions

Load: Radial load of 10 N

Lubrication: PTFE coating Temperature: Room temp. to 60°C Ambient pressure: Normal to 10⁻² Pa



Liquid Crystal Panel Bonding and

Substrate bonding press jigs for use in furnaces must be low

The Clean Pro Hybrid Ceramic Linear Motion Ball Bearings

in particle emissions and have a long service life under high

LC Sealing Furnace

temperature conditions.

are widely used for such jigs.

Suitable for clean environments thanks to low particle emissions

Product: Hybrid Ceramic Linear Motion Ball Bearing

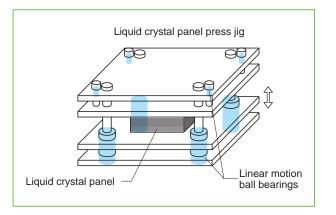
■ Use conditions

Stroke speed: 5 mm/s

Lubrication: Clean pro coating

Temperature: 200°C

Ambient pressure: Normal pressure



Sputtering Equipment

Sputtering systems have a high temperature vacuum conveyor, in which High temperature Clean Pro Bearings are



Applicable to a clean environment under high temperature and vacuum conditions

Product: High temperature Clean Pro Bearing

■ Use conditions

Rotational speed: 60 min⁻¹

Load: Radial load of 100 to 150 N

Lubrication: High temperature Clean pro coating

Temperature: Room temp. to 260°C

Ambient pressure: 10⁻⁵ Pa

Wafer Transfer Equipment

For application in wafer transfer equipment, low particle emissions performance is required.

For such devices, Clean Pro Hybrid Ceramic Linear Way Bearing Units are widely used.



- Suitable for clean environments thanks to low particle emissions
- Corrosion resistant to cleaning agent splashes

Product: Hybrid Ceramic Linear Way Bearing Unit (with special features)

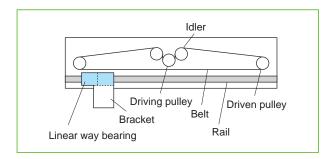
■ Use conditions

Stroke speed: 350 mm/s

Lubrication: Clean pro coating

Temperature: Room temp.

Ambient pressure: Normal pressure



Vacuum Environments

2

2 Vacuum Environments

Vacuum Evaporator

Bearings used in the planetary section of vacuum evaporator are required to be high in durability under high temperatures, high load (moment) conditions. To ensure a long bearing life under high temperature conditions, High temperature Hybrid Ceramic Bearings with special features are used.

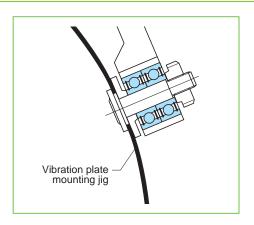
 Improved reliability in vacuum and high temperature environments Product: High Temperature Hybrid Ceramic Bearing (with special features)

■ Use conditions

Rotational speed: 1 to 30 min⁻¹

Lubrication: Molybdenum disulfide or silver

Temperature: 200 to 400°C Ambient pressure: 10⁻⁶ to 10⁻⁸ Pa



Bearing Units, which integrate the flange and shaft.

For rotational anode X-ray tubes, Full Complement Ball

These bearing units are required to be resistant to vacuum,

good high speed performance, heat resistant, and load capacity.

X-ray Tube

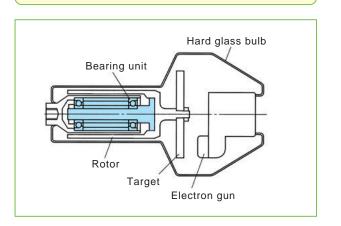
 Improved reliability in vacuum and high temperature environments **Product: Full Complement Ball Bearing Unit**

■ Use conditions

Rotational speed: 3 000 to 10 000 min⁻¹

Lubrication: Silver

Temperature: 250 to 500°C Ambient pressure: 10⁻⁵ Pa



Turbo Molecular Pump

Magnetic bearings are used in turbo molecular pumps driven at extremely high speeds. To protect the blades from fracture in case of a power failure or magnetic failure, touchdown bearing units are used. As touchdown bearings, Full Complement Hybrid Ceramic Ball Bearings are used to increase the service life of the touchdown bearings under severe hostile conditions.

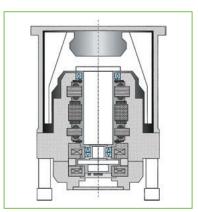
Improved reliability in vacuum environments

99

Product: Full Complement Hybrid Ceramic Ball Bearing (with special features)

■ Use conditions

Rotational speed: 20 000 to 60 000 min⁻¹ Lubrication: Molybdenum disulfide or silver Ambient pressure: 1 Pa



3 High Temperature Environments

Furnaces Cars

The bogies, conveyers and other carrier systems used in furnaces are exposed to high temperatures.

Because of their high heat resistance, High Temperature Hybrid Ceramic Bearings are used in such applications.





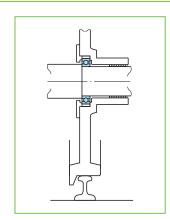
Applicable to high temperature environments

Product: High Temperature Hybrid Ceramic Bearing

■ Use conditions

Rotational speed: 10 to 500 min⁻¹

Lubrication: Graphite Temperature: 500°C



Carton Manufacturing Equipment

In carton manufacturing equipment, polyethylene film, which is attached to carton board in advance, is heat bonded by a gas burner in the high temperature gas burner bonding process.

The PN Bearings, which have superior heat resistance, are used to support the guide rollers of the belt that carries carton board in this process, thus avoiding contaminating the carton board with grease.



- Prevention of grease scattering
- Improved durability and reliability under high temperatures

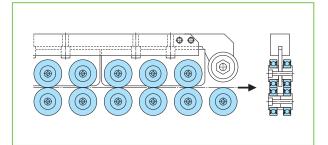
Product: PN Bearing

■ Use conditions

Rotational speed: 3 000 to 4 000 min⁻¹

Lubrication: Molybdenum disulfide and other means

Temperature: 220°C



Baking Furnace Cars

In the kiln that bakes fluorine resin onto the heat rollers of copying machines, conveyor bearings must be low in particle emissions under high temperatures. Because it is structurally difficult to mount bearings accurately, High temperature Hybrid Ceramic Bearings are used for this application, along with aligning rings.

Compatible with high temperature environments

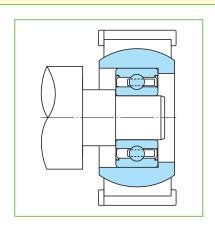
Product: High Temperature Hybrid Ceramic Bearing

■ Use conditions

Rotational speed: 3 to 10 min⁻¹

Lubrication: Graphite

Temperature: 400 to 500°C



Tube Annealing Furnace Guide Rolls

The guide roll bearings installed inside tube annealing furnaces are used under high temperatures without lubrication. Hybrid Ceramic Bearings are suitable for such applications.

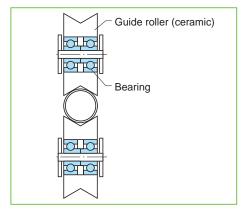
Compatible with high temperature environments

Product: Hybrid Ceramic Bearing

■ Use conditions

Rotational speed: 300 min⁻¹

Temperature: 300°C



4 Corrosive Environments

Synthetic Fiber Manufacturing Equipment

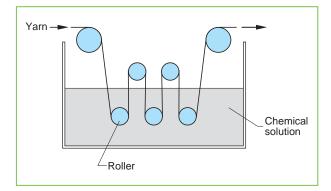
Acid solution, alkaline solution, water, and other liquids are used in synthetic fiber yarn reinforcing processes. Corrosion Resistant Hybrid Ceramic Bearings are applied in such corrosive environments.

Corrosion resistance under acid solution, alkaline solution and water

Product: Corrosion Resistant Hybrid Ceramic Bearing

■ Use conditions

Rotational speed: 20 to 100 min⁻¹ Lubrication: Chemical solution Temperature: Room temp. to 90°C



Aluminum Electrolytic Capacitor Manufacturing Equipment

In an aluminum foil electrolytic capacitor manufacturing equipment, a strong acid solution is used to treat the aluminum foils

High Corrosion Resistant Ceramic Bearings are widely used in such highly corrosive environments.



Corrosion resistance to strong acid solution

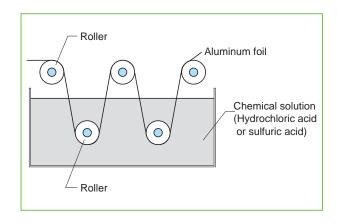
Product: High Corrosion Resistant Ceramic Bearing

■ Use conditions

Rotational speed: 50 min⁻¹ Lubrication: Chemical solution

(hydrochloric acid and sulfuric acid)

Temperature: 90°C



Blood Contrifuge

Corrosion resistance is required of bearings to be used in blood contrifuge especially to physiological saline.

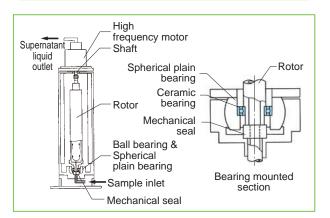
Hybrid Ceramic Bearings with bearing rings coated with a corrosion resistant film are suitable for such corrosive environments.

Corrosion resistance to physiological saline

Product: Hybrid Ceramic Bearing (with special coating)

■ Use conditions

Rotational speed: 20 000 min⁻¹ Lubrication: Grease Temperature: –10 to 10°C



Liquid Crystal Polarizing Film Manufacturing Equipment

Liquid crystal polarizing film manufacturing equipment use acid solution, alkaline solution, dying solution, distilled water, and other solutions.

In such corrosive environments, Corrosion Resistant Hybrid Ceramic Bearings are widely used.

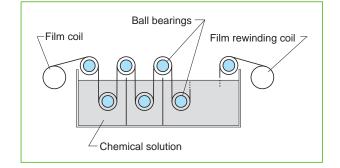


 Corrosion resistance to solutions such as acid solution, alkaline solution, dying solution, and distilled water

Product: Corrosion Resistant Hybrid Ceramic Bearing

■ Use conditions

Rotational speed: 80 min⁻¹ Lubrication: Chemical solution Temperature: Room temp. to 80°C



4 Corrosive Environments

Spin-dryer for Wafer Cleaning Equipment

In semiconductor wafer cleaning processes, wafers are cleaned in cleansing chemicals, rinsing liquids, distilled water, and other liquids

Because of their high corrosion resistance, Corrosion Resistant Hybrid Ceramic Bearings are widely used in wafer cleaners.



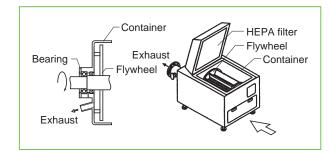
Corrosion resistance to solutions such as cleaning

Product: Corrosion Resistant Hybrid Ceramic Bearing

■ Use conditions

Rotational speed: 2 000 to 3 000 min⁻¹

Lubrication: Grease Temperature: Room temp.



chemicals, rinsing liquids, and distilled water

Wafer Cleaning Equipment for Chemical Mechanical Polishing System

In the semiconductor multilayer production process, each wafer surface should be treated to maintain evenness. This process uses chemical mechanical polishing equipment, and the cleaner attached to the equipment uses Corrosion Resistant Ceramic Bearings.



Corrosion resistance to corrosive solutions

Product: Corrosion Resistant Ceramic Bearing

■ Use conditions

Rotational speed: 100 min⁻¹ Lubrication: Fluorine polymer Temperature: Room temp.

5 Magnetic Field Environments

Electron Beam Lithography

The bearings in semiconductor production electron beam

Because of their non-magnetic characteristics, Hybrid

lithography are exposed to strong magnetic fields.

Ceramic Bearings are used in such machines.

Compatible with vacuum, strong magnetic field environments

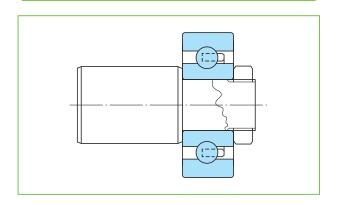
Product: Non-magnetic Hybrid Ceramic Bearing

■ Use conditions

Rotational speed: 100 min⁻¹

Lubrication: Grease

Temperature: Room temp. Ambient pressure: 10⁻⁵ Pa



Ultrasonic Motor in Magnetic Resonance Imagers

The motors installed in magnetic resonance imagers (MRI) use magnetism insensitive Ceramic Bearings.



Compatible with strong magnetic field environments

Product: Ceramic Bearing

■ Use conditions

Rotational speed: 500 min⁻¹

Lubrication: Grease

Temperature: Room temp.

Electric Field Environments

6 Electric Field Environments

Wind Turbine Generator

Wind Turbine Generator are strongly required to operate for extensive periods of time without the need of maintenance. However, bearings used in generators are subject to electrical pitting, which may cause the bearings to break down.

Hybrid Ceramic Bearings, which have superior durability and reliability, are widely used in such aerogenerators.



- Prevention of electrical pitting
- Extension of grease service life (three times longer than Koyo steel bearings)

Product: Hybrid Ceramic Bearing

■ Use conditions

Rotational speed: 2 700 min⁻¹

Lubrication: Grease

Temperature: Below freezing point to approx. 60°C

Bearing location: Generators



Motor

Bearings used in motors are susceptible to electrical pitting. Hybrid Ceramic Bearings are widely used to prevent such pitting.



Prevention of electrical pitting

Product: Hybrid Ceramic Bearing

■ Use conditions

Rotational speed: 5 000 min⁻¹

Lubrication: Grease

Temperature: -10 to 120°C



DVD Sputtering Equipment

To improve reliability further, Hybrid Ceramic Bearings are used.

Insulation

Product: Hybrid Ceramic Bearing

■ Use conditions

Rotational speed: 300 min⁻¹ Lubrication: Grease Temperature: Room temp.



Photographic Film Manufaturing Equipment

A photographic film production line treats film surfaces by applying a high voltage.

Hybrid Ceramic Bearings are widely used in such environments, because the ceramic inner ring and balls serve as

Insulation under high voltage environments

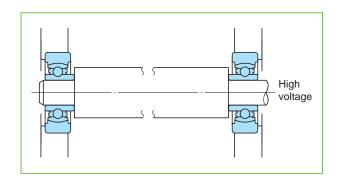
Product: Hybrid Ceramic Bearing (with special features)

■ Use conditions

Rotational speed: 200 min⁻¹

Lubrication: Grease

Temperature: Room temp.



7 High Speed Applications

Turbocharger

Bearings that support the spindle of turbochargers should have good acceleration response characteristics and high durability under low viscosity, contaminated oil.

Because of their high reliability in these respects, Hybrid Ceramic Bearings are widely used for this application.



- Three times longer service life than that of steel bearings
- Acceleration response up 20%
- An 80% reduction in oil supply

Product: Hybrid Ceramic Bearing

■ Use conditions

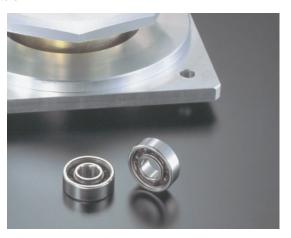
Rotational speed: 180 000 to 210 000 min⁻¹

Lubrication: Oil Temperature: 350°C



Polygon Scanner Motor

Hybrid Ceramic Bearings, which exhibit superior high speed performance, are widely used in high speed polygon scanner



Product: Hybrid Ceramic Bearing

■ Use conditions

Rotational speed: 26 000 min⁻¹ or higher Lubrication: Grease

Excellent reliability in high speed rotation

Spindle for Machine Tool

Machine tool spindle bearings are required to have superior rotational performance at extremely high speeds, quick acceleration/ deceleration, high rigidity, and reduced temperature rises.

Hybrid Ceramic Bearings, which satisfy these requirements, are widely used in this application.

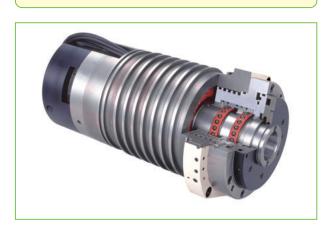


- 20% to 30% reduction in temperature rises
- The upper limit of the rotational speed range is 1.2 to 1.5 times higher (compared with Koyo steel bearings).

Product: Hybrid Ceramic Bearing (High Ability Angular Contact Ball Bearing)

■ Use conditions

Rotational speed: 25 000 min⁻¹ ($d_m n = 2.75 \times 10^6$) Lubrication: Oil or grease Spindle power: 75 kW



Switched Reluctance Motor

For high speed, high efficiency switched reluctance (SR) motors, which do not use coils or permanent magnets, Hybrid Ceramic Bearings are applied.



Excellent reliability in high speed rotation

Product: Hybrid Ceramic Bearing

■ Use conditions

Rotational speed: 30 000 min⁻¹ Lubrication: Grease

J

High Speed Applications

7 High Speed Applications

Steel Wire Stranding Machine

Product: Hybrid Ceramic Bearing

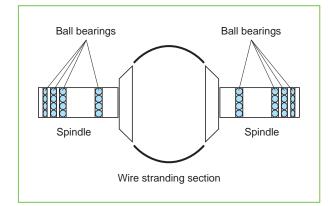
Steel wires for radial tires are produced by stranding steel wires to attain the required strength. In steel wire stranding machines, which involve high speed rotation, Hybrid Ceramic Bearings are used for improved service life and stability.



- Reduced temperature rises
- Reliable durability

■ Use conditions

Rotational speed: 6 000 min⁻¹ or higher Lubrication: Grease



-7 Inline Skates

Because of their low running torque and high durability, Hybrid Ceramic Bearings are widely used in speed skates.



Product: Hybrid Ceramic Bearing

■ Use conditions

Rotational speed: 10 000 min⁻¹ Lubrication: Oil or grease

Low torque and improved durability

Jet Electrostatic Coating Machine

In a jet electrostatic coating machine, grease may escape from the spray nozzle due to the air motor, affecting the quality of the paint to be coated.

To resolve this problem, Hybrid Ceramic Bearings that do not use grease are used.

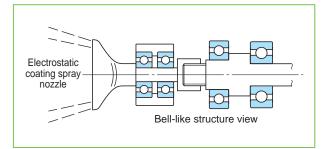


- Prevention of grease scattering
- Prevention of paint contamination

Product: Hybrid Ceramic Bearing

■ Use conditions

Rotational speed: 20 000 min⁻¹ Lubrication: Fluorine polymer



7-8 Micro Gas Turbine Generator

The world's smallest gas turbine generators emit clean exhaust emissions and hence are friendly to the environment. Hybrid Ceramic Bearings are used in these generators because they are low in vibration and noise generation, and have excellent high speed performance.



Improved reliability in high speed rotation

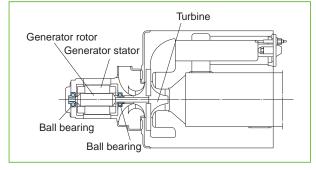
Product: Hybrid Ceramic Bearing

■ Use conditions

Rotational speed: 100 000 min⁻¹

 $(dmn = 2.22 \times 10^6)$

Lubrication: Oil Temperature: 200°C



7 High Speed Applications

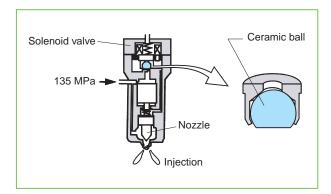
Fuel Injection System Control Valve

Product: Ceramic Ball

The common rail system (fuel injection system), which enables diesel engines to feature high power, good fuel economy and low emissions, is equipped with Ceramic Balls in the control valves.

 Compatible with high pressure fuel injection thanks to improved wear resistance and seizure resistance ■ Use conditions

Maximum pressure: 135 MPa



4 Supplementary Tables

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Supplementary table 1 Shaft tolerances (deviation from nominal dimensions)

Unit: µm (Refer.)

Nomin	nal s mete							Devi	ation o	lasses	of sha	aft dian	neter																	inal shaft	$\frac{1}{\Delta d_{\rm mp}^{1}} \frac{({\sf Refer.})}{({\sf refer.})}$
(n	mm)		46	06	46		76							l ioE	ios	io7	l is	ic	LE.	l/C	l ₂ 7	l mE	m6		nE	n6	ne l	*C *		(mm)	bearing
over 3		6	- 30 - 38	e6 - 20 - 28	f6 - 10 - 18	g5 - 4 - 9	g6 - 4 - 12	h5 0 - 5	h6 0 - 8	h7 0 - 12	h8 0 - 18	0 - 30	h10 0 - 48	js5 ± 2.5	js6 ± 4	js7 ± 6	j5 + 3 - 2	j6 + 6 - 2	k5	+ 9 + 1	+13 + 1	m5 + 9 + 4	m6 +12 + 4	m7 + 16 + 4	n5 +13 + 8	n6 + 16 + 8	p6 + 20 + 12	+ 23 +	7 ove 27 15	r up to 6	0 - 8
6		10	4049	- 25 - 34	- 13 - 22	- 5 - 11	- 5 - 14	0 - 6	0 - 9	0 - 15	0 - 22	0 - 36	0 - 58	± 3	± 4.5	± 7.5	+ 4	+ 7	+ 7 + 1	+10	+16 + 1	+12 + 6	+15 + 6	+ 21 + 6	-		+ 24 + 15	+ 28 +	34	6 10	0
10		18	- 50 - 61	- 32 - 43	- 16 - 27	- 6 - 14	- 6 - 17	0 - 8	0 - 11	0 - 18	0 – 27	0 - 43	0 - 70	± 4	± 5.5	± 9	+ 5	+ 8 - 3	+ 9 + 1	+ 1	+19 + 1	+15 + 7	+18 + 7	+ 25 + 7	+20 +12	+ 23 + 12	+ 29 + 18		23	0 18	- 8
18		30	- 65 - 78	- 40 - 53	- 20 - 33	- 7 - 16	- 7 - 20	- 9	0 - 13	0 - 21	- 33	0 - 52	0 - 84	± 4.5	± 6.5	±10.5	+ 5	+ 9 - 4	+11 + 2	+ 2	+23 + 2	+17 + 8	+21 + 8	+ 29 + 8	+24 +15	+ 28 + 15	+ 35 + 22	+ 28 +	28	8 30	_ 10
30		50	- 80 - 96	- 50 - 66	- 25 - 41	- 9 - 20	- 9 - 25	0 - 11	0 - 16	0 - 25	0 - 39	0 - 62	0 -100	± 5 . 5	± 8	±12.5	+ 6	+11	+13 + 2		+27 + 2	+20 + 9	+25 + 9	+ 34 + 9	+28 +17		+ 42 + 26		34	0 50	0 - 12
50		80	-100 -119	- 60 - 79	- 30 - 49	- 10 - 23	- 1 - 29	0 - 13	0 – 19	0 - 30	0 - 46	0 – 74	0 -120	± 6.5	± 9 . 5	±15	+ 6 - 7	+12	+15 + 2		+32 + 2	+24 +11	+30 +11	+ 41 + 11			+ 51 + 32	+ 41 +	41 5 73	0 65	0 - 15
																			-		-							+ 43 +	43	5 80	
80		120	-120 -142	7294	- 36 - 58	- 12 - 27	134	22 - 15	0 - 22	0 - 35	0 - 54	0 - 87	0 -140	± 7 . 5	±11	±17 . 5	+ 6 - 9	+13 - 9	+18 + 3		+38 + 3	+28 +13	+35 +13	+ 48 + 13	+38 +23		+ 59 + 37		51 8 9 10	0 100	20
																												+ 88 +	03		
120		180	-145 -170	- 85 -110	- 43 - 68	- 14 - 32	- 14 - 39	0 - 18	0 – 25	0 - 40	0 - 63	0 -100	0 -160	± 9	±12.5	±20	+ 7 -11	+14	+21 + 3	+28 + 3	+43 + 3	+33 +15	+40 +15	+ 55 + 15			+ 68 + 43	+ 90 +	63 14 65 14		0
			-170	-110	- 00	- 32	- 39	- 10	- 25	- 40	- 03	-100	-100				-''	-11	+ 3	T 3	+ 3	+13	+15	+ 15	TZ/	T 2/	T 43	+ 93 +	08 68 16	0 180	
																												+106 +	123 77	0 200	
180		250	-170 -199	-100 -129	- 50 - 79	- 15 - 35	1544	0 - 20	0 - 29	0 - 46	0 - 72	0 -115	0 -185	±10	±14.5	±23	+ 7 -13	+16 -13	+24 + 4		+50 + 4	+37 +17	+46 +17	+ 63 + 17		+ 60 + 31	+ 79 + 50	+ 80 +	26 80 20	0 225	0 - 30
																												+ 84 +	84 22	5 250	
250		315	-190 -222	-110 -142	- 56 - 88	- 17 - 40	1749	0 - 23	0 - 32	0 – 52	0 - 81	0 -130	0 -210	±11.5	±16	±26	+ 7 -16	±16	+27	+36 + 4	+56 + 4	+43 +20	+52 +20	+ 72 + 20	+57 +34	+ 66 + 34	+ 88	+ 94 +	94 25	0 280	0 - 35
			-222	-142	- 00	- 40	- 45 	- 23	- 32	- 52	- 01	-130	-210				-10		+ 4	+ 4	+ 4	+20	+20	+ 20	+34	+ 34	+ 50	+ 98 +	98 20		
315		400				- 18 - 43			0 - 36	0 - 57	0 - 89	0 -140	0 -230	±12.5	±18	±28.5	+ 7 -18	±18	+29 + 4		+61 + 4	+46 +21	+57 +21	+ 78 + 21		+ 73 + 37			08		_ 40
																												+114 + + + + + + + + + + + + + + + + + +	189		
400		500				- 20 - 47			0 - 40	0 - 63	0 - 97	0 -155	0 -250	±13 . 5	±20	±31.5	+ 7 -20	±20	+32 + 5		+68 + 5	+50 +23	+63 +23			+ 80 + 40		+172 +	95		U
			260	1.45	76	22	22		0	0	0	0	0						. 22	. 44	. 70	, F0	. 70	. 06	. 76	. 00	. 100	+194 +2	220 50		
500		630	-260 -304	-145 -189		- 22 - 54	2266	0 - 32	0 - 44	- 70	0 -110	0 -175	-280	±16	±22	±35	_	_	+32	+44	+70	+58 +26	+70 +26	+ 96 + 26		+ 88 + 44		+199 +2	225 55 56	0 630	0 - 50
620		000	-290	-160	- 80	- 24	- 24	0	0	0	0	0	0	. 10	. 05	. 40			+36	+50	+80	+66	+80	+110	+86	+100	+138	+225 +2	255 75 63	0 710	0
630		800	-340			- 60			- 50	- 80	-125	-200	-320	±18	±25	±40		_	0	0	0	+30	+30	+ 30		+ 50		+235 +2 +185 +2	265 85 71	0 800	- 75
800	1	000	-320				- 26	0	0	0	0	0	0	±20	±28	±45	_	_	+40		+90	+74	+90	+124		+112		+210 +2	800 210	0 900	0
		550	-376	-226	-142	- 66	- 82	- 40	- 56	- 90	-140	-230	-360			- 13			0	0	0	+34	+34	+ 34	+56	+ 56	+100		310 220 90	0 1 000	-100

Note 1) $\Delta_{\rm dmp}$: single plane mean bore diameter deviation

Supplementary table 2 Housing bore tolerances (deviation from nominal dimensions)

		y table	2 Ho	ousing t	ore tol	erances	s (devia	tion fro	om nom	inal dir	nensior	ıs)																		-	(Refer.)
Nominal be diamete (mm)	ore					Devi	iation o	classes	of hou	sing bo	re dian	neter																	Nominal diame	ter	$\Delta D_{\mathrm{mp}}^{-1}$ of bearing
	o to	E6	F6	F7	G6	G7	Н6	H7	Н8	Н9	H10	JS5	JS6	JS7	J6	J7	К5	К6	K7	M5	M6	M7	N5	N6	N7	P6	P7	R7	over		(class 0)
10	18	+ 43	+ 27		+ 17	+ 24	+11	+ 18		+ 43	+ 70	± 4	± 5.5	± 9	+ 6	+10	+ 2	- 1		1	- 4	0		- 9	- 5	- 15	- 11		10	18	0
40		+ 32 + 53	+ 16 + 33	+ 16 + 41	+ 6 + 20	+ 6 + 28	+13	+ 21	+ 33	+ 52	+ 84	4.5	0.5	10.5	- 5 + 8	- 8 +12	<u> </u>				- 15 - 4	- 18 0	-17 -12	- 20 - 11	- 23 - 7	- 26 - 18	- 29 - 14	- 34 - 20			<u> </u>
18	30	+ 40	+ 20	+ 20	+ 7	+ 7	0	0	0	0	0	± 4.5	± 6.5	±10.5	- 5	- 9	_ 8	-11	- 15	-14	- 17	- 21	-21	- 24	- 28	- 31	- 35	- 41	18	30	_ 9
30	50	+ 66 + 50	+ 41 + 25	+ 50 + 25	+ 25 + 9	+ 34 + 9	+16 0	+ 25	+ 39	+ 62 0	+100	± 5 . 5	± 8	±12.5	+10 - 6	+14 -11	+ 2 - 9	1 -		- 5 -16	- 4 - 20	0 - 25	-13 -24	- 12 - 28	833	- 21 - 37	- 17 - 42	- 25 - 50	30	50	0 - 11
																			1									- 30	50	65	
50	80	+ 79 + 60	+ 49 + 30	+ 60 + 30	+ 29 + 10	+ 40 + 10	+19 0	+ 30	+ 46	+ 74	+120	± 6.5	± 9.5	±15	+13 - 6	+18 -12	+ 3 -10		1 -	- 6 -19	- 5 - 24	0 - 30			939	- 26 - 45	- 21 - 51	- 60 - 32			0 - 13
		1 00	1 30	1 30	1 10	10										12	10			13	27	50	20	33	55	73	31	- 62	65	80	
		. 04		. 71	. 24	. 47		. 25		. 07	. 140				.10	. 00			. 10			0	10	10	10	20	0.4	- 38	80	100	
80	120	+ 94 + 72	+ 58 + 36	+ 71 + 36	+ 34 + 12	+ 47 + 12	+22 0	+ 35	+ 54	+ 87 0	+140	± 7 . 5	±11	±17.5	+16 - 6	+22 -13	+ 2 -13		1		- 6 - 28	0 - 35	-18 -33		- 10 - 45	- 30 - 52	- 24 - 59	- 73 - 41	400	400	0 - 15
																												- 76	100	120	
																												- 48 - 88	120	140	(up to150)
120	180	+110	+ 68	+ 83	+ 39	+ 54	+25	+ 40	+ 63	+100	+160	± 9	±12.5	±20	+18	+26	+ 3	- 1			- 8	0		- 20	- 12	- 36		- 50	140	160	- 18
120		+ 85	+ 43	+ 43	+ 14	+ 14	0	0	0	0	0		12.5		– 7	-14	-15	5 -21	- 28	-27	- 33	- 40	-39	- 45	- 52	- 61	- 68	- 90 - 53	140		(over 150) 0
																												- 93	160	180	- 25
																												- 60	180	200	
400		+129	+ 79	+ 96	+ 44	+ 61	+29	+ 46	+ 72	+115	+185	10	445		+22	+30	+ 2	2 + 5	+ 13	-11	- 8	0	-25	- 22	- 14	- 41	- 33	-106 - 63			0
180	250	+100	+ 50	+ 50	+ 15	+ 15	0	0	0	0	0	±10	±14.5	±23	- 7	-16	-18		- 1		- 37	- 46			- 60	- 70		-109	200	225	- 30
																												- 67 -113	225	250	
																												- 74	250	280	
250	315	+142 +110	+ 88 + 56	+108 + 56	+ 49 + 17	+ 69 + 17	+32	+ 52	+ 81	+130 0	+210	±11 . 5	±16	±26	+25 - 7	+36 -16	+ 3 -20				- 9 - 41	0 - 52			- 14 - 66	- 47 - 79	- 36 - 88	-126 - 78			0 - 35
		1110	1 30	1 30	' '/	' ''									'	10	20	' ² '	30		71	52	30	37	00	75	00	-130	280	315	33
		. 161	. 00	. 110	. 54	. 75	. 26	. 57	. 00	. 140	. 220				. 20	. 20			+ 17	1.4	10	0	20	00	10	F1	41	- 87	315	355	
315	400	+161 +125	+ 98 + 62	+119 + 62	+ 54 + 18	+ 75 + 18	+36 0	+ 57	+ 89	+140 0	+230	±12 . 5	±18	±28.5	+29 - 7	+39 -18	+ 3 -22				- 10 - 46	0 - 57			1673		4198	- 144 - 93	055	400	0 - 40
																												-150	355	400	
		+175	+108	+131	+ 60	+ 83	+40	+ 63	+ 97	+155	+250				+33	+43	+ 2	2 + 8	+ 18	-16	- 10	0	-33	- 27	- 17	- 55	- 45	-103 -166	400	450	0
400	500	+135	+ 68	+ 68	+ 20	+ 20	0	0	0	0	0	±13 . 5	±20	±31 . 5	- 7	-20	-25				- 50			- 67				-109	450	500	- 45
																												-172 -150			
500	630	+189	+120	+146	+ 66	+ 92	+44	+ 70	+110	+175	+280	±16	±22	±35		_	0	0	0	-26	- 26	- 26	-44	- 44	- 44	- 78	- 78		500	560	0
300	000	+145	+ 76	+ 76	+ 22	+ 22	0	0	0	0	0	±10	ΤΖΖ	±35	_		-32	2 -44	- 70	-58	- 70	- 96	-76	- 88	-114	-122	-148		560	630	- 50
																												-225 -175	600	740	
630	800	+210	+130	+160	+ 74		+50	+ 80	+125	+200	+320	±18	±25	±40	_	_	0	0	0	-30	- 30				- 50		- 88	-255	630	710	0
		+160	+ 80	+ 80	+ 24	+ 24	0	0	0	0	0						-36	5 -50	0 - 80	-66	- 80	-110	-86	-100	-130	-138	-168	-185 -265	710	800	- 75
																												-210	800	900	
800 1	000	+226 +170	+142 + 86		+ 82 + 26	+116 + 26	+56 0	+ 90	+140 0	+230	+360	±20	±28	±45	_	_	0 -40	0 0 -56	0 - 90	-34 -74	- 34 - 90				- 56 -146	-100 -156					0 -100
		170		100	_ 20	20	L										-40				50	124		114	170	130	130	-310	900	1 000	
		. 001	104	. 002	. 04	, 122		. 105	. 105	. 000	. 400									40	40	40	60			100	100	-250	1 000	1 120	
000 1	250	+261 +195	+164 + 98		+ 94 + 28	+133 + 28		+105	+165 0	+260	+420	±23 . 5	±33	±52 . 5	_		0 -47	,	0 -105		- 40 -106		-66 -113			-120 -186		-355			0 -125
					-,																							-365	1 120	1 250	3

Note 1) $\Delta_{\it Dmp}$: single plane mean outside diameter deviation

Supplementary table 3 Numerical values for standard tolerance grades IT

Basic	size							Sta	andard	tolera	ınce g	rades (IT)						
(m	m)	1	2	3	4	5	6	7	8	9	10	11	12	13	14 ¹)	15 ¹)	16 ¹)	17 ¹)	18 ¹)
over	up to					Tole	rances	(µm)							Tole	rances	(mm)		
_	3	0.8	1.2	2	3	4	6	10	14	25	40	60	0.10	0.14	0.26	0.40	0.60	1.00	1.40
3	6	1	1.5	2.5	4	5	8	12	18	30	48	75	0.12	0.18	0.30	0.48	0.75	1.20	1.80
6	10	1	1.5	2.5	4	6	9	15	22	36	58	90	0.15	0.22	0.36	0.58	0.90	1.50	2.20
10	18	1.2	2	3	5	8	11	18	27	43	70	110	0.18	0.27	0.43	0.70	1.10	1.80	2.70
18	30	1.5	2.5	4	6	9	13	21	33	52	84	130	0.21	0.33	0.52	0.84	1.30	2.10	3.30
30	50	1.5	2.5	4	7	11	16	25	39	62	100	160	0.25	0.39	0.62	1.00	1.60	2.50	3.90
50	80	2	3	5	8	13	19	30	46	74	120	190	0.30	0.46	0.74	1.20	1.90	3.00	4.60
80	120	2.5	4	6	10	15	22	35	54	87	140	220	0.35	0.54	0.87	1.40	2.20	3.50	5.40
120	180	3.5	5	8	12	18	25	40	63	100	160	250	0.40	0.63	1.00	1.60	2.50	4.00	6.30
180	250	4.5	7	10	14	20	29	46	72	115	185	290	0.46	0.72	1.15	1.85	2.90	4.60	7.20
250	315	6	8	12	16	23	32	52	81	130	210	320	0.52	0.81	1.30	2.10	3.20	5.20	8.10
315	400	7	9	13	18	25	36	57	89	140	230	360	0.57	0.89	1.40	2.30	3.60	5.70	8.90
400	500	8	10	15	20	27	40	63	97	155	250	400	0.63	0.97	1.55	2.50	4.00	6.30	9.70
500	630	_	_	_	_	_	44	70	110	175	280	440	0.70	1.10	1.75	2.80	4.40	7.00	11.00
630	800	_	_	_	_	_	50	80	125	200	320	500	0.80	1.25	2.00	3.20	5.00	8.00	12.50
800	1 000	_	_	_	_	_	56	90	140	230	360	560	0.90	1.40	2.30	3.60	5.60	9.00	14.00
1 000	1 250	_	-	_	_	_	66	105	165	260	420	660	1.05	1.65	2.60	4.20	6.60	10.50	16.50
1 250	1 600	_	_	_	_	_	78	125	195	310	500	780	1.25	1.95	3.10	5.00	7.80	12.50	19.50
1 600	2 000	_	_	_	_	_	92	150	230	370	600	920	1.50	2.30	3.70	6.00	9.20	15.00	23.00
2 000	2 500	_	_	_	_	_	110	175	280	440	700	1 100	1.75	2.80	4.40	7.00	11.00	17.50	28.00
2 500	3 150	_	_	_	_	_	135	210	330	540	860	1 350	2.10	3.30	5.40	8.60	13.50	21.00	33.00

Note 1) Standard tolerance grades IT 14 to IT 18 (incl.) shall not be used for basic sizes less than or equal to 1 mm.

Supplementary table 4 Steel hardness conversion

Rockwell		Bri	nell	Rocl	kwell	
C-scale 1471.0 N	Vicker's	Standard ball	Tungsten carbide ball	A-scale 588.4 N	B-scale 980.7 N	Shore
68 67 66	940 900 865			85.6 85.0 84.5		97 95 92
65 64 63 62 61	832 800 772 746 720		739 722 705 688 670	83.9 83.4 82.8 82.3 81.8		91 88 87 85 83
60 59 58 57 56	697 674 653 633 613		654 634 615 595 577	81.2 80.7 80.1 79.6 79.0		81 80 78 76 75
55 54 53 52 51	595 577 560 544 528		560 543 525 512 496	78.5 78.0 77.4 76.8 76.3		74 72 71 69 68
50 49 48 47 46	513 498 484 471 458	475 464 451 442 432	481 469 455 443 432	75.9 75.2 74.7 74.1 73.6		67 66 64 63 62
45 44 43 42 41	446 434 423 412 402	40 40 39	21 09 00 90 81	73.1 72.5 72.0 71.5 70.9		60 58 57 56 55
40 39 38 37 36	392 382 372 363 354	36 35 34	71 62 53 44 36	70.4 69.9 69.4 68.9 68.4		54 52 51 50 49
35 34 33 32 31	345 336 327 318 310	3: 3: 3:	27 19 11 01 94	67.9 67.4 66.8 66.3 65.8	(108.5) (108.0) (107.5) (107.0) (106.0)	48 47 46 44 43
30 29 28 27 26	302 294 286 279 272	27 27 28	86 79 71 64 58	65.3 64.7 64.3 63.8 63.3	(105.5) (104.5) (104.0) (103.0) (102.5)	42 41 41 40 38
25 24 23 22 21	266 260 254 248 243	24	53 47 43 37 31	62.8 62.4 62.0 61.5 61.0	(101.5) (101.0) 100.0 99.0 98.5	38 37 36 35 35
20 (18) (16) (14) (12)	238 230 222 213 204	2° 2° 20	26 19 12 03 94	60.5 — — — — —	97.8 96.7 95.5 93.9 92.3	34 33 32 31 29
(10) (8) (6) (4) (2) (0)	196 188 180 173 166 160	17 17 18 19 19	87 79 71 65 58		90.7 89.5 87.1 85.5 83.5 81.7	28 27 26 25 24 24

Mass	SI units	Other Units 1)	Conversion into SI units	Conversion from SI units
Angle	rad [radian(s)]	° [degree(s)] * ′ [minute(s)] * ″ [second(s)] *	1° = $\pi/180 \text{ rad}$ 1′ = $\pi/10 800 \text{ rad}$ 1″ = $\pi/648 000 \text{ rad}$	1 rad=57.295 78°
Length	m [meter(s)]	Å [Angstrom unit] μ [micron(s)] in [inch(es)] ft [foot(feet)] yd [yard(s)] mile [mile(s)]	1Å=10 ⁻¹⁰ m=0.1 nm=100pm 1 µ=1 µ m 1 in=25.4 mm 1 ft=12 in=0.304 8 m 1 yd=3 ft=0.914 4 m 1 mile=5 280 ft=1 609.344 m	1 m=10 ¹⁰ Å 1 m=39,37 in 1 m=3,280 8 ft 1 m=1,093 6 yd 1 km=0.621 4 mile
Area	m²	a [are(s)] ha [hectare(s)] acre [acre(s)]	1 a=100m ² 1 ha=10 ⁴ m ² 1 acre=4 840 yd ² =4 046.86 m ²	1 km ² =247.1 acre
Volume	m ³	ℓ, L [liter(s)] * cc [cubic centimeters] gal (US) [gallon(s)] floz (US) [fluid ounce(s)] barrel (US) [barrels(US)]	1 ℓ = 1 dm ³ =10 ⁻³ m ³ 1 cc=1 cm ³ =10 ⁻⁶ m ³ 1 gal (US)=231 in ³ =3,785 41 dm ³ 1 floz (US)=29.573 5 cm ³ 1 barrel (US)=158.987 dm ³	1 m ³ =10 ³ ℓ 1 m ³ =10 ⁶ cc 1 m ³ =264.17 gal 1 m ³ =33 814 floz 1 m ³ =6.289 8 barrel
Time	s [second(s)]	min [minute(s)]		
Angular velocity	rad/s			
Velocity	m/s	kn [knot(s)] m/h *	1 kn=1 852 m/h	1 km/h=0.539 96 kn
Acceleration	m/s ²	G	1 G=9.806 65 m/s ²	1 m/s ² =0.101 97 G
Frequency	Hz [hertz]	c/s [cycle(s)/second]	$1 \text{ c/s}=1 \text{ s}^{-1}=1 \text{ Hz}$	
Rotation frequency	s ⁻¹	rpm [revolutions per minute] min ⁻¹ * r/min	1 rpm=1/60 s ⁻¹	1 s ⁻¹ =60 rpm
Mass	kg [kilogram(s)]	t [ton(s)] * lb [pound(s)] gr [grain(s)] oz [ounce(s)] ton (UK) [ton(s) (UK)] ton (US) [ton(s) (US)] car [carat(s)]	1 t=10 ³ kg 1 lb=0.453 592 37 kg 1 gr=64.798 91 mg 1 oz=1/16 lb=28.349 5 g 1 ton (UK)=1 016.05 kg 1 ton (US)=907.185 kg 1 car=200 mg	1kg=2.204 6 lb 1 g=15.432 4 gr 1kg=35.274 0 oz 1 t=0.984 2 ton (UK) 1 t=1.102 3 ton (US) 1 g=5 car

Mass	SI units	Other Units 1)	Conversion into SI units	Conversion from SI units
Density	kg/m³			
Linear density	kg/m			
Momentum	kg • m/s			
Moment of momentum, angular momentum	{ kg⋅m²/s			
Moment of inertia	kg • m²			
Force	N [newton(s)]	dyn [dyne(s)] kgf [kilogram-force] gf [gram-force] tf [ton-force] lbf [pound-force]	1 dyn = 10 ⁻⁵ N 1 kgf = 9.806 65 N 1 gf = 9.806 65×10 ⁻³ N 1 tf = 9.806 65×10 ³ N 1 lbf = 4.448 22 N	1 N=10 ⁵ dyn 1 N=0,101 97 kgf 1 N=0,224 809 lbf
Moment of force	N • m [Newton meter(s)]	gf • cm kgf • cm kgf • m tf • m lbf • ft	1 gf·cm =9.806 65×10 ⁻⁵ N·m 1 kgf·cm =9.806 65×10 ⁻² N·m 1 kgf·m =9.806 65 N·m 1 tf·m =9.806 65×10 ³ N·m 1 lbf·ft =1.355 82 N·m	1 N • m=0.101 97 kgf • m 1 N • m=0.737 56 lbf • ft
Pressure, Normal stress	Pa [Pascal(s)] or N/m ² {1 Pa=1 N/m ² }	gf/cm ² kgf/mm ² kgf/m² lbf/in² bar [bar(s)] at [engineering air pressure] mH ₂ O, mAq [meter water column] atm [atmosphere] mHg [meter mercury column]	1 gf/cm ² =9.806 65×10 Pa 1 kgf/mm ² =9.806 65×10 ⁶ Pa 1 kgf/m ² =9.806 65 Pa 1 lbf/in ² =6 894.76 Pa 1 bar=10 ⁵ Pa 1 at=1 kgf/cm ² =9.806 65×10 ⁴ Pa 1 mH ₂ O=9.806 65×10 ³ Pa 1 atm =101 325 Pa 1 mHg = 101 325 Pa 1 Torr =1 mmHg=133.322 Pa	1 MPa =0.101 97 kgf/mm ² 1 Pa =0.101 97 kgf/m ² 1 Pa =0.145×10 ⁻³ lbf/in ² 1 Pa =10 ⁻² mbar 1 Pa=7.500 6×10 ⁻³ Torr
Viscosity	Pa • s [pascal second]	P [poise] kgf • s/m²	10 ⁻² P=1 cP=1 mPa • s 1 kgf • s/m ² =9.806 65 Pa • s	1 Pa • s=0.101 97 kgf • s/m²
Kinematic viscosity	m²/s	St [stokes]	$10^{-2} \text{St} = 1 \text{ cSt} = 1 \text{ mm}^2/\text{s}$	
Surface tension	N/m			

Supplementary table 5(3) SI units and conversion factors

Mass	SI units	Other Units 1)	Conversion into SI units	Conversion from SI units
Work, energy	J [joule(s)] {1 J=1 N·m}	eV [electron volt(s)] * erg [erg(s)] kgf • m lbf • ft	1 eV=(1.602 189 2± 0.000 004 6)×10 ⁻¹⁹ J 1 erg=10 ⁻⁷ J 1 kgf • m =9.806 65 J 1 lbf • ft =1.355 82 J	1 J=10 ⁷ erg 1 J=0.101 97 kgf • m 1 J=0.737 56 lbf • ft
Power	W [watt(s)]	erg/s [ergs per second] kgf • m/s PS [French horse-power] HP [horse-power (British)] lbf • ft/s	1 erg/s=10 ⁻⁷ W 1 kgf • m/s=9.806 65 W 1 PS=75 kgf • m/s=735.5 W 1 HP=550 lbf • ft/s=745.7 W 1 lbf • ft/s=1.355 82 W	1 W=0.101 97 kgf • m/s 1 W=0.001 36 PS 1 W=0.001 34 HP
Thermo-dynamic temperature	K [kelvin(s)]			
Celsius temperature		°F [degree(s) Fahrenheit]	$t^*F = \frac{5}{9}(t-32)^{\circ}C$	$t^{\circ} = (\frac{9}{5}t + 32)^{\circ} F$
Linear expansiona coefficient	K ⁻¹	\mathbb{C}^{-1} [per degree]		
Heat	J [joule(s)] {1 J=1 N·m}	erg [erg(s)] kgf • m cal _{IT} [I. T. calories]	1 erg=10 ⁻⁷ J 1 cal=4.186 8 J 1 Mcal _{IT} =1.163 kW • h	1 J=10 ⁷ erg 1 J=0.238 85 cal _{IT} 1 kW • h=0.86×10 ⁶ cal _{IT}
Thermal conductivity	W/(m • K)	$W/(m \cdot ^{\circ}C)$ cal/ $(s \cdot m \cdot ^{\circ}C)$	1 W/ (m • °C)=1 W/ (m • K) 1 cal/ (s • m • °C)= 4.186 05 W/ (m • K)	
Coeffcient of heat transfer	W/ (m² • K)	$W/(m^2 \cdot ^{\circ}C)$ cal/ $(s \cdot m^2 \cdot ^{\circ}C)$	1 W/ (m ² · °C)=1 W/ (m ² · K) 1 cal/ (s · m ² · °C)= 4.186 05 W/ (m ² · K)	
Heat capacity	J/K	J/°C	1 J/℃=1 J/K	
Massic heat capacity	J/ (kg • K)	J/ (kg • °C)		

Supplementary table 5(4) SI units and conversion factors

Mass	SI units	Other Units 1)	Conversion into SI units	Conversion from SI units
Electric current	A [ampere(s)]			
Electric charge,	C [coulomb(s)]	A • h *	1 A • h=3.6 kC	
quantity of electricity	{1 C=1 A • s}			
Tension, electric potential	V [volt(s)] {1 V=1 W/A}			
Capacitance	F [farad(s)] {1 F=1 C/V}			
Magnetic field strength	A/m	Oe [oersted(s)]	$1 \text{ Oe} = \frac{10^3}{4 \pi} \text{ A/m}$	$1 \text{ A/m} = 4 \pi \times 10^{-3} \text{ Oe}$
Magnetic flux density		Gs [gauss(es)] γ [gamma(s)]	1 Gs= 10^{-4} T 1 $\gamma = 10^{-9}$ T	1 T=10 ⁴ Gs 1 T=10 ⁹ γ
Magnetic flux	Wb [weber(s)] {1 Wb=1 V • s}	Mx [maxwell(s)]	1 Mx=10 ⁻⁸ Wb	1 Wb=10 ⁸ Mx
Self inductance	H [henry (- ries)] {1 H=1 Wb/A}			
Resistance (to direct current)	Ω [ohm(s)] $\{1 \Omega = 1 \text{ V/A}\}$			
Conductance (to direct current)	S [siemens] {1 S=1 A/V}			
Active power	W 1 W=1 J/s =1 A•V			

Supplementary table 6 Inch / millimeter conversion

							inches					
ir	nch	0	1	2	3	4	5	6	7	8	9	10
							mm					
0 1/64 1/32 3/64	0 0.015625 0.03125 0.046875	0 0.3969 0.7938 1.1906	25.4000 25.7969 26.1938 26.5906	50.8000 51.1969 51.5938 51.9906	76.2000 76.5969 76.9938 77.3906	101.6000 101.9969 102.3938 102.7906	127.0000 127.3969 127.7938 128.1906	152.4000 152.7969 153.1938 153.5906	177.8000 178.1969 178.5938 178.9906	203.2000 203.5969 203.9938 204.3906	228.6000 228.9969 229.3938 229.7906	254.0000 254.3969 254.7938 255.1906
1/16	0.0625	1.5875	26.9875	52.3875	77.7875	103.1875	128.5875	153.9875	179.3875	204.7875	230.1875	255.5875
5/64	0.078125	1.9844	27.3844	52.7844	78.1844	103.5844	128.9844	154.3844	179.7844	205.1844	230.5844	255.9844
3/32	0.09375	2.3812	27.7812	53.1812	78.5812	103.9812	129.3812	154.7812	180.1812	205.5812	230.9812	256.3812
7/64	0.109375	2.7781	28.1781	53.5781	78.9781	104.3781	129.7781	155.1781	180.5781	205.9781	231.3781	256.7781
1/8 9/64 5/32 11/64	0.125 0.140625 0.15625 0.171875	3.1750 3.5719 3.9688 4.3656	28.5750 28.9719 29.3688 29.7656	53.9750 54.3719 54.7688 55.1656	79.3750 79.7719 80.1688 80.5656	104.7750 105.1719 105.5688 105.9656	130.1750 130.5719 130.9688 131.3656	155.5750 155.9719 156.3688 156.7656	180.9750 181.3719 181.7688 182.1656	206.3750 206.7719 207.1688 207.5656	231.7750 232.1719 232.5688 232.9656	257.1750 257.5719 257.9688 258.3656
3/16	0.1875	4.7625	30.1625	55.5625	80.9625	106.3625	131.7625	157.1625	182.5625	207.9625	233.3625	258.7625
13/64	0.203125	5.1594	30.5594	55.9594	81.3594	106.7594	132.1594	157.5594	182.9594	208.3594	233.7594	259.1594
7/32	0.21875	5.5562	30.9562	56.3562	81.7562	107.1562	132.5562	157.9562	183.3562	208.7562	234.1562	259.5562
15/64	0.234375	5.9531	31.3531	56.7531	82.1531	107.5531	132.9531	158.3531	183.7531	209.1531	234.5531	259.9531
1/4 17/64 9/32 19/64	0.25 0.265625 0.28125 0.296875	6.3500 6.7469 7.1438 7.5406	31.7500 32.1469 32.5438 32.9406	57.1500 57.5469 57.9438 58.3406	82.5500 82.9469 83.3438 83.7406	107.9500 108.3469 108.7438 109.1406	133.3500 133.7469 134.1438 134.5406	158.7500 159.1469 159.5438 159.9406	184.1500 184.5469 184.9438 185.3406	209.5500 209.9469 210.3438 210.7406	234.9500 235.3469 235.7438 236.1406	260.3500 260.7469 261.1438 261.5406
5/16	0.3125	7.9375	33.3375	58.7375	84.1375	109.5375	134.9375	160.3375	185.7375	211.1375	236.5375	261.9375
21/64	0.328125	8.3344	33.7344	59.1344	84.5344	109.9344	135.3344	160.7344	186.1344	211.5344	236.9344	262.3344
11/32	0.34375	8.7312	34.1312	59.5312	84.9312	110.3312	135.7312	161.1312	186.5312	211.9312	237.3312	262.7312
23/64	0.359375	9.1281	34.5281	59.9281	85.3281	110.7281	136.1281	161.5281	186.9281	212.3281	237.7281	263.1281
3/8	0.375	9.5250	34.9250	60.3250	85.7250	111.1250	136.5250	161.9250	187.3250	212.7250	238.1250	263.5250 263.9219 264.3188 264.7156
25/64	0.390625	9.9219	35.3219	60.7219	86.1219	111.5219	136.9219	162.3219	187.7219	213.1219	238.5219	
13/32	0.40625	10.3188	35.7188	61.1188	86.5188	111.9188	137.3188	162.7188	188.1188	213.5188	238.9188	
27/64	0.421875	10.7156	36.1156	61.5156	86.9156	112.3156	137.7156	163.1156	188.5156	213.9156	239.3156	
7/16	0.4375	11.1125	36.5125	61.9125	87.3125	112.7125	138.1125	163.5125	188.9125	214.3125	239.7125	265.1125
29/64	0.453125	11.5094	36.9094	62.3094	87.7094	113.1094	138.5094	163.9094	189.3094	214.7094	240.1094	265.5094
15/32	0.46875	11.9062	37.3062	62.7062	88.1062	113.5062	138.9062	164.3062	189.7062	215.1062	240.5062	265.9062
31/64	0.484375	12.3031	37.7031	63.1031	88.5031	113.9031	139.3031	164.7031	190.1031	215.5031	240.9031	266.3031
1/2 33/64 17/32 35/64	0.5 0.515625 0.53125 0.546875	12.7000 13.0969 13.4938 13.8906	38.1000 38.4969 38.8938 39.2906	63.5000 63.8969 64.2938 64.6906	88.9000 89.2969 89.6938 90.0906	114.3000 114.6969 115.0938 115.4906	139.7000 140.0969 140.4938 140.8906	165.1000 165.4969 165.8938 166.2906	190.5000 190.8969 191.2938 191.6906	215.9000 216.2969 216.6938 217.0906	241.3000 241.6969 242.0938 242.4906	266.7000 267.0969 267.4938 267.8906
9/16	0.5625	14.2875	39.6875	65.0875	90.4875	115.8875	141.2875	166.6875	192.0875	217.4875	242.8875	268.2875
37/64	0.578125	14.6844	40.0844	65.4844	90.8844	116.2844	141.6844	167.0844	192.4844	217.8844	243.2844	268.6844
19/32	0.59375	15.0812	40.4812	65.8812	91.2812	116.6812	142.0812	167.4812	192.8812	218.2812	243.6812	269.0812
39/64	0.609375	15.4781	40.8781	66.2781	91.6781	117.0781	142.4781	167.8781	193.2781	218.6781	244.0781	269.4781
5/8 41/64 21/32 43/64	0.625 0.640625 0.65625 0.671875	15.8750 16.2719 16.6688 17.0656	41.2750 41.6719 42.0688 42.4656	66.6750 67.0719 67.4688 67.8656	92.0750 92.4719 92.8688 93.2656	117.4750 117.8719 118.2688 118.6656	142.8750 143.2719 143.6688 144.0656	168.2750 168.6719 169.0688 169.4656	193.6750 194.0719 194.4688 194.8656	219.0750 219.4719 219.8688 220.2656	244.4750 244.8719 245.2688 245.6656	269.8750 270.2719 270.6688 271.0656
11/16	0.6875	17.4625	42.8625	68.2625	93.6625	119.0625	144.4625	169.8625	195.2625	220.6625	246.0625	271.4625
45/64	0.703125	17.8594	43.2594	68.6594	94.0594	119.4594	144.8594	170.2594	195.6594	221.0594	246.4594	271.8594
23/32	0.71875	18.2562	43.6562	69.0562	94.4562	119.8562	145.2562	170.6562	196.0562	221.4562	246.8562	272.2562
47/64	0.734375	18.6531	44.0531	69.4531	94.8531	120.2531	145.6531	171.0531	196.4531	221.8531	247.2531	272.6531
3/4	0.75	19.0500	44.4500	69.8500	95.2500	120.6500	146.0500	171.4500	196.8500	222.2500	247.6500	273.0500 273.4469 273.8438 274.2406
49/64	0.765625	19.4469	44.8469	70.2469	95.6469	121.0469	146.4469	171.8469	197.2469	222.6469	248.0469	
25/32	0.78125	19.8438	45.2438	70.6438	96.0438	121.4438	146.8438	172.2438	197.6438	223.0438	248.4438	
51/64	0.796875	20.2406	45.6406	71.0406	96.4406	121.8406	147.2406	172.6406	198.0406	223.4406	248.8406	
13/16	0.8125	20.6375	46.0375	71.4375	96.8375	122.2375	147.6375	173.0375	198.4375	223.8375	249.2375	274.6375
53/64	0.828125	21.0344	46.4344	71.8344	97.2344	122.6344	148.0344	173.4344	198.8344	224.2344	249.6344	275.0344
27/32	0.84375	21.4312	46.8312	72.2312	97.6312	123.0312	148.4312	173.8312	199.2312	224.6312	250.0312	275.4312
55/64	0.859375	21.8281	47.2281	72.6281	98.0281	123.4281	148.8281	174.2281	199.6281	225.0281	250.4281	275.8281
7/8 57/64 29/32 59/64	0.875 0.890625 0.90625 0.921875	22.2250 22.6219 23.0188 23.4156	47.6250 48.0219 48.4188 48.8156	73.0250 73.4219 73.8188 74.2156	98.4250 98.8219 99.2188 99.6156	123.8250 124.2219 124.6188 125.0156	149.2250 149.6219 150.0188 150.4156	174.6250 175.0219 175.4188 175.8156	200.0250 200.4219 200.8188 201.2156	225.4250 225.8219 226.2188 226.6156	250.8250 251.2219 251.6188 252.0156	276.2250 276.6219 277.0188 277.4156
15/16	0.9375	23.8125	49.2125	74.6125	100.0125	125.4125	150.8125	176.2125	201.6125	227.0125	252.4125	277.8125
61/64	0.953125	24.2094	49.6094	75.0094	100.4094	125.8094	151.2094	176.6094	202.0094	227.4094	252.8094	278.2094
31/32	0.96875	24.6062	50.0062	75.4062	100.8062	126.2062	151.6062	177.0062	202.4062	227.8062	253.2062	278.6062
63/64	0.984375	25.0031	50.4031	75.8031	101.2031	126.6031	152.0031	177.4031	202.8031	228.2031	253.6031	279.0031

Supplementary table 7 Cleanliness classes

JIS B9920/ISO14644-1 Upper limit to the concentration of individual cleanliness classes (particle count/m³) (Comparison with the U.S. federal standards)

Cleanliness class									
FED 209D (particle count/ft³)	_	_	class 1	class 10	class 100	class 1 000	class 10 000	class 100 000	_
Particulate diameter (µm)	class 1	class 2	class 3	class 4	class 5	class 6	class 7	class 8	class 9
0.1	10	100	1 000	10 000	100 000	1 000 000	_	_	_
0.2	2	24	237	2 370	23 700	237 000	_	_	_
0.3	_	10	102	1 020	10 200	102 000	_	_	_
0.5	_	4	35	352	3 520	35 200	352 000	3 520 000	35 200 000
1.0	_	_	8	83	832	8 320	83 200	832 000	8 320 000
5.0	_	_	_	_	29	293	2 930	29 300	293 000
Particle diameter range	0.1 to 0.2	0.1 to 0.5	0.1 to	0 1.0	0.1 to	o 5 . 0		0.5 to 5.0	

Remarks 1) The U.S. Federal Standards are no longer in effect; however, in Japan and in the U.S., the old Federal Standard (FED-STD-209D) is commonly referred to.

2) The FED-STD-209D specifies that Class 100 limits the count of particles 0.5 μm or greater in diameter) to 100 (3 520 per cubic meter). This corresponds to Class 5 in the Japanese Industrial Standard and ISO Standard. (1 m³ = 35.3 ft³)

	JTEKT
- I	TEKT CORPORATION

Company name		Division, department, and section	
Name of staff member in charge	Phone	FAX	JIEKI COKP

Koyo Extreme Special Environments Specifications Sheet for Ceramic Bearings and/or **EXSEV** Bearings

Note: For the selection of the most suitable bearing this sheet must be completed in as much detail as possible.	Date
--	------

	CICCHOIT OF LITE	most suitable bearing this sheet must be com	ipieteu iii a	3 1110	JUIT UELO	ili as possible.	Date	
Bearing size and bearing number								
Application	a. For new	design b. For repair						
Required performance	a. Life b. High	speed c. Low dust generation d. Vacuum e. Corrosion	n resistance f	. Hig	h temperat	ure g. Non-magn	etism h. Insulation	i. Others ()
	Rotation speed, min ⁻¹	a. Inner ring rotating b. Outer ring romin. : max. : Normal :		Kunning time	· h	/day		
Operating						Material	Tolerance	Surface roughness
condition				ıtıng	Shaft	emperature g. Non-magnetism h. Insulation 24 h/day h/day Other () Material Tolerance Shaft ousing lity: Cleanness: pheric \iff vacuum c. Vacuum d.		
	IN .	Moment.	[Ь	Housing			
		Temperature: Normal , max	x. H	lum	idity:		Cleanness:	
Application Application	<	c. Vacuum d	. Other ()					
	Environment	Corrosive gas:						
		Corrosive liquid:						
	Bearing ma	nterial:						
			L	ubr	icant:			
1								
condition	Failure con	dition:						
Rough sketch of bearing mounting section and/or other remarks								

			JILKI
Company name		Division, department, and section	ITEKT CORPORATION
Name of staff member in charge	Phone	FAX	JIEKI CORPORATION

Koyo Extreme Special Environments Specifications Sheet for Linear Motion Bearings

Note: For the selection of the most suitable bearing this sheet must be completed in as much detail as possible. Date

.	1					<u> </u>				
Bearing size and bearing number										
Application	a. For new design b. For repair									
Required performance	a. Life b. High speed c. Low dust generation d. Vacuum e. Corrosion resistance f. High temperature g. Non-magnetism h. Insulation i. Others ()									
	Linear motion speed, mm/s	min. : max. : Normal : Start-up time :		Running time	· 24 h/d · h/d · Other	ay				
	Stroke, mm			Drive	system					
Operating condition	Load N	Bearing loaded : Moment : Other :	Bearing loaded : Moment :							
	Environment	Temperature: Normal , max.			idity:	Cleanness:				
		Pressure: Pa	a. Atmospheric	b. Atmo	ospheric <	c. Vacuum	d. 0	ther ()	
		Corrosive gas:								
		Corrosive liquid:								
	Bearing ma	aterial:								
	Lubrication	:		Lubri	icant:					
Present	Bearing life:									
condition	Failure con	dition:								
Rough sketch of bearing mounting section and/or other remarks										

By this sheet, the ceramic and/or EXSEV bearings most suitable to operating conditions can be created.

[•] By this sheet, the linear motion bearings most suitable to operating conditions can be created.

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